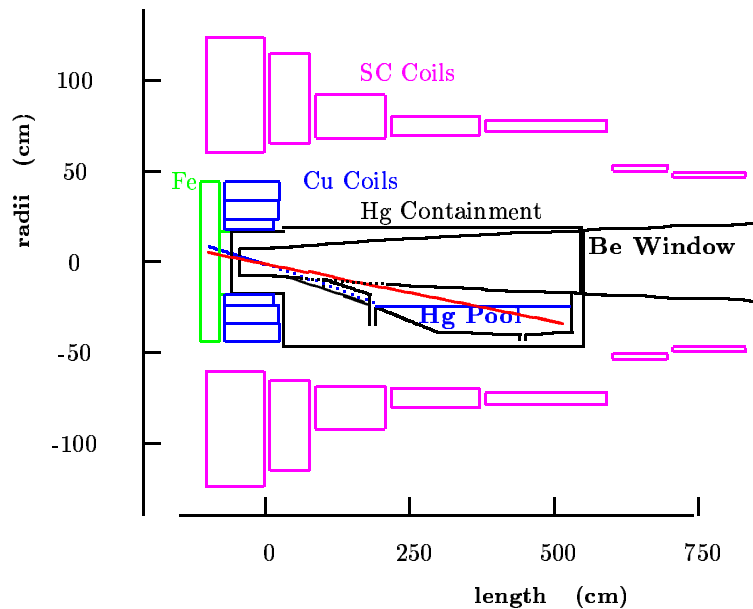
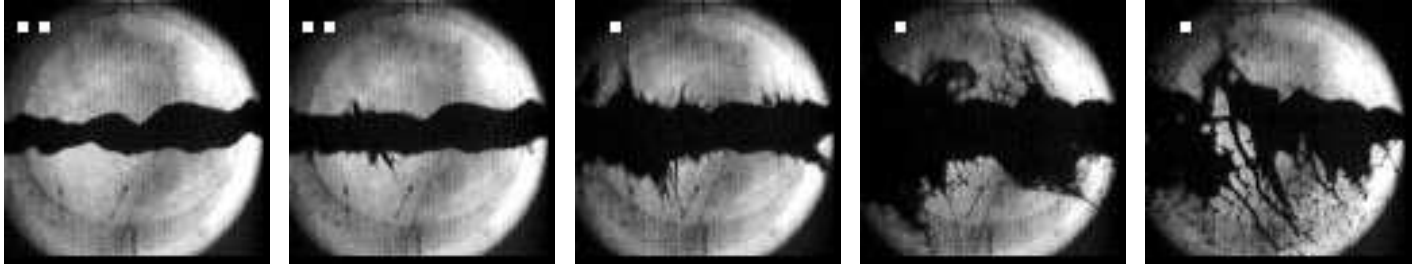


# Targetry for a Neutrino Factory and Muon Collider



K.T. McDonald

Princeton U.

NuFact03

Columbia U., June 9, 2003

Targetry Web Page:

<http://puhep1.princeton.edu/mumu/target/>

Various Physics Examples:

<http://puhep1.princeton.edu/~mcdonald/examples/>

**A Short Course on Targetry**  
**presented at the NuFact03 Summer Institute**  
**June 4, 2003**

E. Fermi: “I can calculate anything to 20% in 20 minutes.”

An everyday targetry physics question: What is the threshold intensity of sunlight to damage human skin?

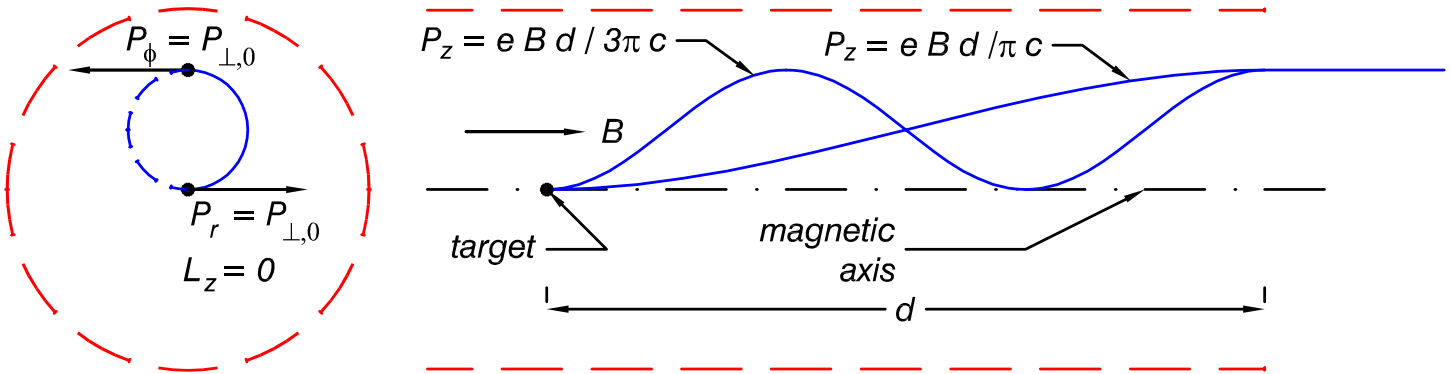
*[Ans: Bright sunlight,  $\approx 1 \text{ kW/m}^2$ .]*

A metaphysics question: Why do people enjoy getting sunburned?

## A Solenoidal Targetry System for a Superbeam

- A precursor to a Neutrino Factory is a Neutrino Superbeam based on decay of pions from a multimegawatt proton target station.
- 4 MW proton beams are achieved in both the BNL and FNAL (and CERN) scenarios via high rep rates:  $\approx 10^6$ /day.
- Classic neutrino horns based on high currents in conductors that intercept much of the secondary pions will have lifetimes of only a few days in this environment.
- Consider instead a solenoid “horn” with conductors at larger radii than the pions of interest – similar to the Neutrino Factory capture solenoid.
- Pions produced on axis inside the solenoid have zero (canonical) angular momentum,  $L_z = r(P_\phi + eA_\phi/c) = 0$ ,  $\Rightarrow P_\phi = 0$  on exiting the solenoid.
- If the pion has made exactly 1/2 turn on its helix when it reaches the end of the solenoid, then its initial  $P_r$  has been rotated into a pure  $P_\phi$ ,  $\Rightarrow P_\perp = 0$  on exiting the solenoid,  $\Rightarrow$  Point-to-parallel focusing.

## Narrowband Beam via Solenoid Focusing



- The point-to-parallel focusing occurs for  $P_\pi = e B d / (2n+1)\pi c$ .
- $\Rightarrow$  Narrowbeam neutrino beam with peaks at

$$E_\nu \approx \frac{e B d}{(2n+1)2\pi c}$$

- $\Rightarrow$  Can study several neutrino oscillation peaks at once, at

$$\frac{1.27 M_{23}^2 [\text{eV}^2] L [\text{km}]}{E_\nu [\text{GeV}]} = \frac{(2n+1)\pi}{2}$$

- Get both  $\nu$  and  $\bar{\nu}$  at the same time,
  - $\Rightarrow$  Must use detector that can identify sign of  $\mu$  and  $e$ ,
  - $\Rightarrow$  Magnetized liquid argon TPC.

## Why Targetry?

- **Targetry** = the task of producing and capturing  $\pi$ 's and  $\mu$ 's from proton interactions with a nuclear target.

- At a **muon collider** the key parameter is **luminosity**:

$$\mathcal{L} = \frac{N_1 N_2 f}{A} \text{ s}^{-1} \text{ cm}^{-2},$$

⇒ Gain as square of source strength (targetry),  
but small beam area (cooling) is also critical.

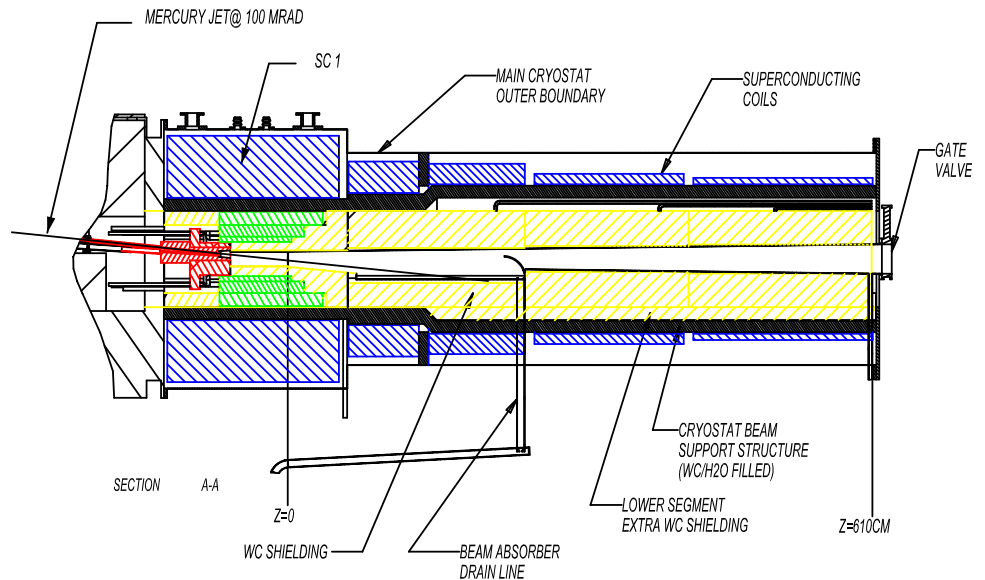
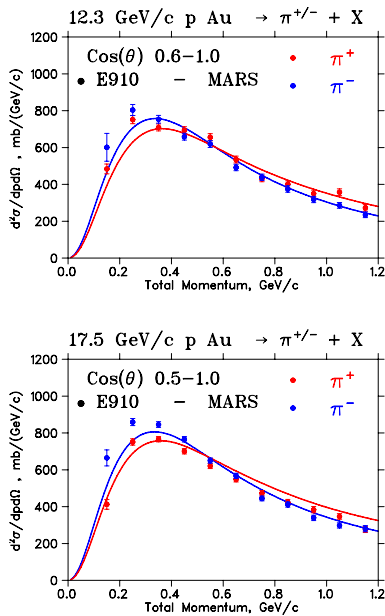
- At a **neutrino factory** the key parameter is **neutrino flux**,  
⇒ Source strength (targetry) is of pre-eminent concern.

[Beam cooling important mainly to be sure the beam fits in the pipe.]

- Since its inception the Neutrino Factory/Muon Collider Collaboration has recognized the importance of high performance targetry, and has dedicated considerable resources towards R&D on advanced targetry concepts.
- The exciting results from atmospheric and reactor neutrino programs (Super-K, SNO, KamLAND) reinforce the opportunity for neutrino physics with intense accelerator neutrino beams, where **targetry is the major challenge**.

## Targetry Challenges

- Use of a multimegawatt proton beam for maximal production of soft pions → muons.
- Capture pions in a 20-T solenoid, followed by a 1.25-T decay channel (with beam and target tilted by 100 mrad w.r.t. magnetic axis).



- A carbon target is feasible for 1.5-MW proton beam power.
- For  $E_p \gtrsim 16$  GeV, factor of 2 advantage with high- $Z$  target.
- Static high- $Z$  target would melt, ⇒ Moving target.
- A free mercury jet target is feasible for beam power of 4 MW (and more).

## Thermal Shock

When beam pulse length  $t$  is less than target radius  $r$  divided by speed of sound  $v_{\text{sound}}$ , beam-induced pressure waves (thermal shock) are a major issue.

Simple model: if  $U$  = beam energy deposition in, say, Joules/g, then the instantaneous temperature rise  $\Delta T$  is given by

$$\Delta T = \frac{U}{C},$$

where  $C$  = heat capacity in Joules/g/K.

The temperature rise leads to a strain  $\Delta r/r$  given by

$$\frac{\Delta r}{r} = \alpha \Delta T = \frac{\alpha U}{C},$$

where  $\alpha$  = thermal expansion coefficient.

The strain leads to a stress  $P$  (= force/area) given by

$$P = E \frac{\Delta r}{r} = \frac{E \alpha U}{C},$$

where  $E$  is the modulus of elasticity.

In many metals, the tensile strength obeys  $P \approx 0.002E$ ,  $\alpha \approx 10^{-5}$ , and  $C \approx 0.3$  J/g/K, in which case

$$U_{\text{max}} \approx \frac{PC}{E\alpha} \approx \frac{0.002 \cdot 0.3}{10^{-5}} \approx 60 \text{ J / g.}$$

## How Much Beam Power Can a Solid Target Stand?

How many protons are required to deposit 60 J/g in a material?  
What is the maximum beam power this material can withstand without cracking, for a 10-GeV beam at 10 Hz with area 0.1 cm<sup>2</sup>.

Ans. If we ignore “showers” in the material, we still have  $dE/dx$  ionization loss, of about 1.5 MeV/g/cm<sup>2</sup>.

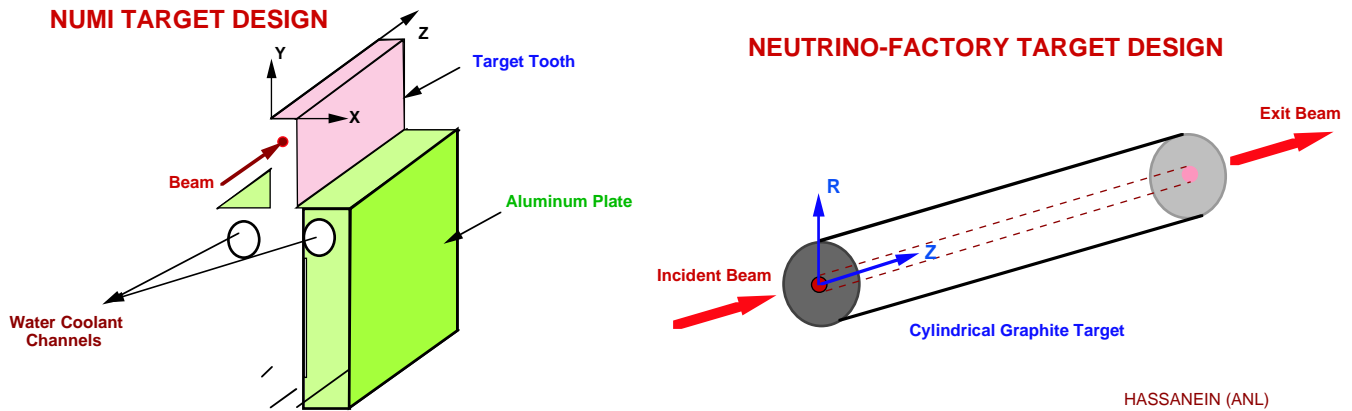
Now, 1 MeV =  $1.6 \times 10^{-13}$  J, so 60 J/g requires a proton beam intensity of  $60/(1.6 \times 10^{-13}) = 10^{15}/\text{cm}^2$ .

