

Nuclear Graphite - Fission Reactor Brief Outline of Experience and Understanding

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Overview

- Nuclear Graphite – Use, Manufacture, Microstructure
- Irradiation Damage to Crystal Structure
- Radiolytic Oxidation
- Physical Changes – to Polycrystalline Graphite due to Fast Neutron Damage and Radiolytic Oxidation
- Irradiation Creep

Use of Graphite in the Nuclear Industry

- Moderator
 - Slow down neutrons by scattering
 - High scatter cross-section
 - Low absorption cross-section
- Reflector
 - Reflects neutrons back into the core
 - Protect surrounding supports structure and pressure vessel
- Major Structural Component
 - Provided channels for control rods and coolant gas
- Neutron Shield
 - Boronated graphite
- Thermal columns in research reactors
- Moulds for casting uranium fuel

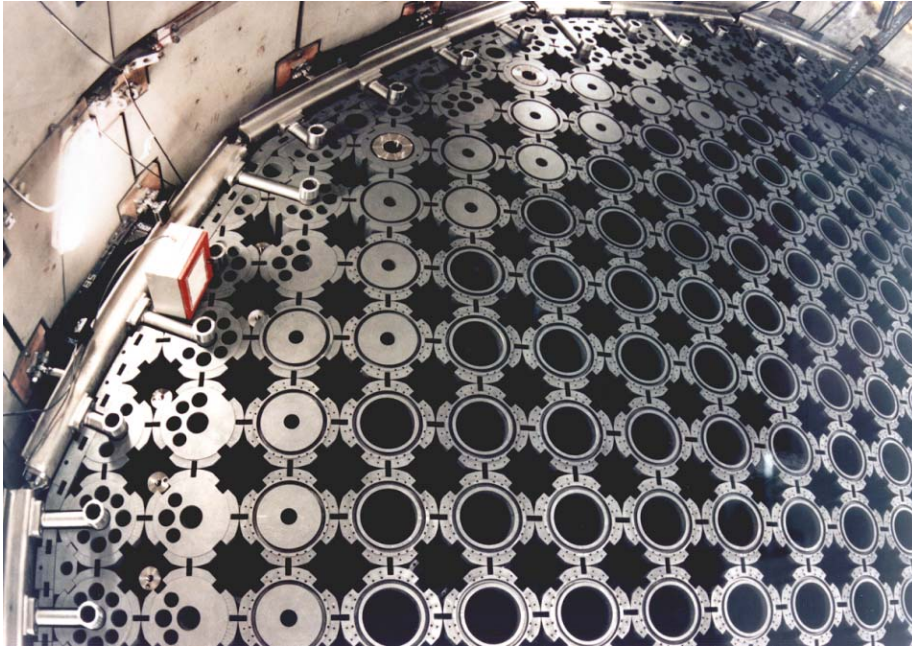
Type of Graphite Moderated Reactors

- Air-cooled
 - Chicago Pile, GLEEP, BEPO, Windscale Piles, G1-France
- Light Water-cooled Graphite Moderated
 - Hanford, Russian-PPR, RBMK
- Carbon Dioxide Cooled
 - UK and French Magnox reactors, AGR
- Helium Cooled
 - Dragon, Peach Bottom, Fort St. Vrain, THTR, AVR
 - HTR, HTR-10 China, HTTR Japan, PBMR South Africa
 - Generation IV - VHTR

