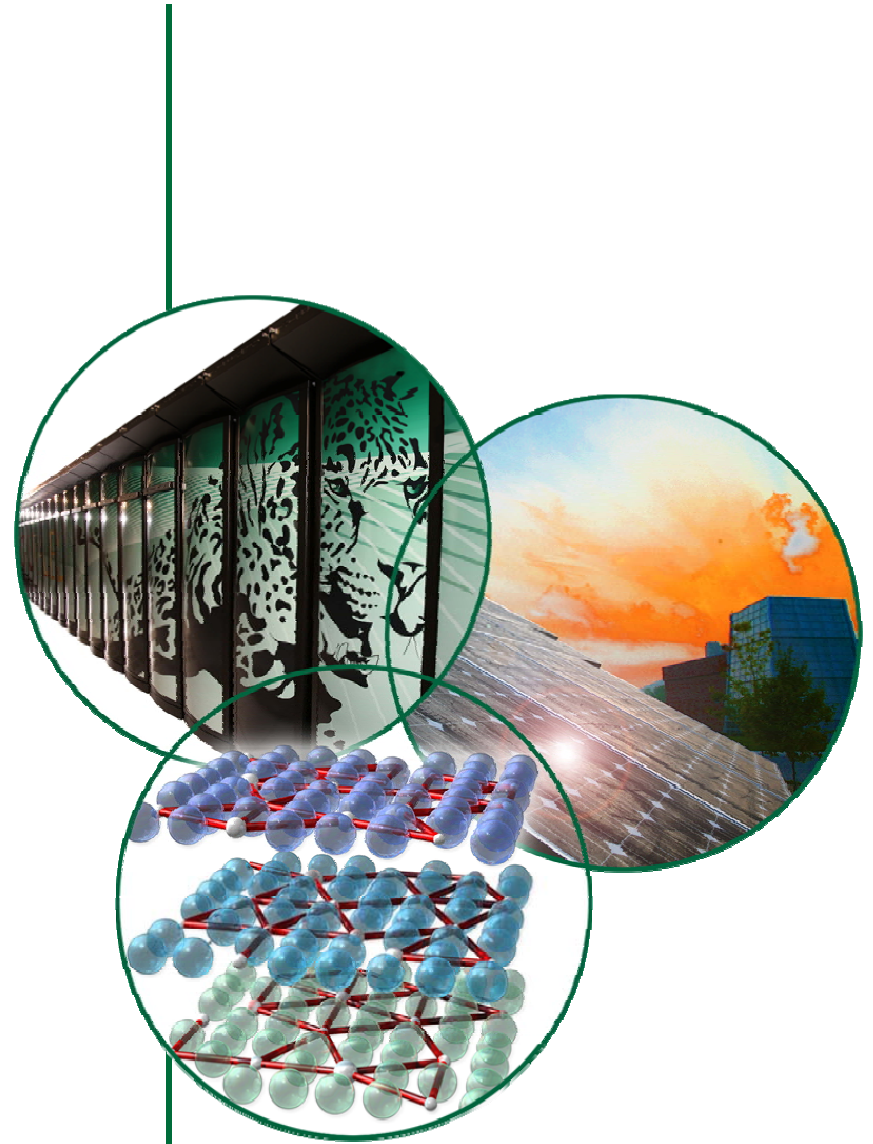


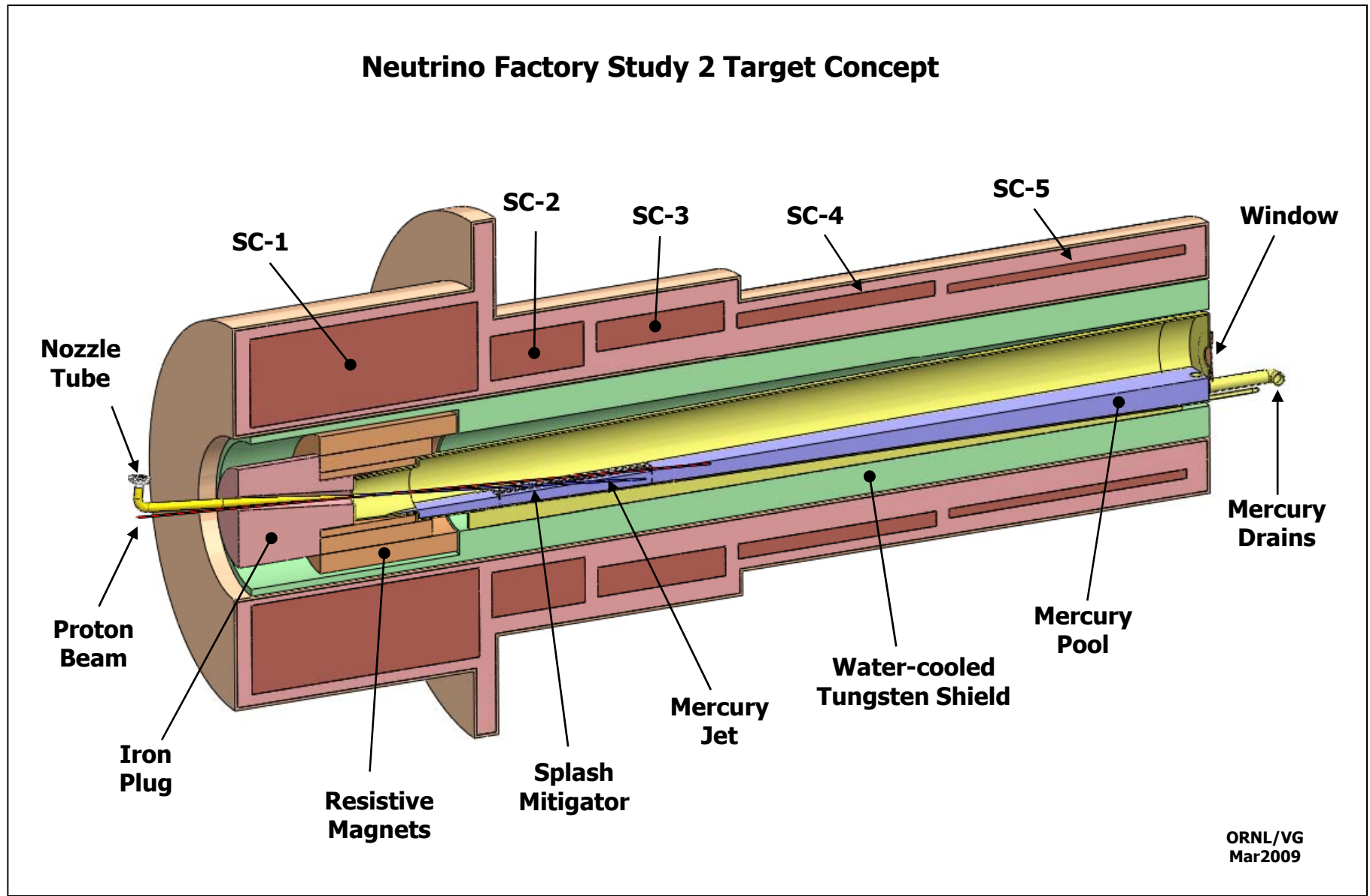
SC Magnet Shielding

Cale Caldwell
Van Graves

IDS-NF Phone Meeting
April 6, 2010



General Target Concept



Study 2 Energy Deposition (Table 3.5)

- SC shielding absorbs ~60% of beam power (589kW for 1MW beam)
- Value confirmed by more recent studies

Table 3.5: Energy deposition by cell in the target system. (x) stands for $\times 10^x$.