Then,  $P_{\text{max}} \approx 10 \text{ Hz} \cdot 10^{10} \text{ eV} \cdot 1.6 \times 10^{-19} \text{ J/eV} \cdot 10^{15}/\text{cm}^2 \cdot 0.1 \text{ cm}^2$   
 $\approx 1.6 \times 10^6 \text{ J/s} = 1.6 \text{ MW}$ .

**Solid targets are viable up to about 1.5 MW beam power!**

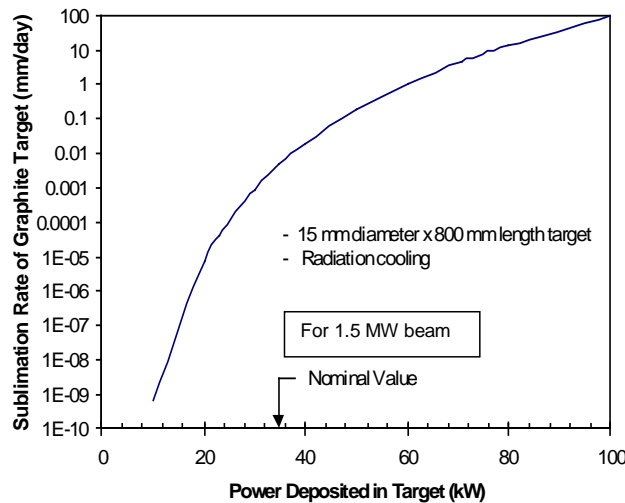


# A Carbon Target is Feasible at 1-MW Beam Power



A carbon-carbon composite with near-zero thermal expansion is largely immune to beam-induced pressure waves.

A carbon target in vacuum sublimates away in 1 day at 4 MW.

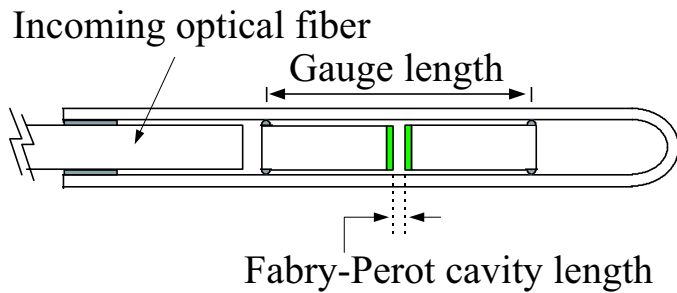


Sublimation of carbon is negligible in a helium atmosphere. (P. Thieberger) Tests underway at ORNL to confirm this.

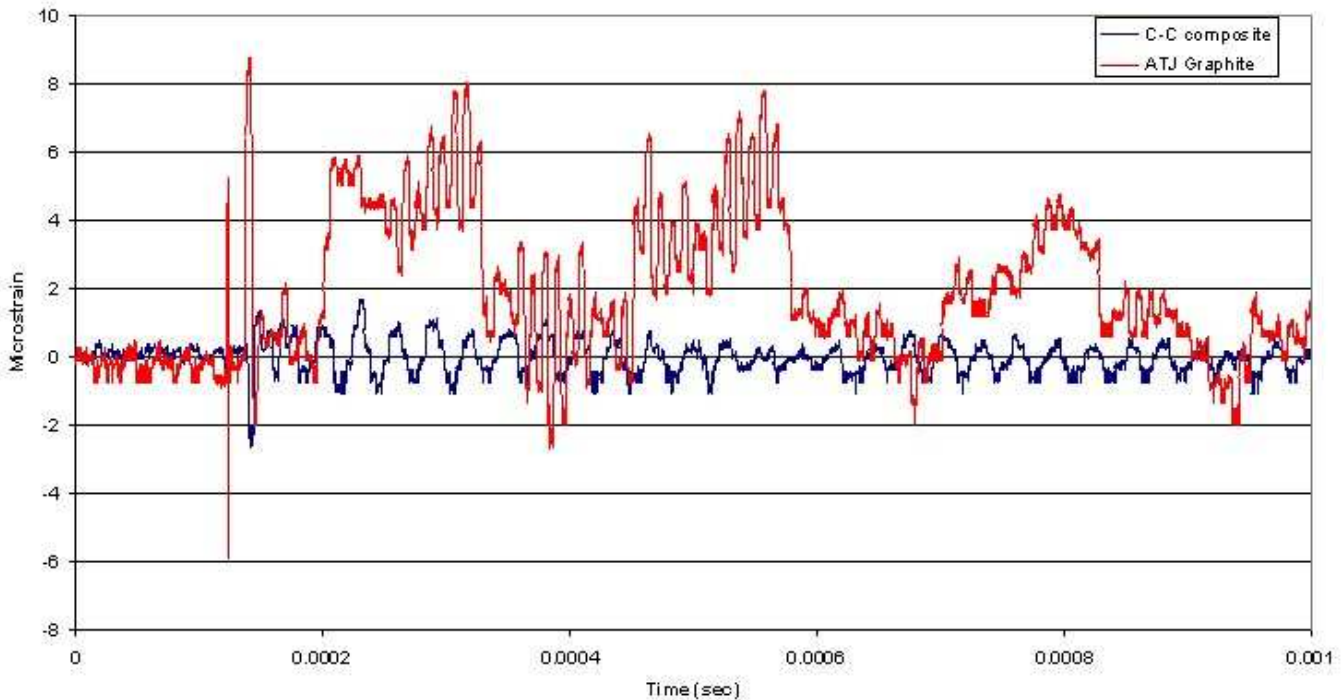
Radiation damage is limiting factor:  $\approx 12$  weeks at 1 MW.

# Lower Thermal Shock If Lower Thermal Expansion Coefficient

Proton beams studies of ATJ graphite and a 3-d weave of carbon-carbon fibers, instrumented with fiberoptic strain sensors:

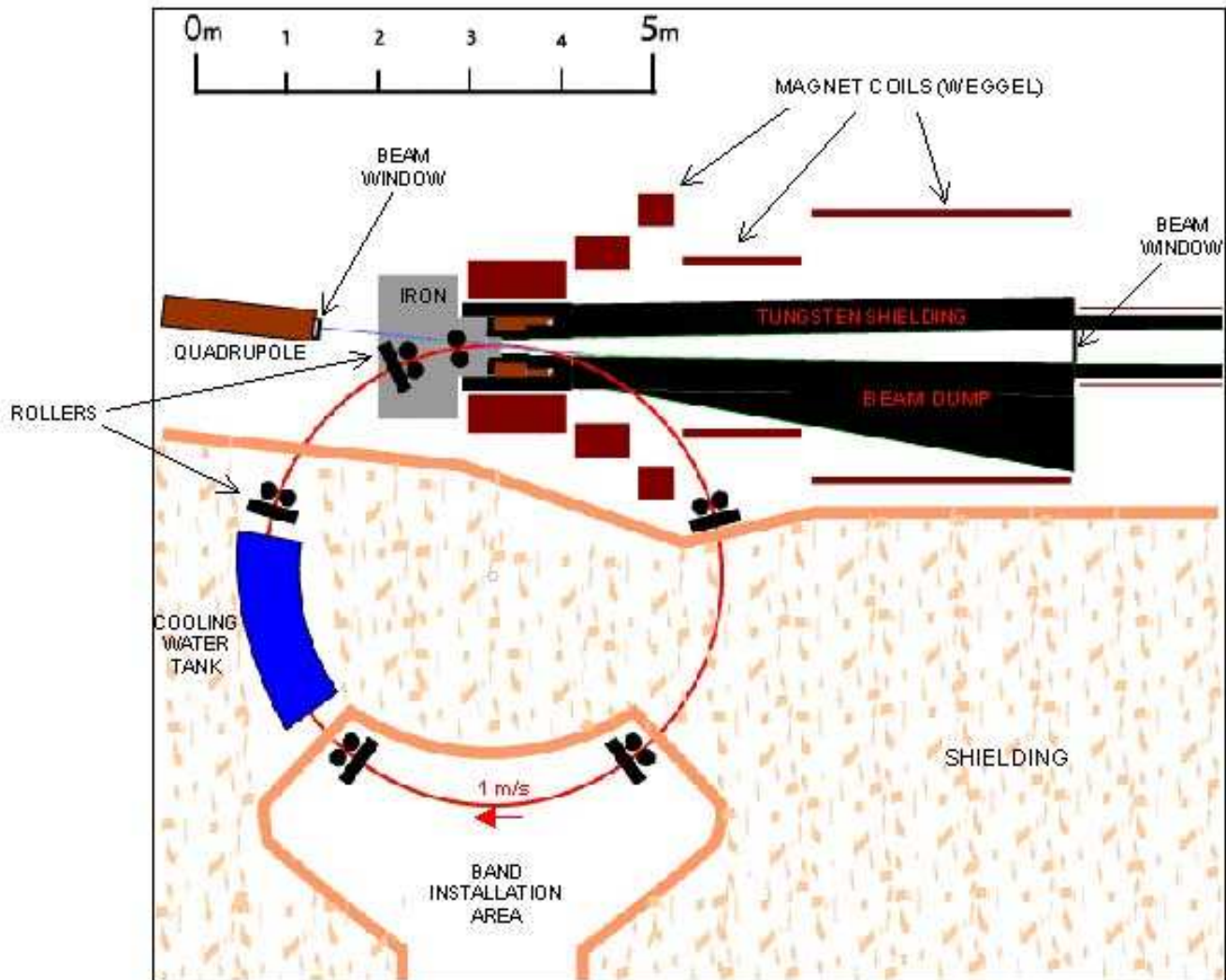


**BNL E951 Target Experiment**  
**24 GeV 3.0 e12 proton pulse on Carbon-Carbon and ATJ graphite targets**  
**Recorded strain induced by proton pulse**



## Maybe Can Use a Moving Solid Target

Ex. Rotating band that increases radiation damage life by 1000:

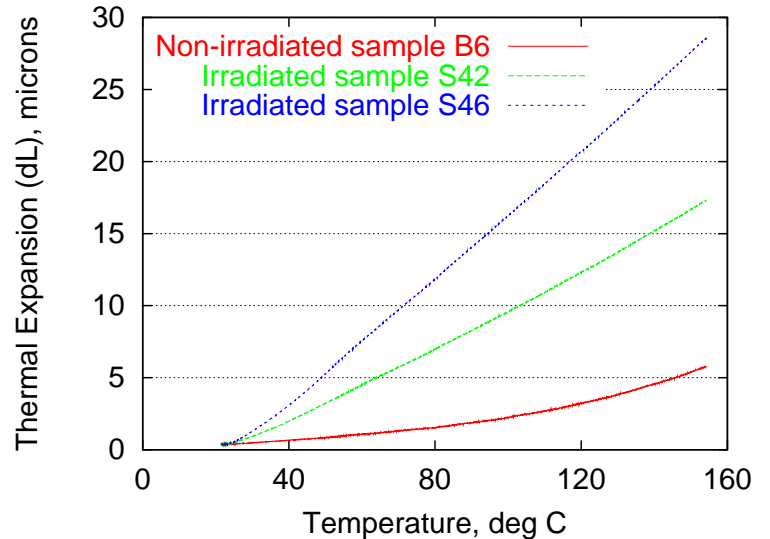


Compatibility of the rotating band with a capture solenoid magnet?

Single-pulse thermal shock still an issue, so maybe use SuperInvar, a material with a very low thermal expansion coefficient.

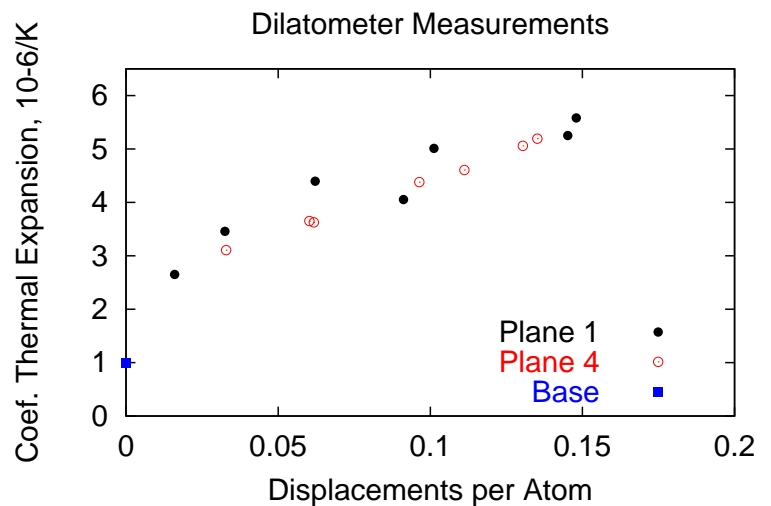
## Effects of Radiation on SuperInvar

SuperInvar has a very low coefficient of thermal expansion (CTA),  
 ⇒ Resistant to “thermal shock” of a proton beam.



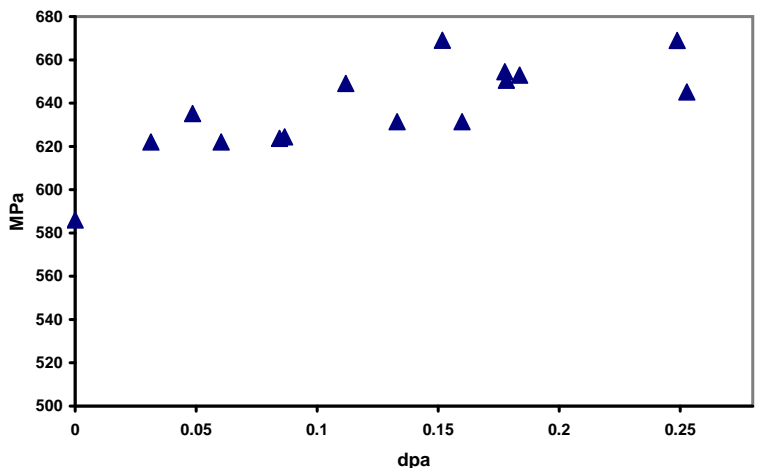
However, irradiation at the BNL BLIP facility show that the CTA increases rapidly with radiation dose.

