



Modelling shock in solid targets

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Estimation of the thermal stress in materials

Thermal Stress ~ $\alpha E \Delta T / (1 - \nu)$ $\Delta T = EDD / C_P$

 $\begin{array}{l} \alpha & - \mbox{ thermal expansion coefficient} \\ E & - \mbox{ elastic modulus} \\ \Delta T & - \mbox{ temperature rise} \\ \nu & - \mbox{ Poisson's ratio} \\ EDD & - \mbox{ energy deposition density} \\ C_p & - \mbox{ specific heat} \end{array}$

α=f(T); E=f(T); v=f(T); Cp=f(T) !!!

Thermal stress as a function of temperature for different materials?



Stress in the target for energy deposition density of 20 J/g

20 J/g corresponds to ~ 300 J/cc in Ta (and W) - energy density for 4-5 MW beam power, 6-10 GeV protons -

Assuming that the tensile strength (=f(T)) is a measure of material mechanical strength we can introduce 'stress quality' factor = thermal stress/tensile strength lower value of stress quality factor -> 'better' candidate for solid target

Material 'stress quality' factor



Looks interesting in general (it is valuable alloying agent). Almost all ultra-high strength steels contain Mo in amounts from 0.25 to 8%.



Simulations of the shock in the solid Neutrino Factory target





Material model used in the analysis

- Temperature Dependent Bilinear Isotropic Model
- Uses 2 slopes (elastic, plastic) for representing of the stress-strain curve
- Inputs: density, Young's modulus, CTE, Poisson's ratio, vield stress....





LS-DYNA input (estimate; especially / for T> 1000K)

Problems with material data:

- reliable data can be found for temperatures up to 1000K (but inconclusive);
- no data (practically) at high temperatures.





Slicing of the target does not help if shock transit time is bigger than macro-pulse length







Status of simulations of the current pulse – wire tests at RAL

Experiment (Tantalum wire)

The wire is 0.5 mm diameter, tantalum.

Originally it protruded from the graphite top connection by 0.5 mm and ended up protruding 3 mm.

The wire ran for 16 hours at 3.125 Hz repetition rate.

The wire was run at 100 C rise per pulse for the first 6.5 hours, ... The last 5 hours was at 4900 A, pulse, corresponding to a temperature rise or 150 C per pulse.

The peak temperature ... was estimated to be ~ 1300 C.

One can see that the wire has become reduced in radius in parts and is thicker in others.

0.1

Geometry

0.5mm diameter; 40mm long wire; supported at bottom, free at top

Loads

Current pulse: ~ 5 kA, exponential rise

The power supply planned for the test purpose can deliver up to 8kA and the pulse waveform has a rise time of about 100ns and a flat top of about 500ns. The shape of the pulse waveform is exponential $I = I_0(1 - e^{-\gamma t})$ with time constant $t_0 = 1/\gamma = 30$ ns. Assuming that an electric field is instantaneously applied across the conductor of radius a and that current density j is circularly symmetric about the axis of the conductor the corresponding diffusion equation can be obtained by using Maxwell's equations. The solution of the diffusion equation for the case of an exponential rise in current density at r = a has the form:

$$\begin{split} j_x &= j_{x0} \{ 1 - \frac{J_0(\sqrt{\gamma r^2/\kappa})}{J_0(\sqrt{\gamma a^2/\kappa})} e^{-\gamma t} + \\ &+ \frac{2\gamma}{a\kappa} \sum_{n=1}^{\infty} \frac{J_0(\beta_n r/a) e^{-k(\frac{\beta_n}{\alpha})^2 t}}{\frac{\beta_n}{a} J_1(\beta_n) [(\frac{\beta_n}{a})^2 - \frac{\gamma}{\kappa}]} \}, \end{split}$$

where j_{z0} is the current density at r = a, β_n are the roots of the Bessel functions of the first kind, $J_1(*)$ and $J_0(*)$ are the corresponding Bessel functions, $\kappa = 1/\mu_0 \sigma$ with μ_0 being the permeability of free space and σ is the electrical conductivity.

Lorentz force induced pressure wave



Multiple pulses

Time [ms]

 Pulse time (heating) ~ 600 ns; APPROXIMATION: Time temperature rise per pulse ~ 110 C between pulses (cooling)~ 500 μ s; 50x longer than Time between pulses (cooling) ~ (longitudinal) characteristic 300 ms; LS-DYNA needs 115 h time! to complete 1 pulse! 50 pulses (16 h to complete); temperature rise ~ 1300 C Ta wire 1.4 PANENDAMANENENAMANENENENAMANENENEN 1.2 A 8991 B 7506 Temperature rise [K] (E+3) 80 80 80 81 1 81 90 82 1 C 6003 D 4500 final \rightarrow 500x longer cooling time than (longitudinal) characteristic time 0 10 15 20 25 30 0 5



Tantalum wire: 0.5 mm diameter, 40 mm long

A 8983

B_7498

C 5995

D_4492

A 8983 B 7498

C 5995

D 4492

X

30

ABC

25

25

30

35

LS-DYNA





Initial temperature = 2300 K



Peak current can be 'tuned' to have a wanted value of the peak stress in the wire





Comparison: Stress in real target vs. stress in tungsten wire





This wire had survived over 3 million pulses at 5 kA. Bent into this severe shape within a few minutes at 7.2 kA. Solution: bigger target radius? It looks possible. Captured yield practically the same for 1 cm radius -> 1.5 cm radius.









Beam radius = rod radius; Beam offset = 1/2 radius.





Tungsten target: 3x20 cm Beam: 4 MW, 50 Hz, 6 GeV, 4x2ns, 10 μs Energy deposition from MARS (S. Brooks)

LS-DYNA (3D)



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Summary

- Solid target for the Neutrino Factory:
 - Shock waves in candidate materials (Ta, W, C) characterised within limitations of material knowledge
 - Effects of beam pulse length and multiple bunches/pulse understood (stress reduction by choosing optimal macro-pulse length)
- Test of wire:

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- First estimate of the lifetime of tantalum (and tungsten) NF target
- VISAR is purchased to measure surface velocity of wire and compare results with LS-DYNA calculations (this will help to extract high temperature material data from experiment)
- Repeat experiment with graphite and the others candidate materials
- **Conclusions**
 - Nice agreement between LS-DYNA and existing experimental results
 - 2 MW -> looks possible in 2 cm diameter target (W is better than Ta)
 - 4 MW -> needs bigger target diameter (2 cm -> 3 cm)