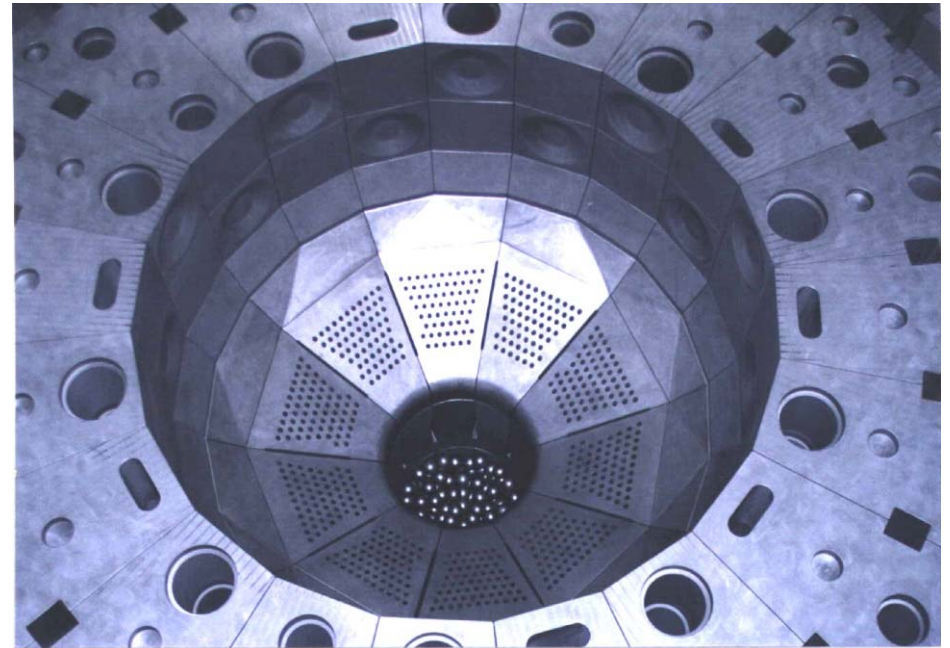


Chicago Pile 1

Typical Graphite Components