CTA *vs.* dose ⇒



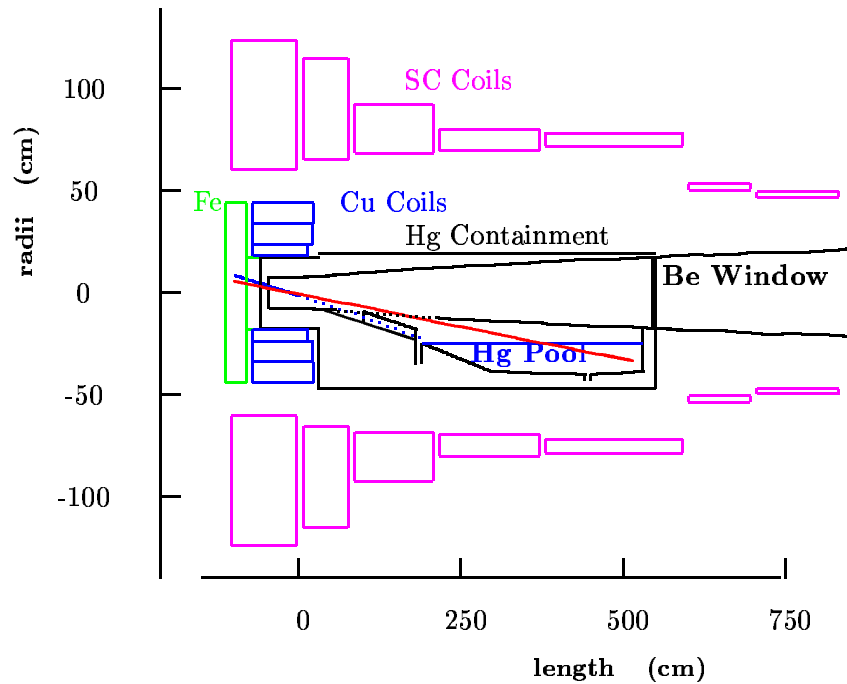
SuperInvar is made stronger by moderate radiation doses (like many materials).

Yield strength *vs.* dose ⇒

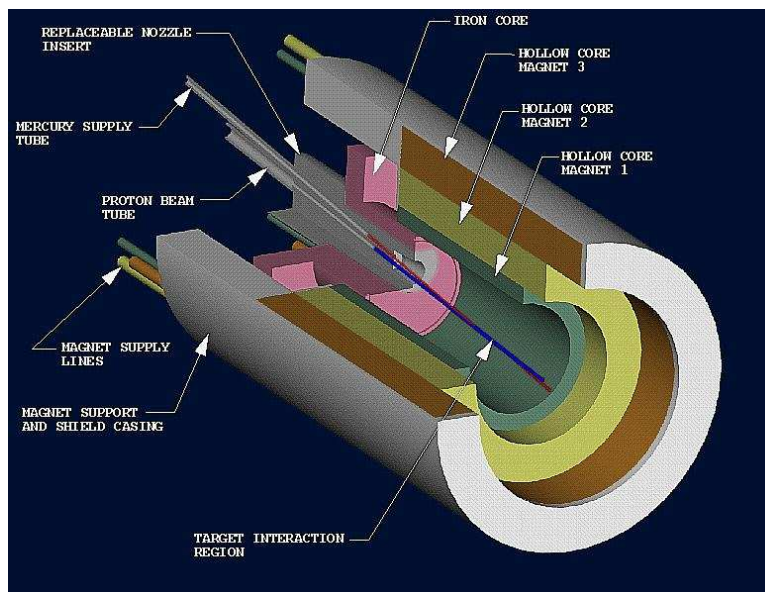


# A Liquid Metal Jet May Be the Best Moving Target

Mercury jet target inside a magnetic bottle: 20-T around target, dropping to 1.25 T in the pion decay channel.

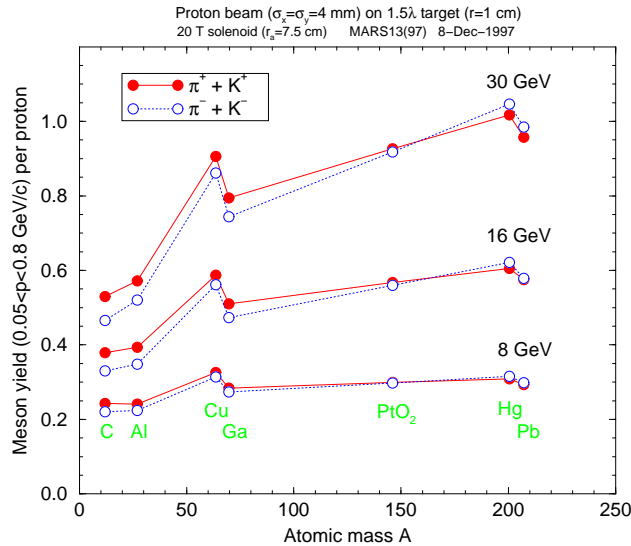


Mercury jet tilted by 100 mrad, proton beam by 67 mrad.

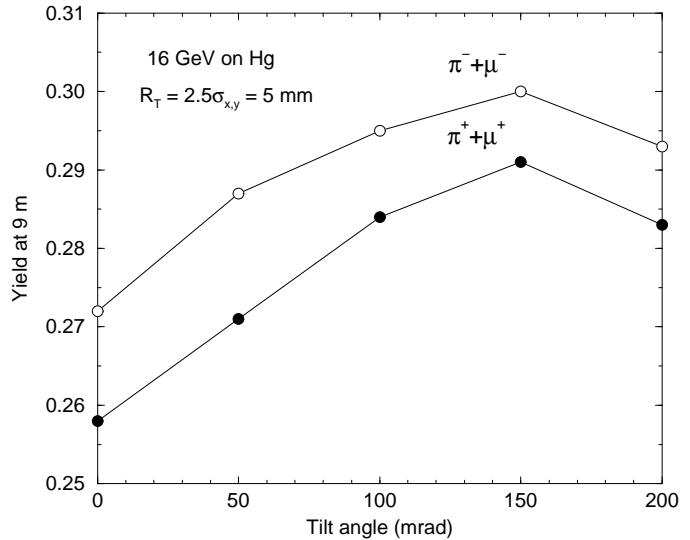
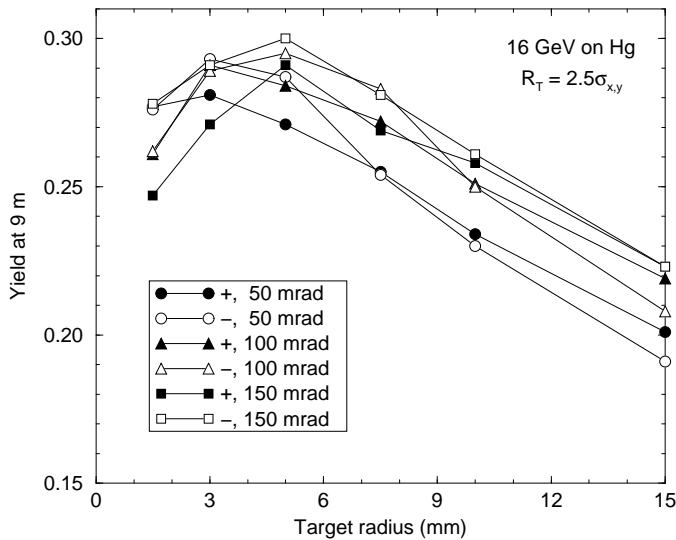


## Pion/Muon Yield

For  $E_p \gtrsim 10$  GeV, more yield with high- $Z$  target.



Mercury target radius should be  $\approx 5$  mm,  
 with target axis tilted by  $\approx 100$  mrad to the magnetic axis.

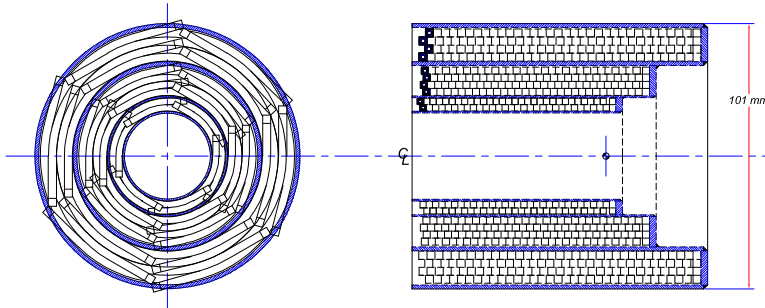


Can capture  $\approx 0.3$  pion per proton with  $50 < P_\pi < 400$  MeV/ $c$ .



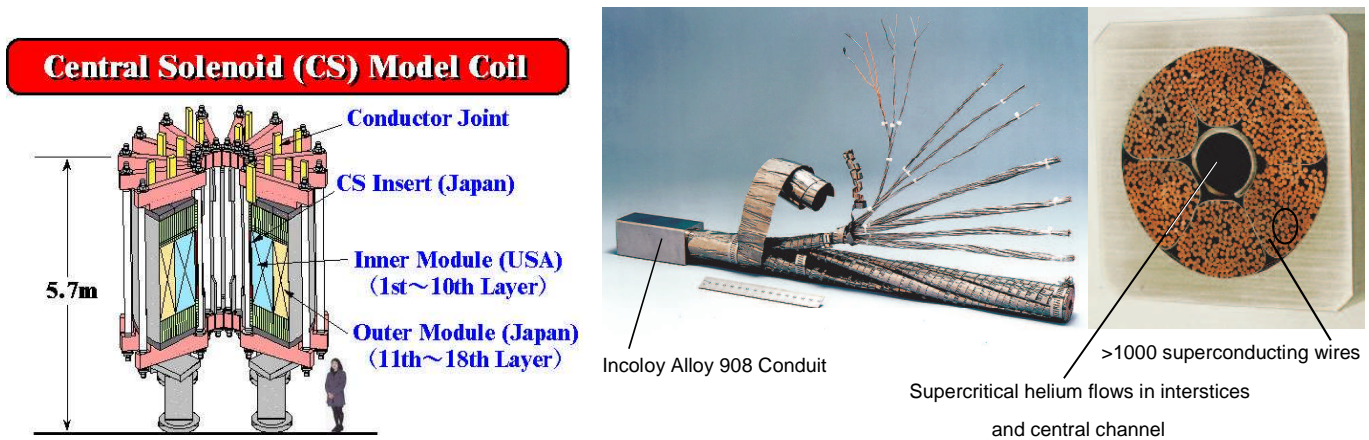
## 20-T Capture Magnet System

Inner, hollow-conductor copper coils generate 6 T @ 12 MW:



Bitter-coil option less costly, but marginally feasible.

Outer, superconducting coils generate 14 T @ 600 MJ:

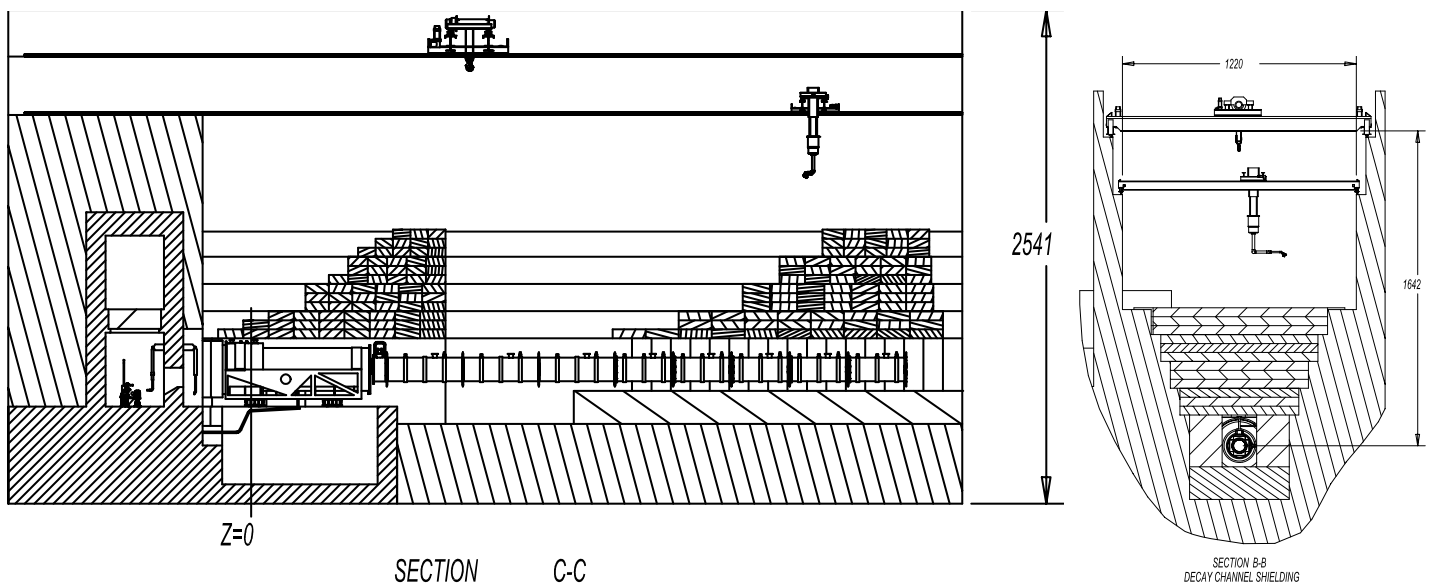
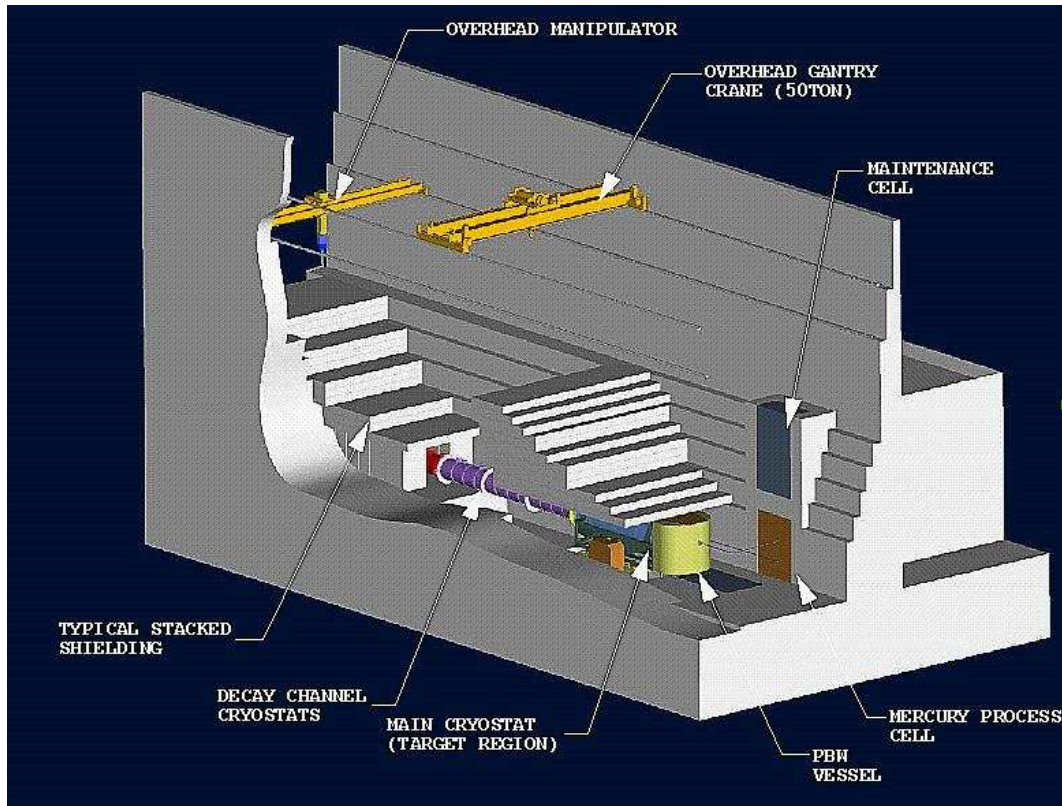