Cell Number	Description	Energy Deposition		
		(Mev/gm-p)	(W/cm ³)	(kW)
8	Surrounding shield	3.11(-4)	0.16	589
12	Primary mercury target	2.62	1.48(3)	53.1
2	Coaxial shield around target	1.55(-3)	0.82	40.4
3	Iron plug behind target	1.21(-3)	0.39	0.99
81	First coaxial magnet	2.61(-4)	0.08	3.54
82	Second coaxial magnet	1.04(-4)	0.03	4.43
83	Third coaxial magnet	2.38(-5)	0.01	1.70
91	Mercury beam stop	6.04(-4)	0.34	1.07
92	Mercury beam stop	8.64(-4)	0.49	2.55
93	Mercury beam stop	1.13(-3)	0.64	4.01
94	Mercury beam stop	4.80(-4)	0.27	1.20
95	Mercury beam stop	4.42(-4)	0.25	1.57
96	Mercury beam stop	4.89(-4)	0.28	1.74
97	Mercury beam stop	5.34(-4)	0.30	1.89
98	Mercury beam stop	6.87(-4)	0.39	2.44
99	Mercury beam stop	6.61(-4)	0.37	2.35
100	Mercury beam stop	4.86(-4)	0.27	1.73
101	Mercury beam stop	3.65(-4)	0.21	0.93

Shielding Geometry

- Baseline concept is water-cooled Tungsten spheres
 - Unknown heat transfer coefficient
 - Unknown packing factor
- Geometry
 - ID = 70cm, OD=114cm, thickness=22cm
 - Length =5m
 - Less thickness available at up-beam end due to resistive magnets
- Can this geometry remove 600kW heat energy?
 - 2.3MW for 4MW beam???

First Approximation Heat Transfer

- Assume solid tungsten cylinder with internal water tubes, single pass water flow
- $Q = \dot{m} * c_p * (T_o - T_i)$
 - $Q = 600 \text{ kW}$
 - $c_p = 4186 \text{ J/kg} * \text{K}$

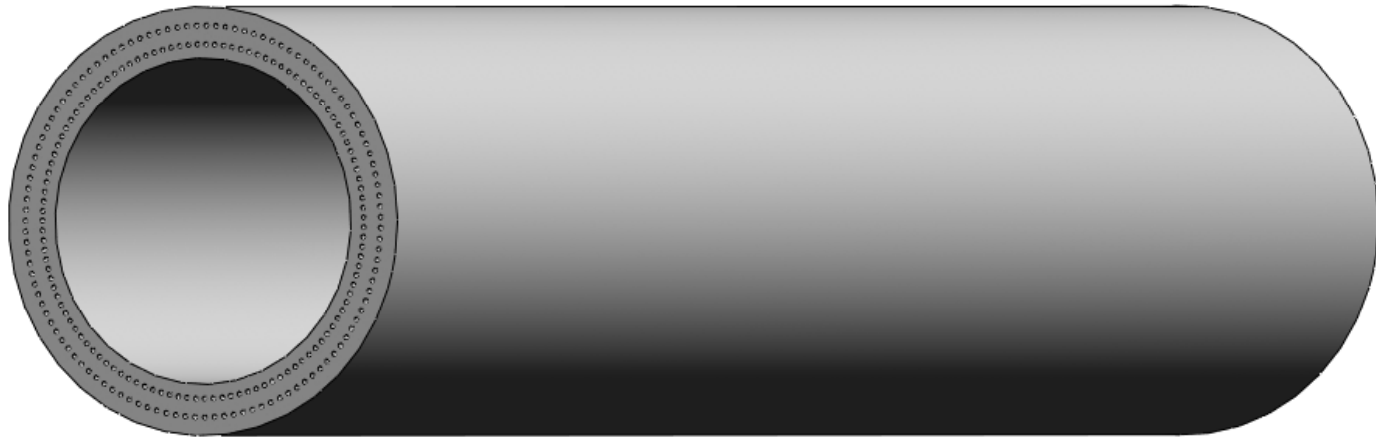
Cooling Water
Inlet T = 0 C



Cooling Water
Outlet T = 100 C

Using water as the coolant and assuming 600kW of heat generated, the required flow rate is 1.4 m³/s.

Flow Distribution



- The large flow rate can be distributed into 1 cm tubes.
- 152 tubes are required to achieve the necessary flow rate.
 - $q = 570$ liters/min (150gpm) per tube
 - $v = 120$ m/sec, not feasible
- 11cm of Tungsten allows enough room for the cooling tubes, while 82% of the cross-sectional area is Tungsten.
 - Reduces effective shielding density

Issues/Next Steps

- Further analysis needed for this case
- More sophisticated analysis needed for spheres

- Look at mercury as a shield/coolant
- Recalculate for 4-MW beam