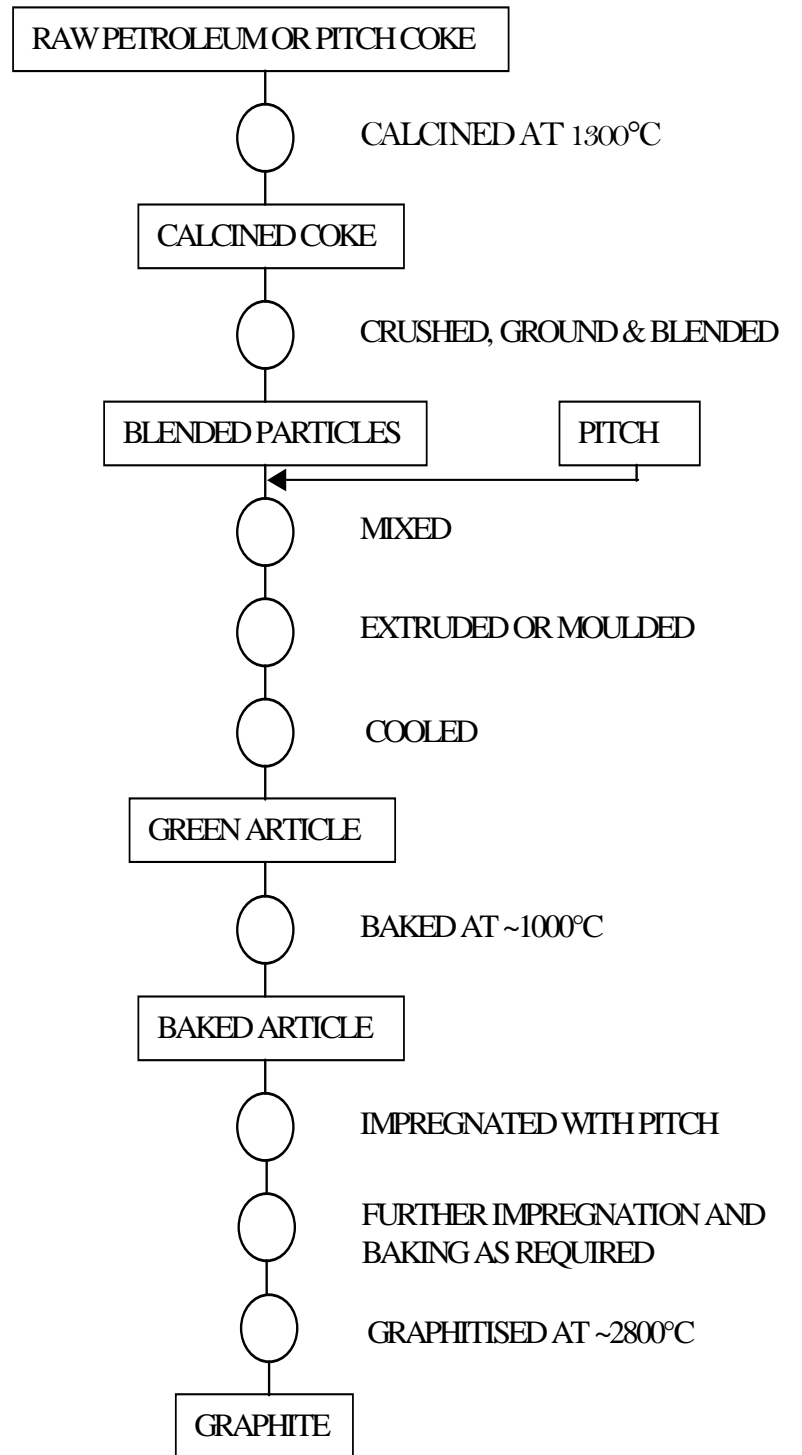
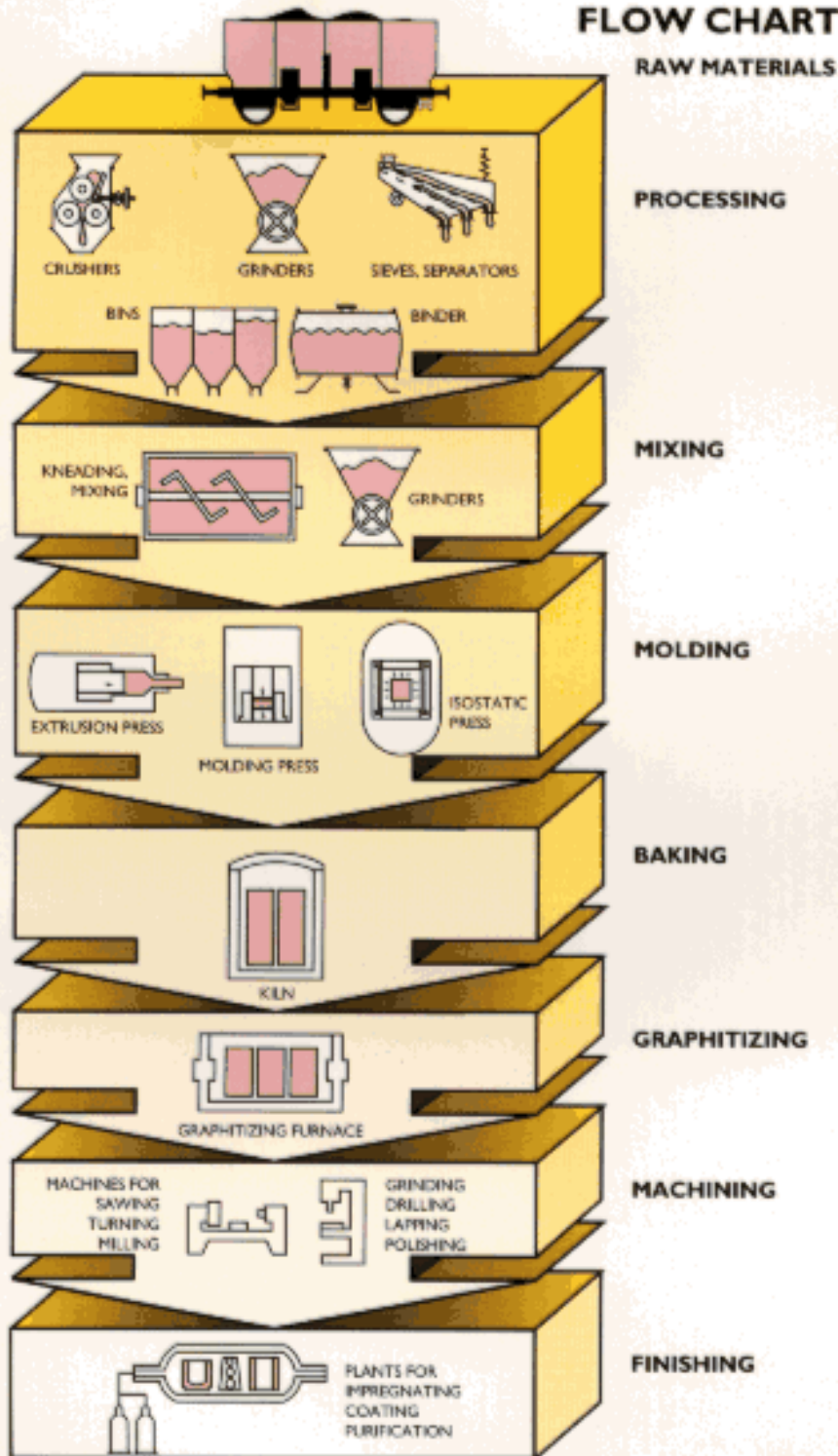