Cable-in-conduit construction similar to ITER central solenoid.

Both coils shielded by tungsten-carbide/water.

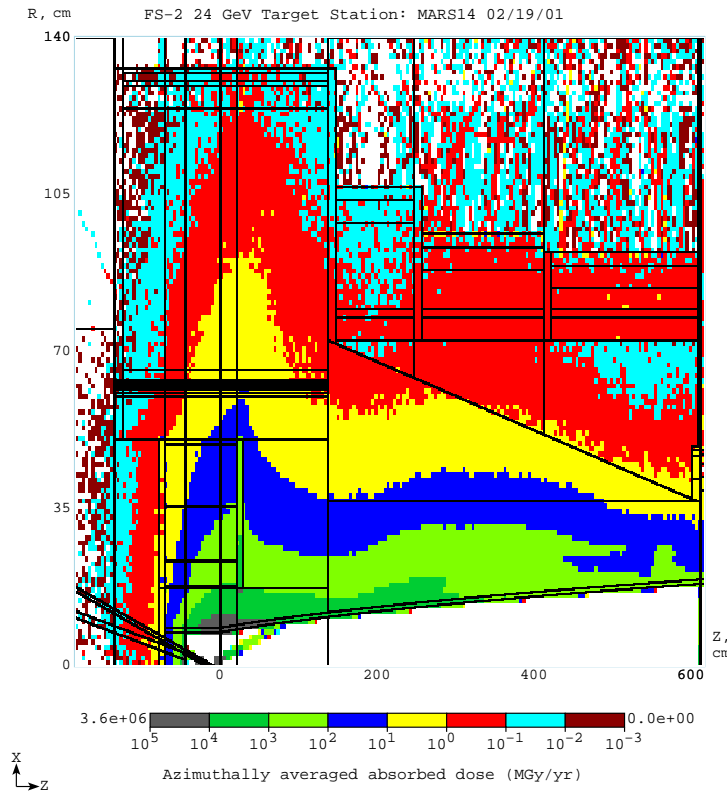
# Target System Support Facility

Extensive shielding; remote handling capability.





# Lifetime of Components in the High Radiation Environment

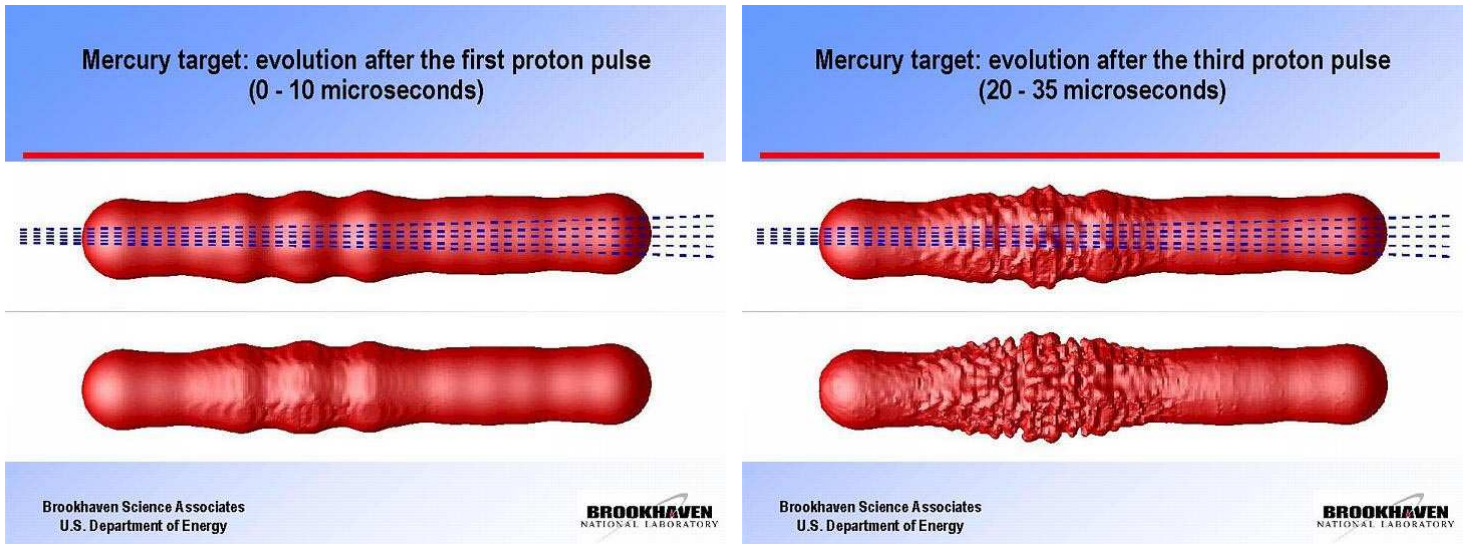


Component	Radius (cm)	Dose/yr (Grays/ $2 \times 10^7$ s)	Max allowed Dose (Grays)	1 MW Life (years)	4 MW life (years)
Inner shielding	7.5	$5 \times 10^{10}$	$10^{12}$	20	5
Hg containment	18	$10^9$	$10^{11}$	100	25
Hollow conductor coil	18	$10^9$	$10^{11}$	100	25
Superconducting coil	65	$5 \times 10^6$	$10^8$	20	5

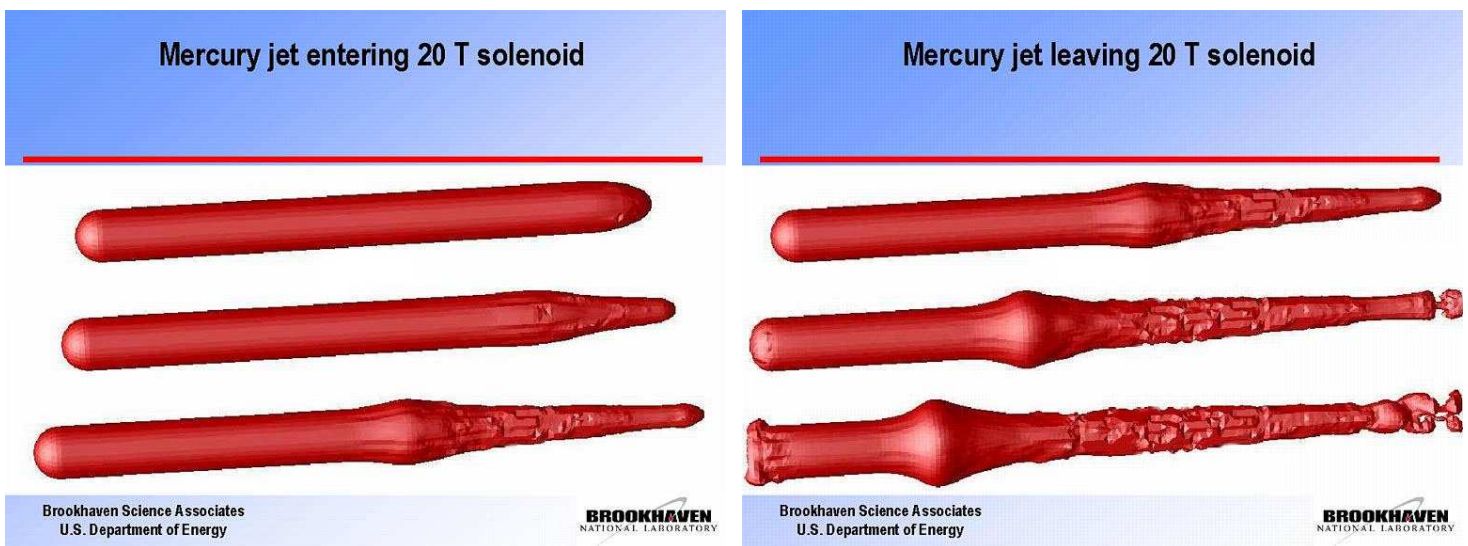
Some components must be replaceable.

# Viability of Targetry and Capture For a Single Pulse

- Beam energy deposition may disperse the jet.



- Eddy currents may distort the jet as it traverses the magnet.



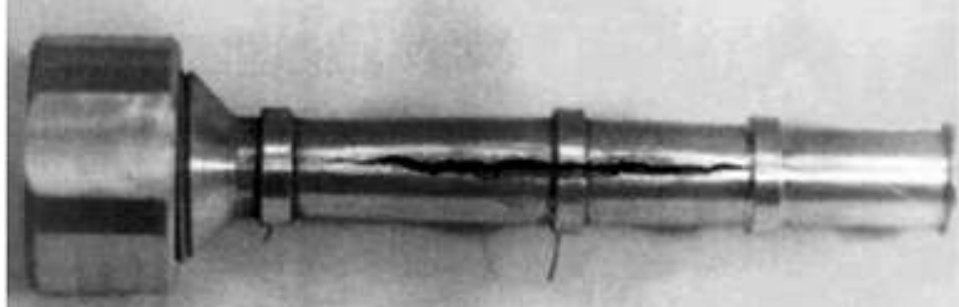
- Computational challenge: to include negative pressure and cavitation in a magnetohydrodynamic (MHD) simulation of a liquid metal with a free surface.

Beam-Induced Cavitation in Liquids Can Break Pipes

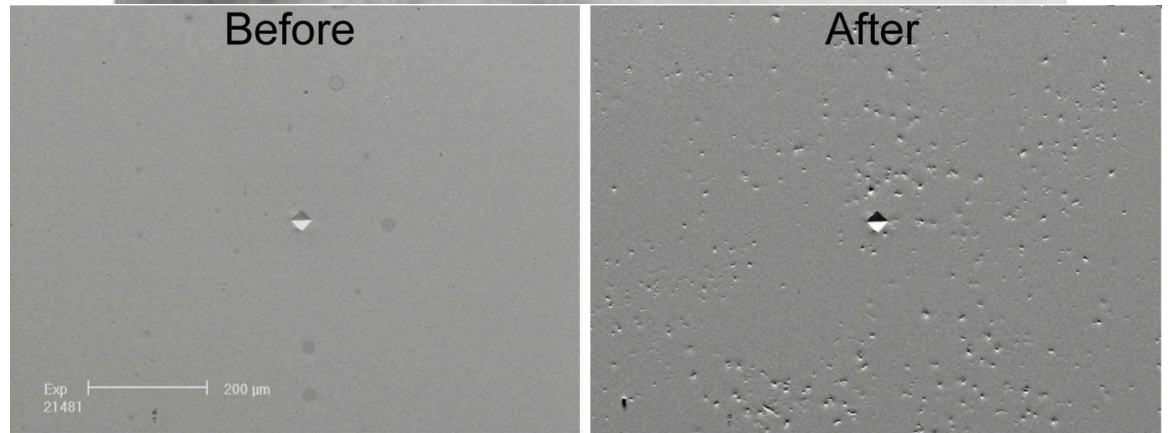
ISOLDE:



BINP:



SNS:

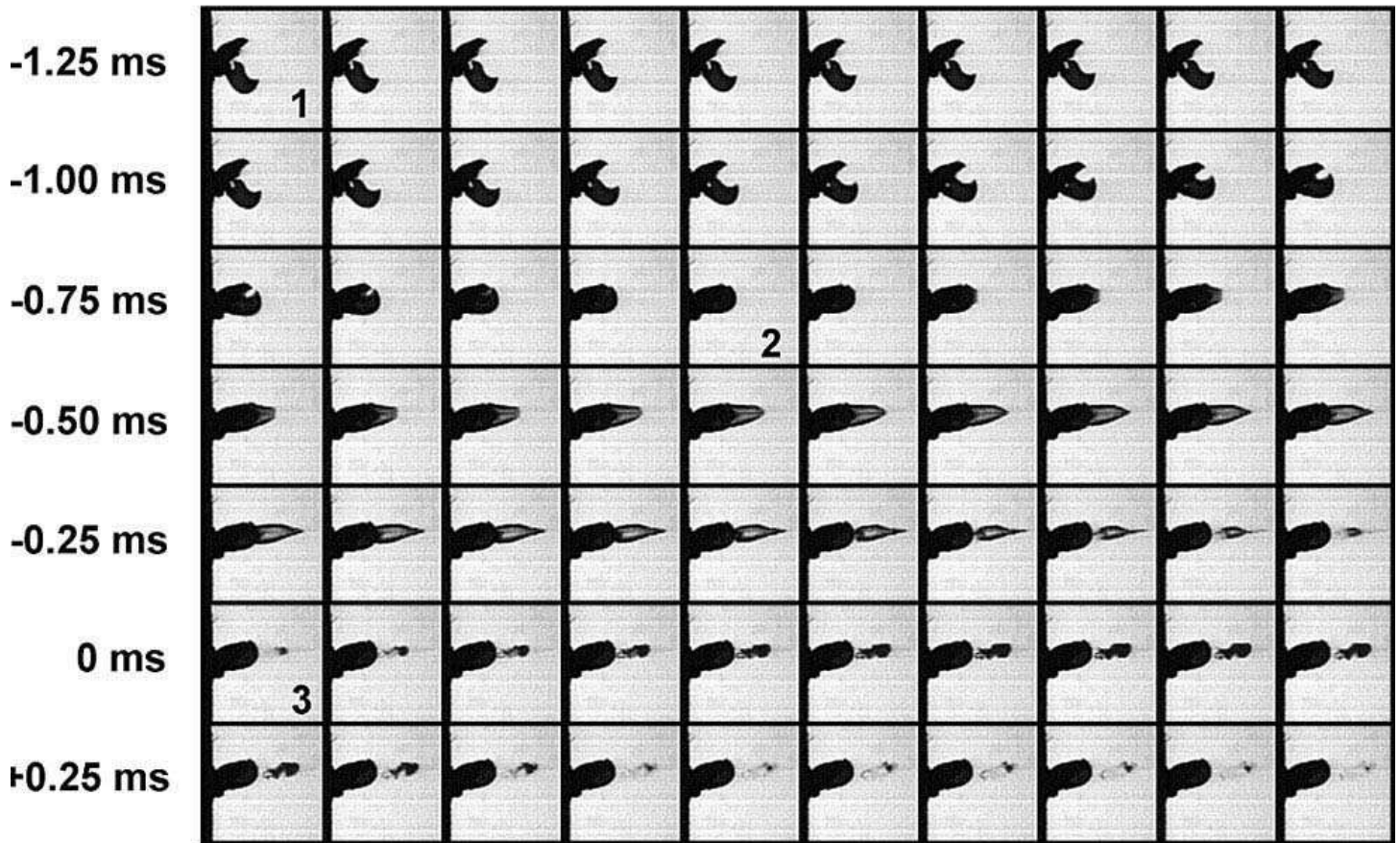
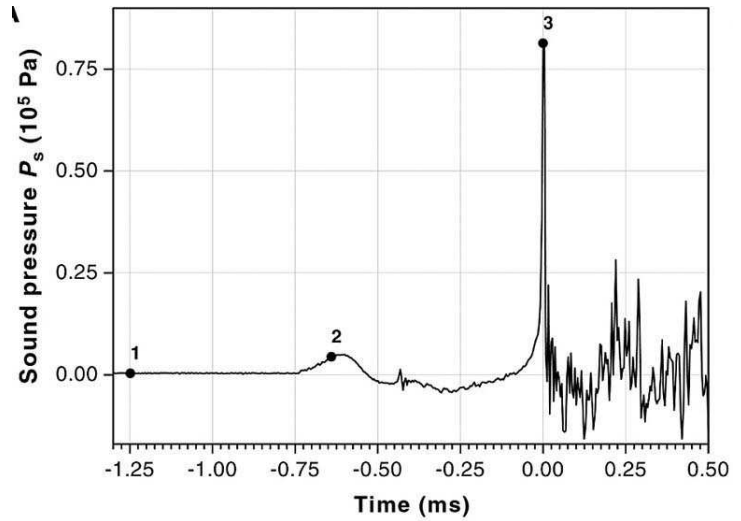
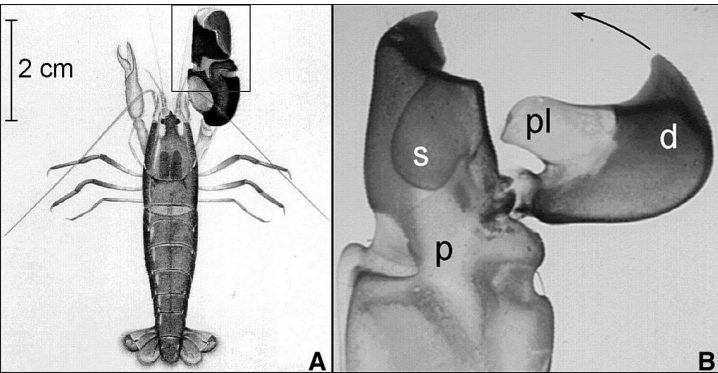


TL - High Power Target
Specimen # 29754
Equivalent SNS Power Level = 2.5



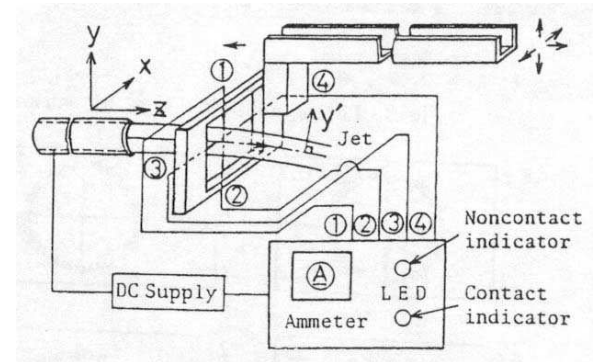
# How Snapping Shrimp Snap: Through Cavitating Bubbles

M. Versluis, Science **289**, 2114 (2000).



2 cm

The Shape of a Liquid Metal Jet under a Non-uniform Magnetic Field



S. Oshima *et al.*, JSME Int. J. **30**, 437 (1987).

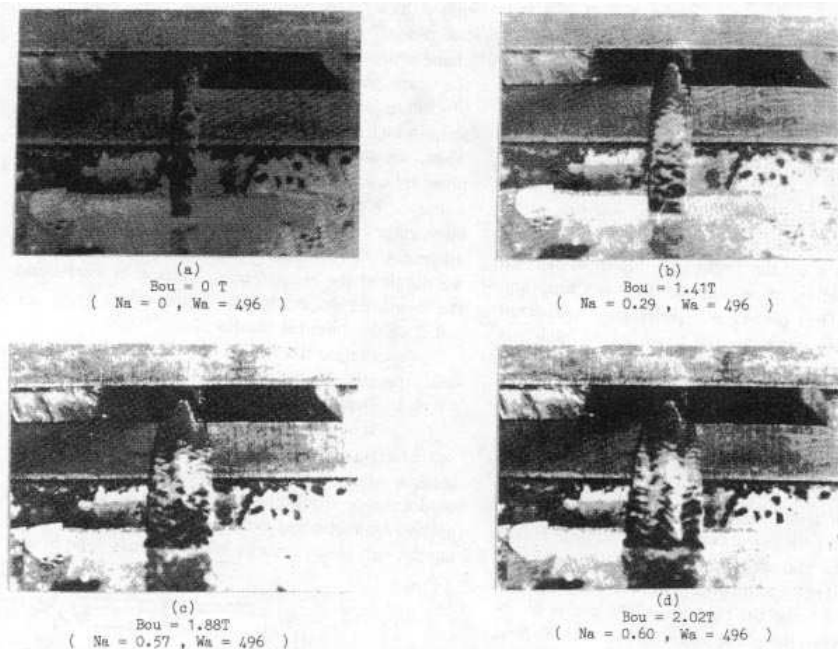


Fig. 9 Photographs of the jet for various applied magnetic field strengths

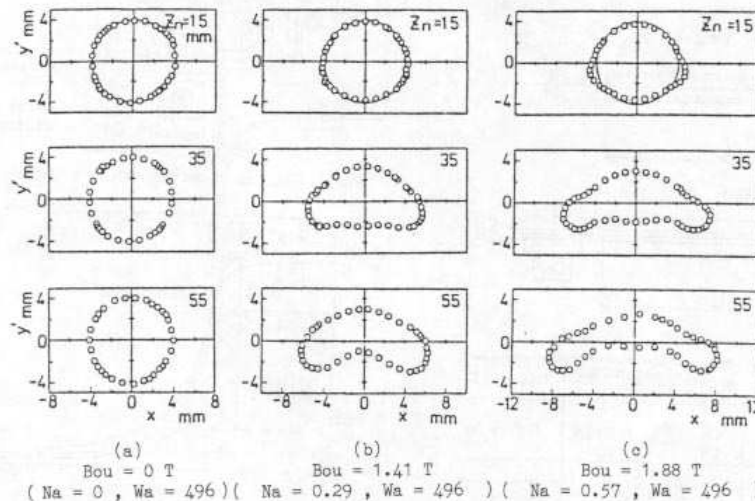
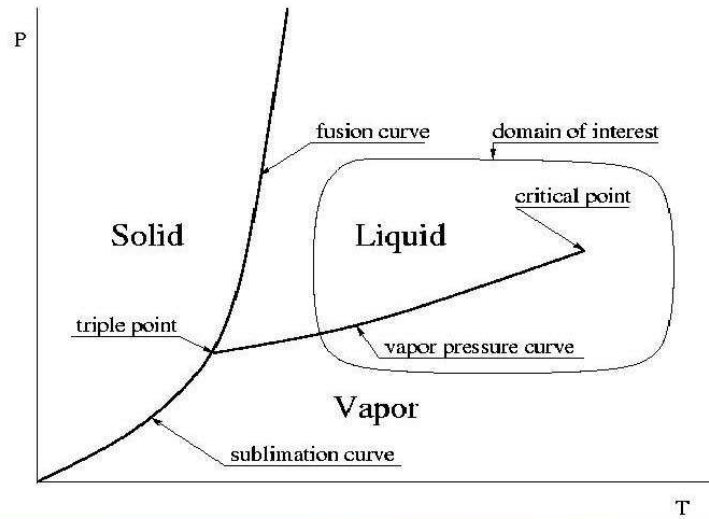


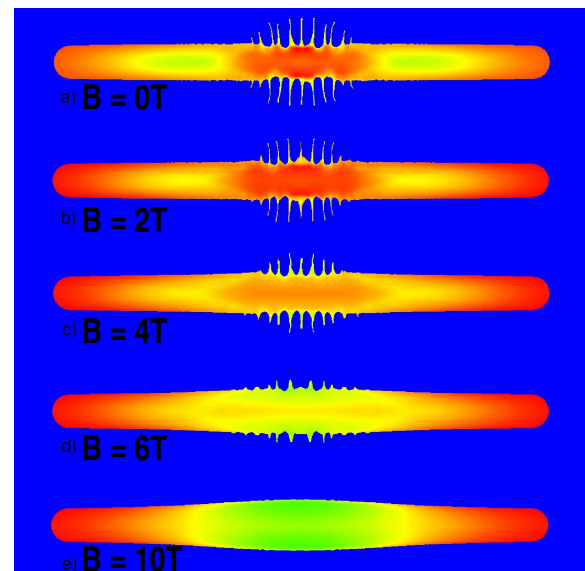
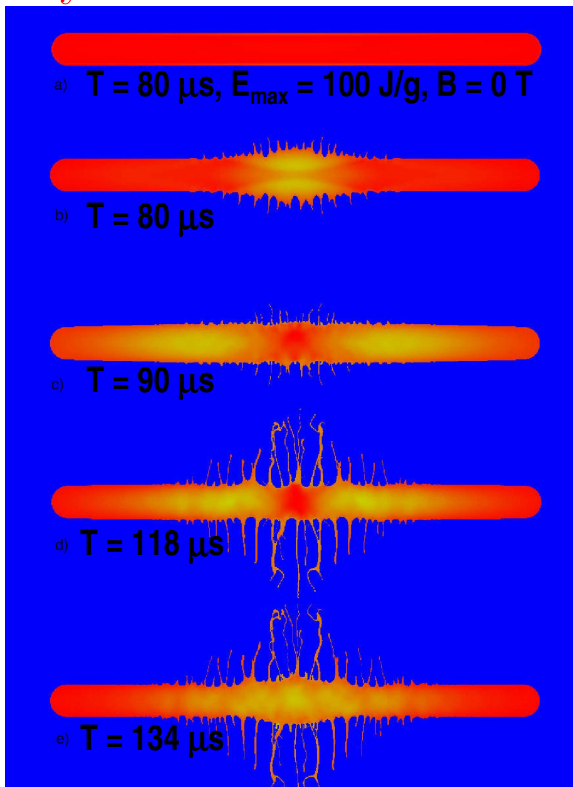
Fig. 10 Cross-sectional shape of the jet obtained by spot a electrode probe

# Computational Magnetohydrodynamics (R. Samulyak)



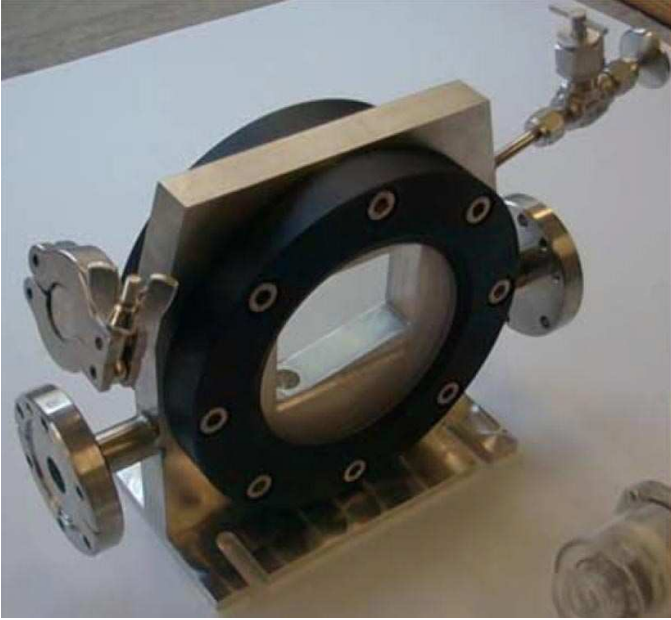
Critical point :  $T_c = 1750\text{K}$ ,  $P_c = 172\text{MPa}$ ,  $V_c = 43\text{cm}^3\text{mol}^{-1}$   
 Boiling point :  $T_b = 629.84\text{K}$ ,  $P_b = 0.1\text{MPa}$ ,  $\rho = 13.546\text{g}\cdot\text{cm}^{-3}$

Need an equation of state that supports negative pressures, but gives way to cavitation.

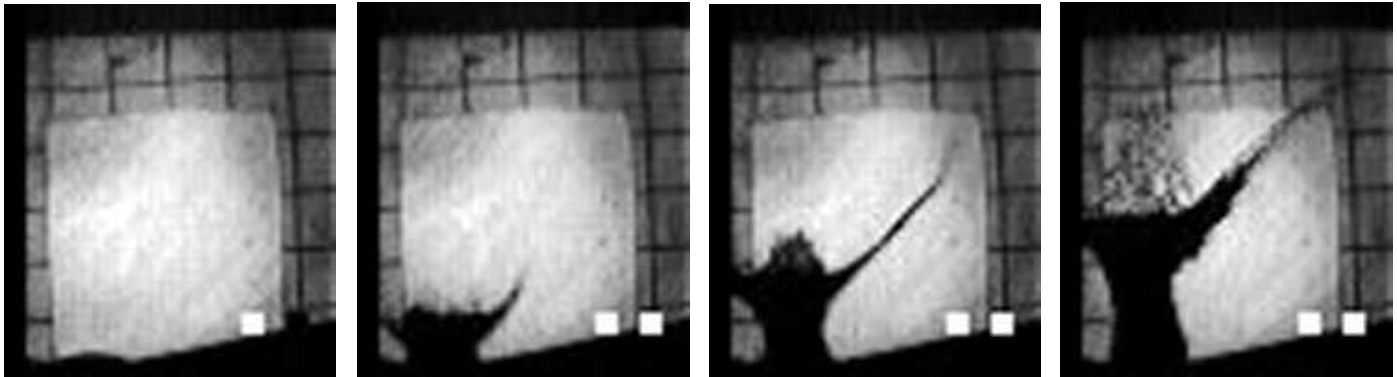




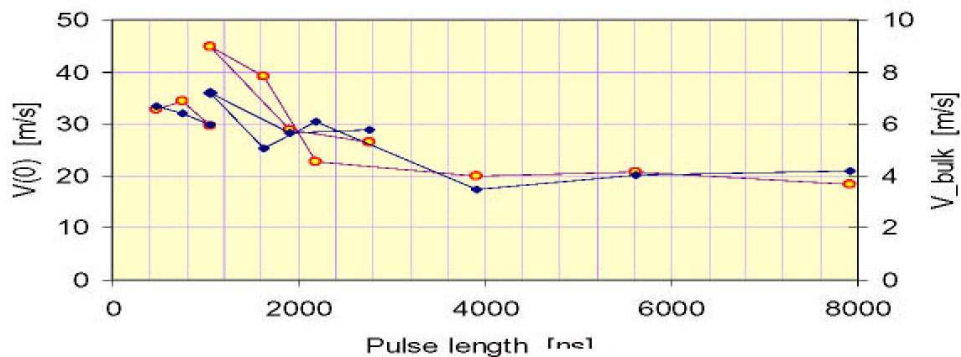
## Passive Mercury Target Tests



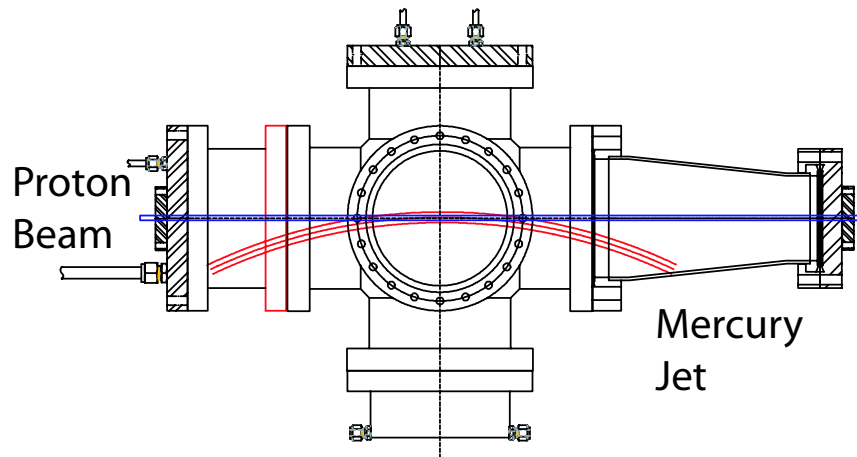
Exposures of  $25 \mu\text{s}$  at  
 $t = 0, 0.5, 1.6, 3.4 \text{ msec}$ ,  
 $\Rightarrow v_{\text{splash}} \approx 20 - 40 \text{ m/s}$ :



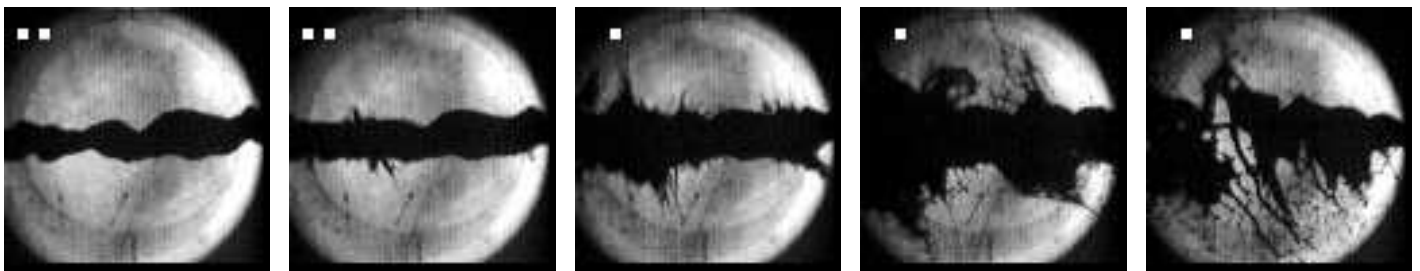
Two pulses of  $\approx 250 \text{ ns}$  give larger dispersal velocity only if separated by less than  $3 \mu\text{s}$ .



## Studies of Proton Beam + Mercury Jet



1-cm-diameter Hg jet in  $2 \times 10^{12}$  protons at  $t = 0, 0.75, 2, 7, 18$  ms.



$$\text{Model: } v_{\text{dispersal}} = \frac{\Delta r}{\Delta t} = \frac{r \alpha \Delta T}{r/v_{\text{sound}}} = \frac{\alpha U}{C} v_{\text{sound}} \approx 50 \text{ m/s}$$

for  $U \approx 100 \text{ J/g}$ .

Data:  $v_{\text{dispersal}} \approx 10 \text{ m/s}$  for  $U \approx 25 \text{ J/g}$ .

$v_{\text{dispersal}}$  appears to scale with proton intensity.

**The dispersal is not destructive.**

Filaments appear only  $\approx 40 \mu\text{s}$  after beam,  $\Rightarrow$  after several bounces of waves, or  $v_{\text{sound}}$  very low.

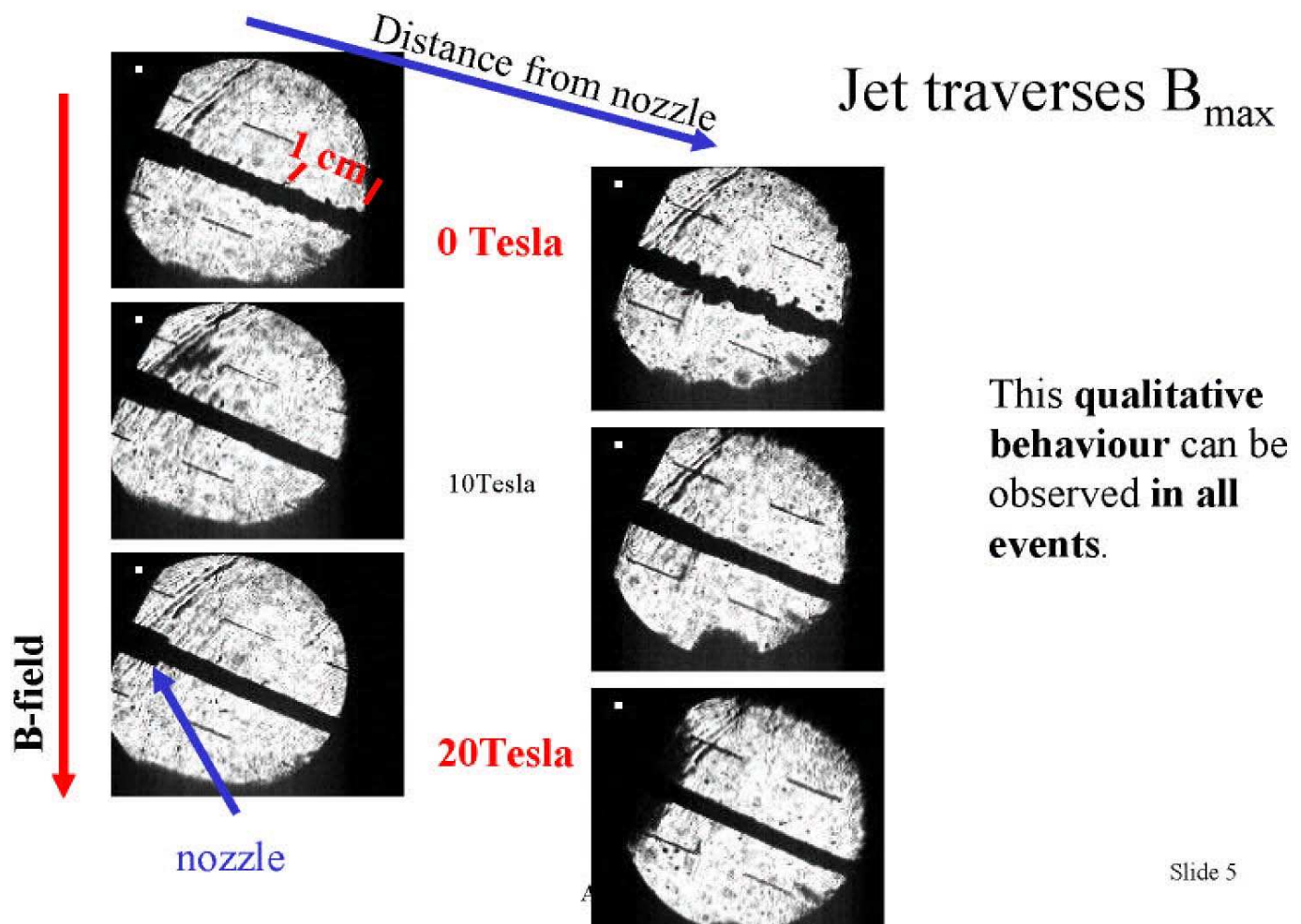


# Tests of a Mercury Jet in a 20-T Magnetic Field (CERN/Grenoble, A. Fabich, Ph.D. Thesis)

Eddy currents may distort the jet as it traverses the magnet.

Analytic model suggests little effect if jet nozzle inside field.

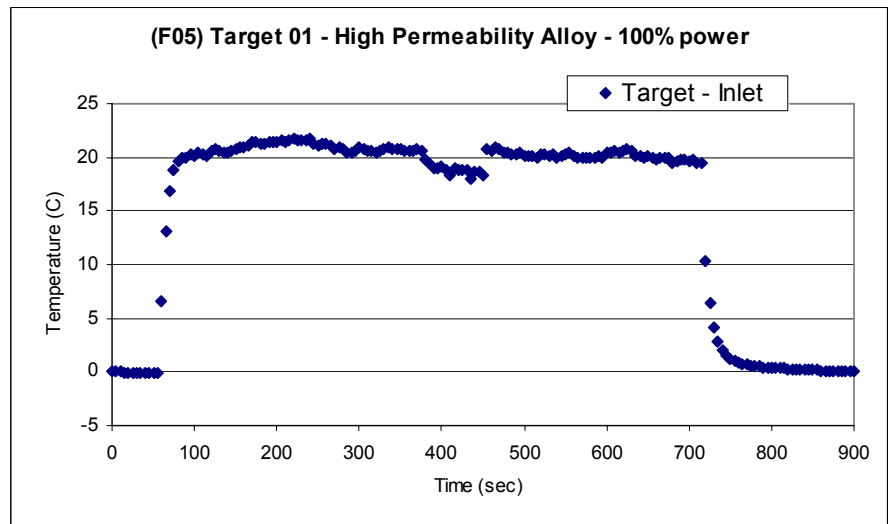
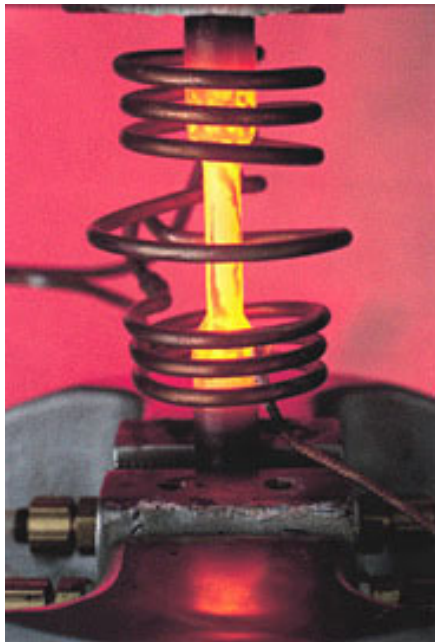
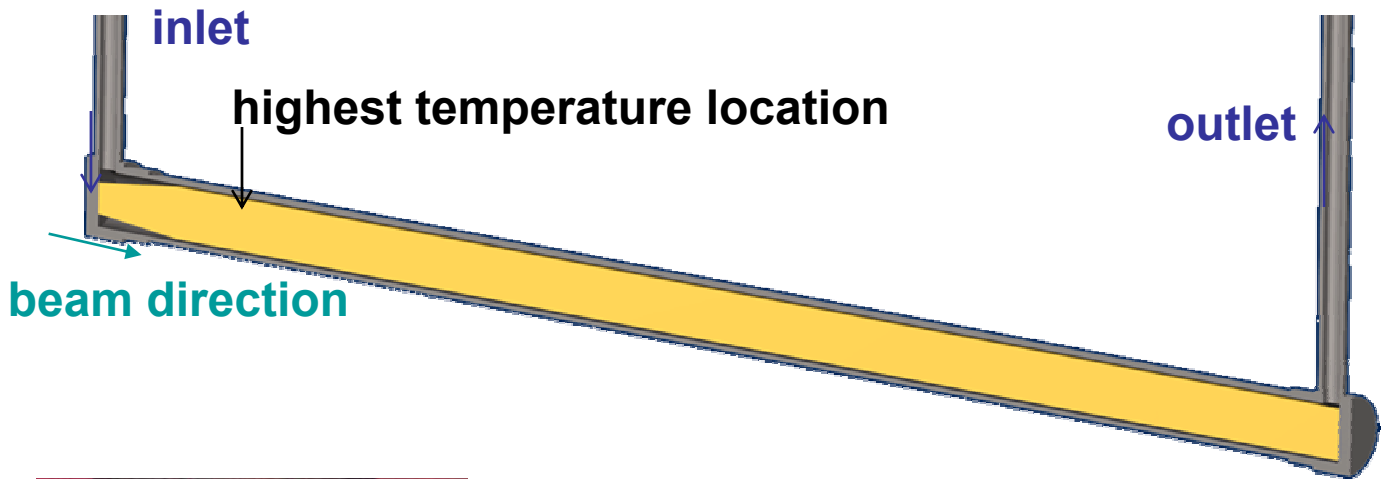
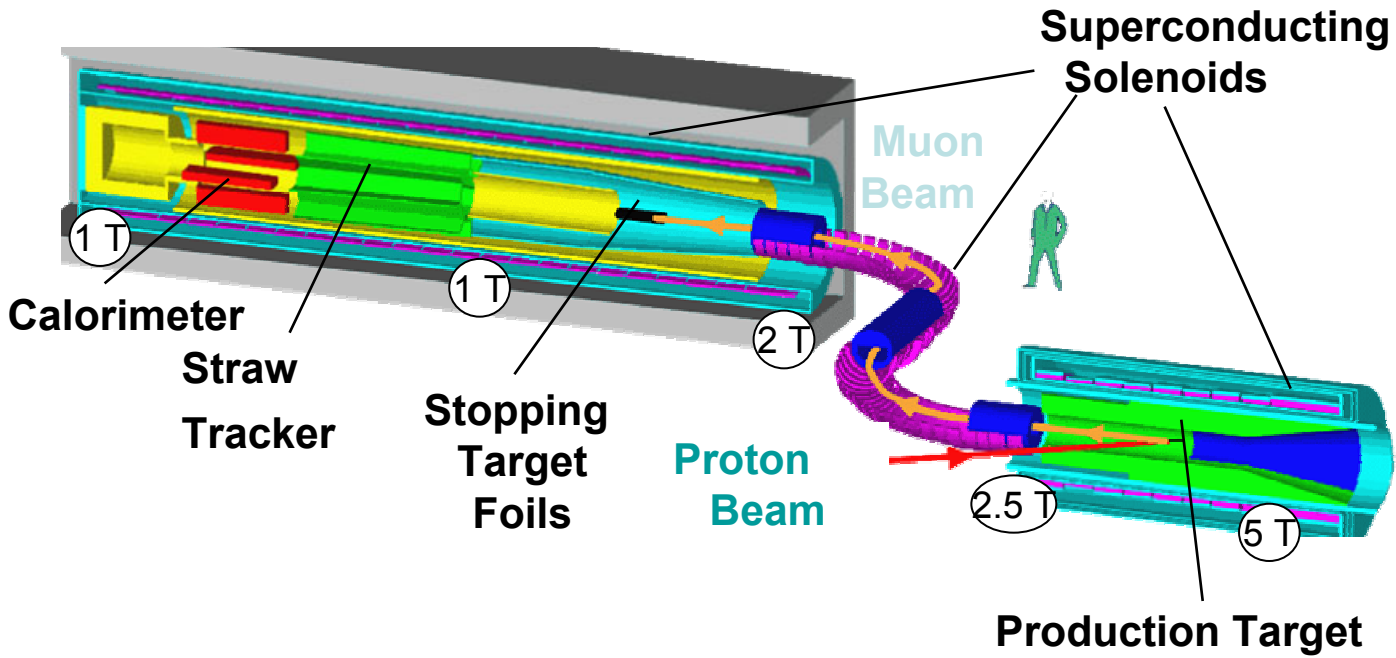
4 mm diam. jet,  $v \approx 12$  m/s,  $B = 0, 10, 20$  T.



⇒ Damping of surface tension waves (Rayleigh instability).

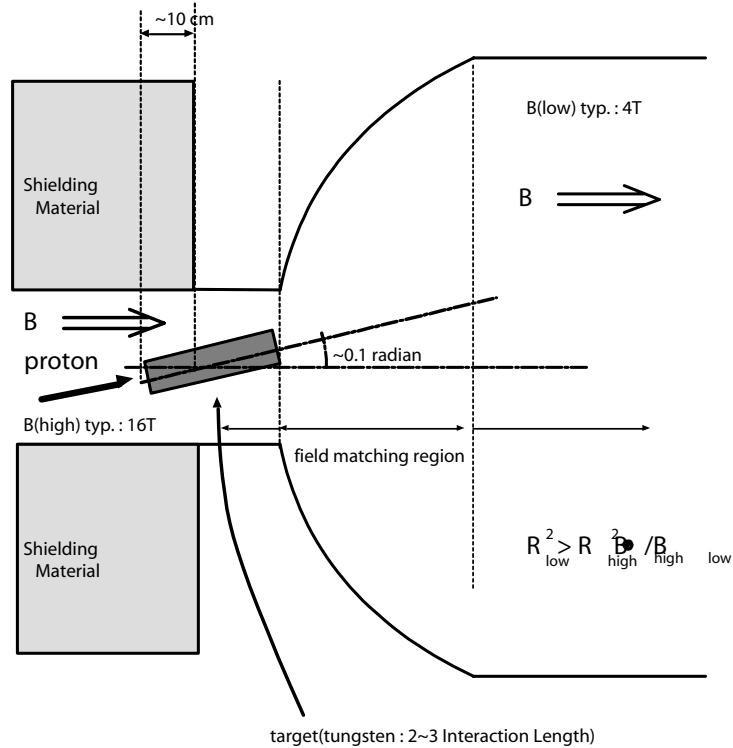
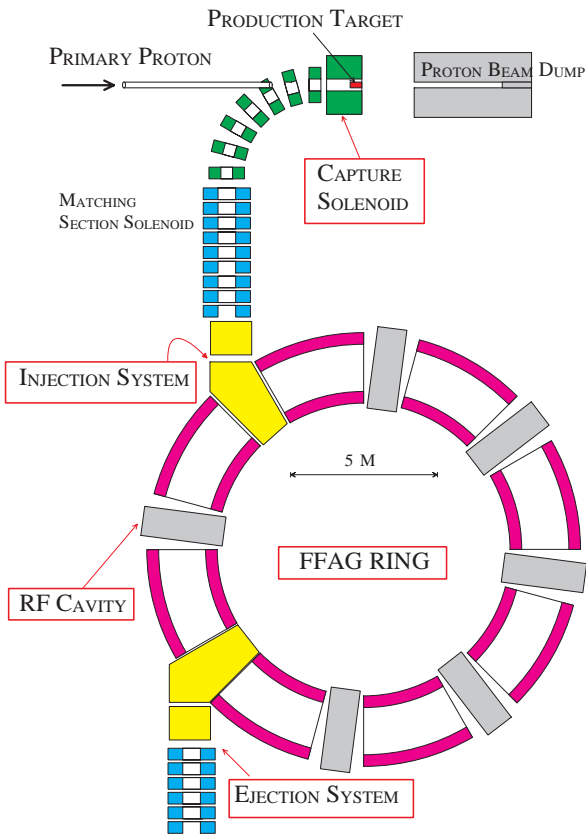
Will the beam-induced dispersal be damped also?

# MECO Target R&D, *J. Popp*



# PRISM Target R&D

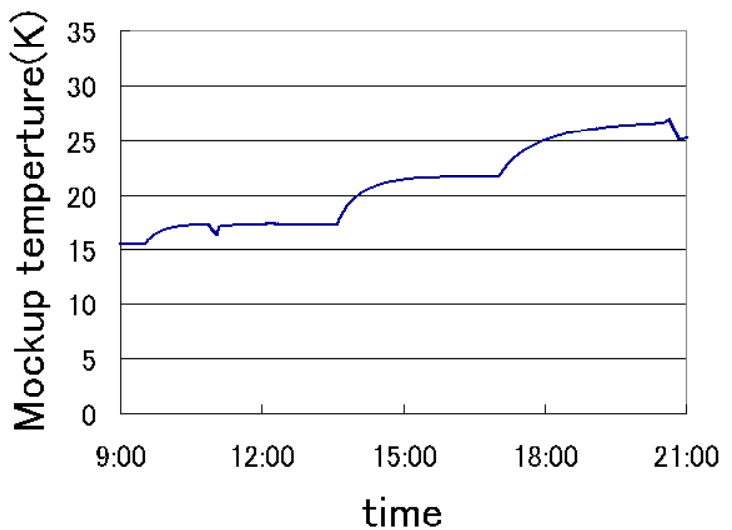
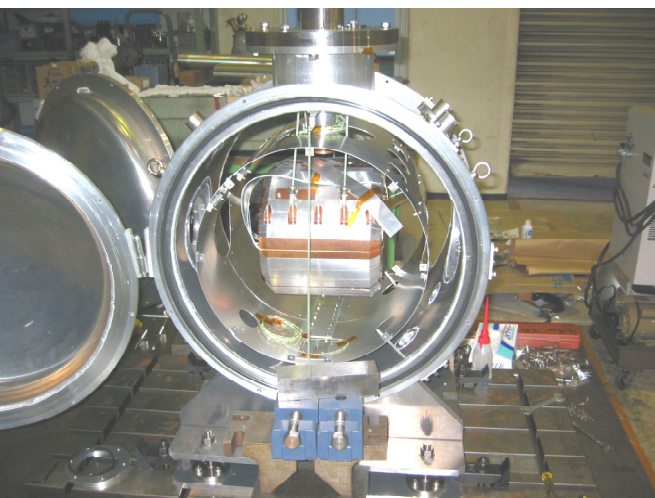
H. Ohnishi, Y. Yamanoi, K. Yoshimura



Target concept similar to Neutrino Factory Study 2.

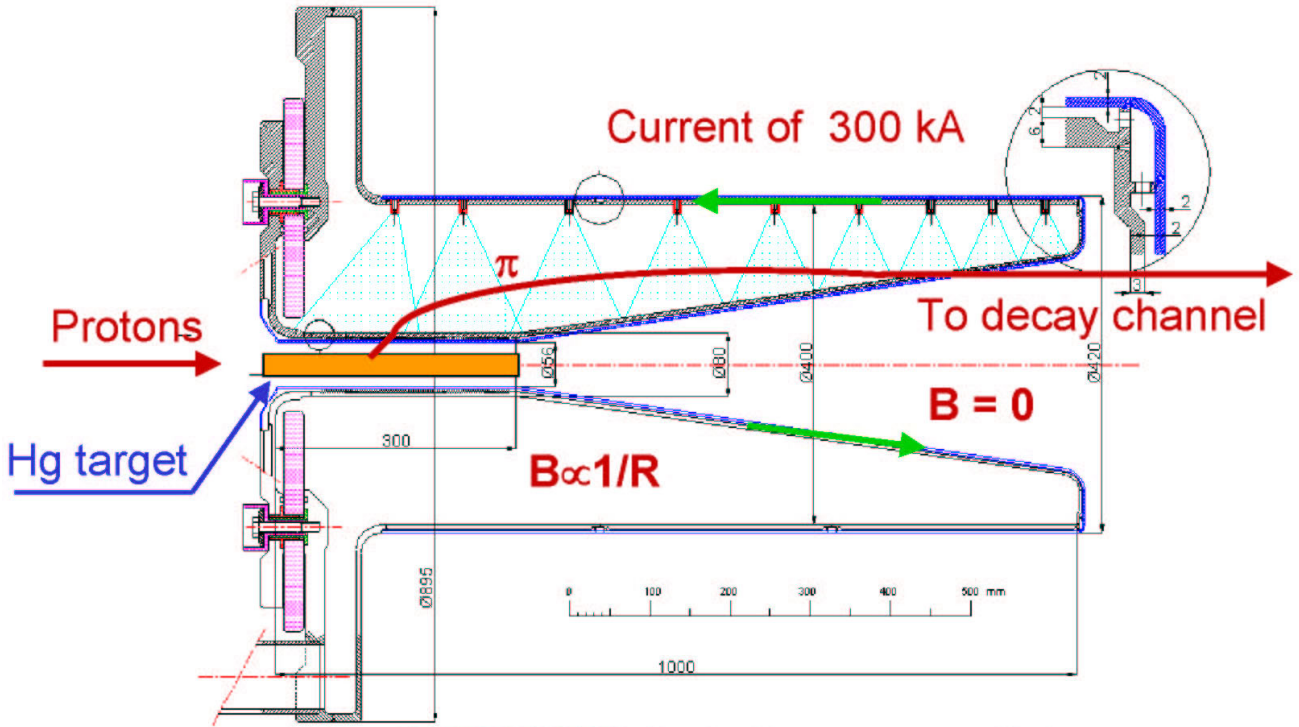
10.9-T Prototype magnet, 6-cm warm bore;  
 hybrid coil (NbTi, Nb<sub>3</sub>Sn, HiTc)  
 Graphite target.

Beam test of coil mockup at KEK with 12-GeV protons, 10<sup>11</sup>/s.



# Neutrino Horn + Target R&D at CERN

*S. Gilardoni et al.*



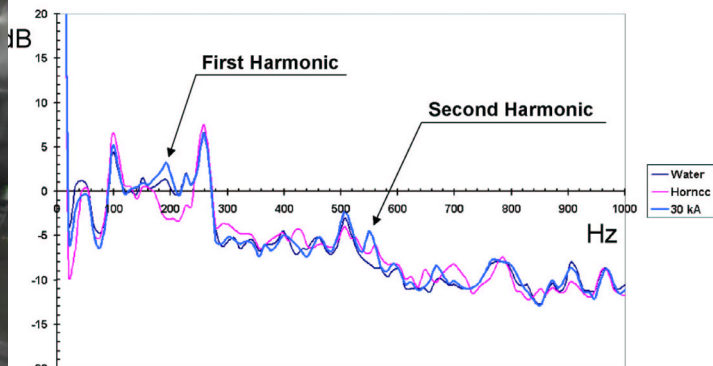
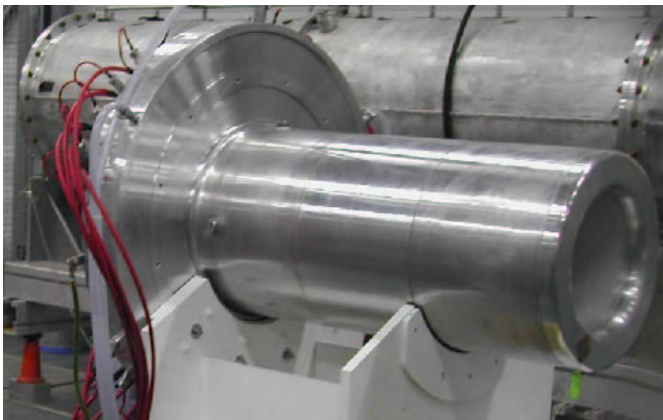
- First “inner” horn 1:1 prototype
- Power supply for Test One:
  - 30 kA and 1 Hz, pulse 100  $\mu$ s long
  - ✓ First mechanical measurements
  - Test of numerical results for vibration
  - ✓ Test of cooling system
- Test Two: 100 kA and 0.5 Hz
  - Testing during this week
- Last test: 300 kA and 50 Hz

done

Unknown schedule

**Goal: Horn Life-Time 6 weeks ( $2 \cdot 10^8$  pulses)**

... eigenfrequencies from horn “sound”



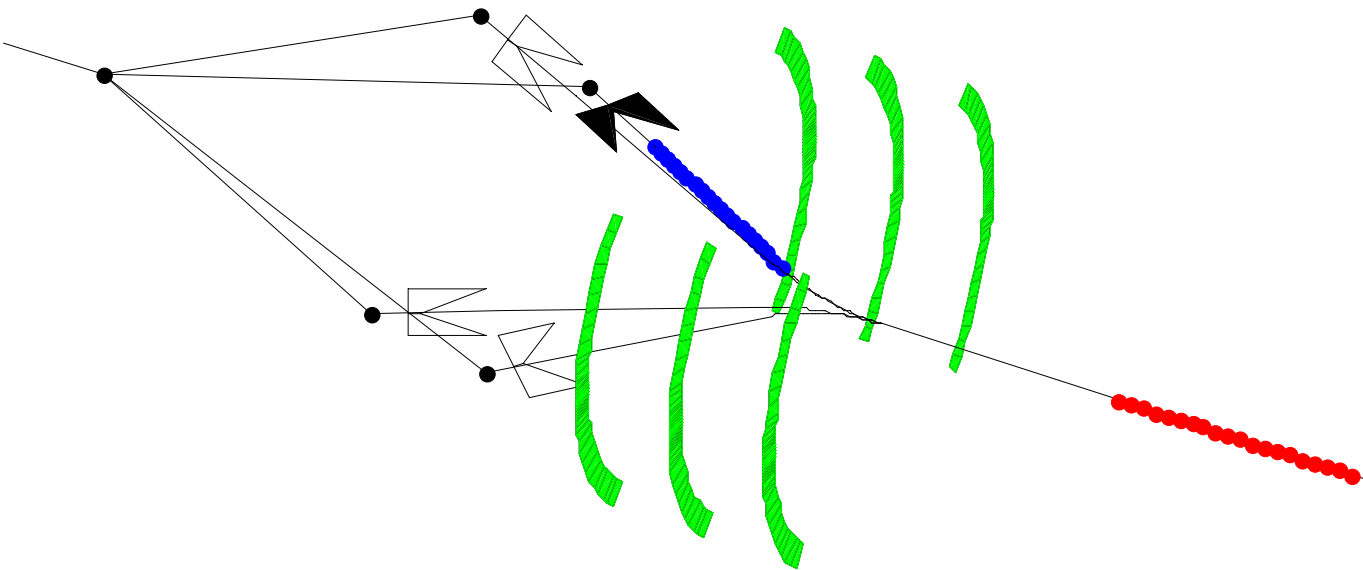


# Funneling $\pi$ 's and $\mu$ 's

B. Autin, P. Sievers, A. Verdier, F. Méot

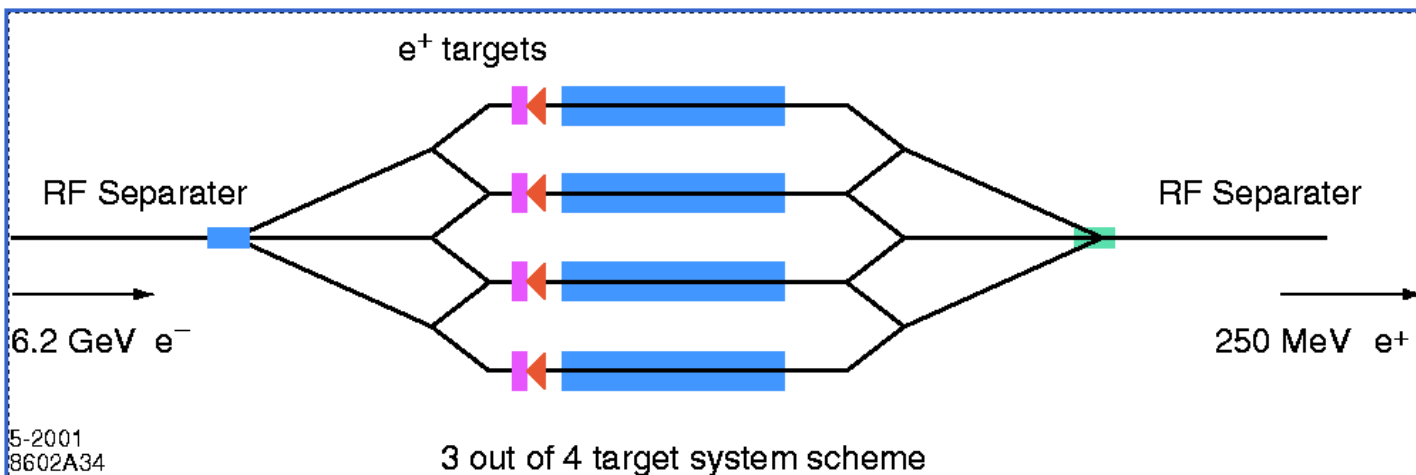
If one neutrino horn is good, 4 horns are better!

Use rotating dipoles to direct beam pulses into four beamlines, each with its own horn.



# Undulator Based Production of Polarized Positrons

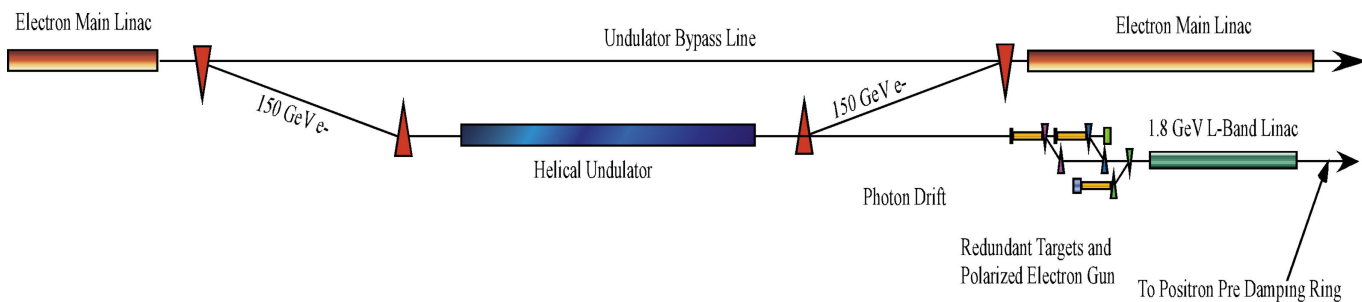
Would need multiple “conventional” positron production targets at a linear collider.



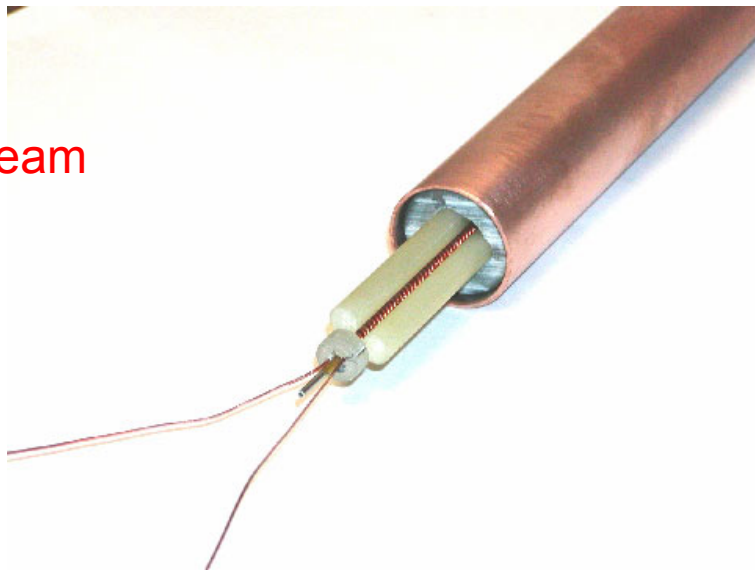
Mikhailichenko: Electron beam + helical undulator

=> Circularly polarized photons of  $\sim 10$  MeV.

=> Longitudinally polarized positrons out of thin target.



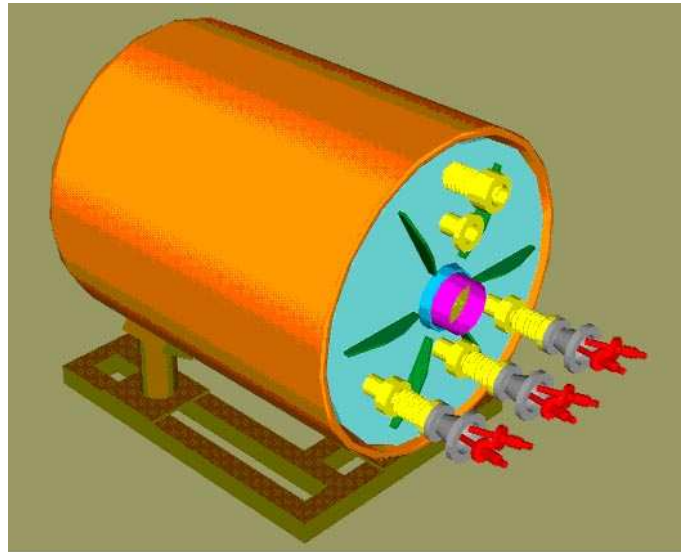
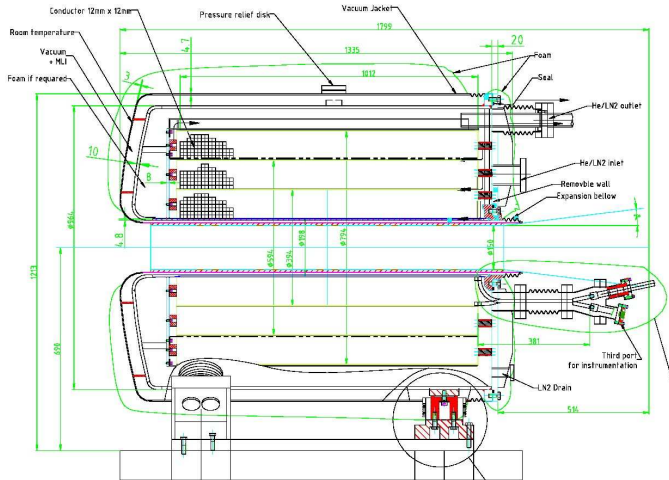
Demonstration proposed at SLAC (E-166) using the 50-GeV Final Focus Test Beam + 1-m-long, 1-mm-diameter pulsed helical undulator.



## Issues for Further Targetry R&D

- Continue numerical simulations of MHD + beam-induced effects.
- Continue tests of mercury jet entering magnet.
- For solid targets, study radiation damage – and issues of heat removal from solid metal targets (bands, chains, *etc.*).
- Confirm manageable mercury-jet dispersal in beams up to full Study-2 intensity – for which single-pulse vaporization may also occur. Test Pb-Bi alloy jet.
- Study issues when combine intense proton beam with mercury jet inside a high-field magnet.
  1. MHD effects in a **prototype target configuration**.
  2. Magnetic damping of mercury-jet dispersal.
  3. Beam-induced damage to jet nozzle – in the magnetic field.
- ⇒ We propose to construct a 15-T pulsed magnet, that can be staged as a 5-T and 10-T magnet.

## A 15-T LN<sub>2</sub>-Cooled Pulsed Solenoid



- Simple solenoid geometry with rectangular coil cross section and smooth bore (of 20 cm diameter)
- Cryogenic system reduces coil resistance to give high field at relatively low current.
  - Circulating coolant is gaseous He to minimize activation, and to avoid need to purge coolant before pulsing magnet.
  - Cooling via N<sub>2</sub> boiloff.
- Most cost effective to build the 4.5-MW supply out of “car” batteries! (We need at most 1,000 pulses of the magnet.)



# Beam + Jet + Magnet at the AGS or J-PARC