Torness Core – During
Construction



HTR-10 During Construction in
China

FLOW CHART



Final Product

- Either anisotropic or semi-isotropic product
 - Modern reactors use graphite with semi-isotropic properties
- Significant porosity ~20%
 - ~10% open porosity, ~10% closed porosity
 - Density 1.72 – 1.8g/cm³ compared to 2.26g/cm³ for perfect graphite crystal
- High purity – impurities measured in parts per million (ppm)
- Nuclear designer requires
 - Semi-isotropic 1.1 Defined by Coefficient of Thermal expansion (CTE) in orthogonal directions
 - High density
 - Optimum material properties
 - High thermal conductivity
 - High purity (neutronic and waste point of view)
 - Dimensional stability under irradiation, associated with high CTE $\sim 4 \times 10^{-6} \text{ K}^{-1}$ (20-120°C)

Pile Grade A Microstructure – Anisotropic

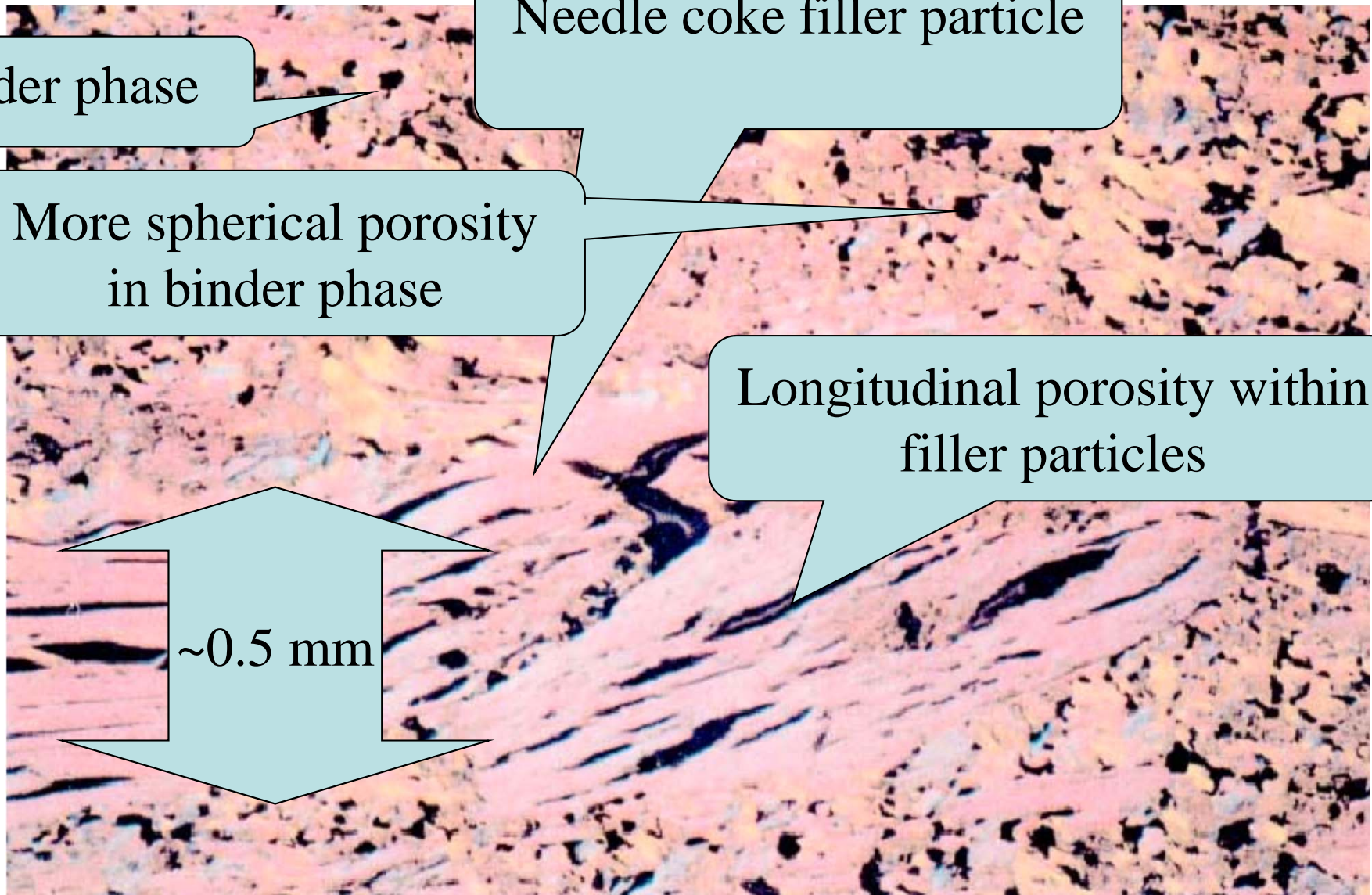
Binder phase

Needle coke filler particle

More spherical porosity
in binder phase

Longitudinal porosity within
filler particles

~0.5 mm

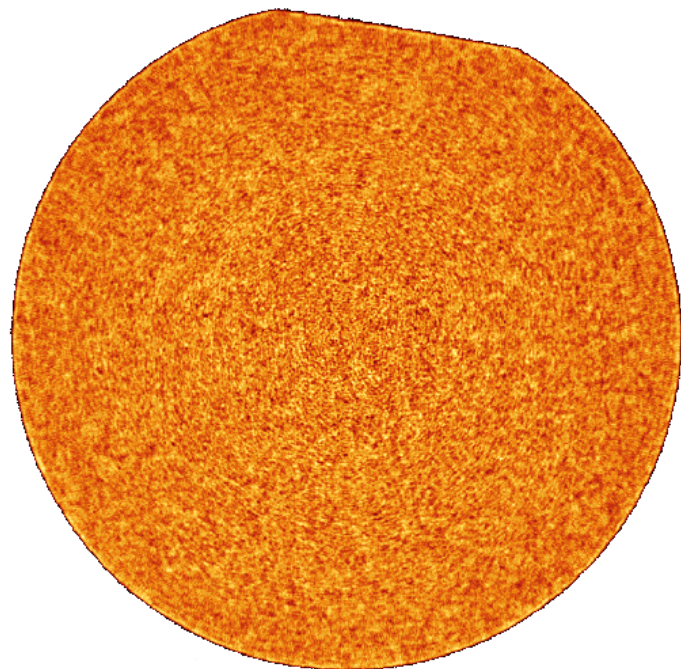


Grade	ZXF-5Q	AXF-5Q	Gilsocarbon	IG-430	IG-110
Comment	candidate	similar to AXF-8Q1 (US historical experience)	UK AGR experience	Japanese & EU experience	Japanese & EU experience
Particle size (μm)	1	5	500	10	20
Pore size (μm)	0.3	0.8	42	-	16
Density (g/cm^3)	1.78	1.78	1.81	1.82	1.77
Comp. strength (MN/m^2)	175	138	70	97	79
Flex. strength (MN/m^2)	112	86	23	52	40
Tensile strength (MN/m^2)	79	62	18	38	27
Modulus (GN/m^2)	14.5	11.0	10.8	10.8	9.7
CTE (10^{-6}K^{-1})	8.1	7.9	4.3	4.5	4.0
Thermal conduct. ($\text{W}/\text{m K}$)	70	95	131	143	135

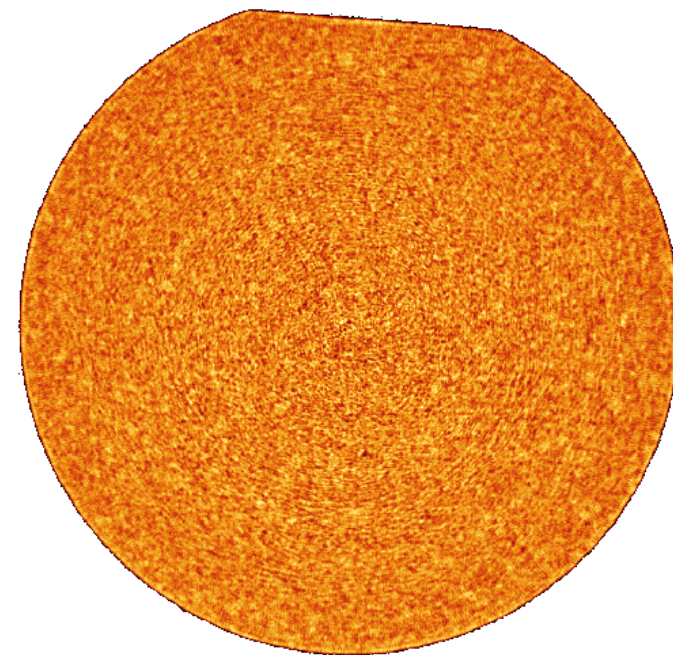
**Computed X-ray
tomography images
of various
grades of graphite**



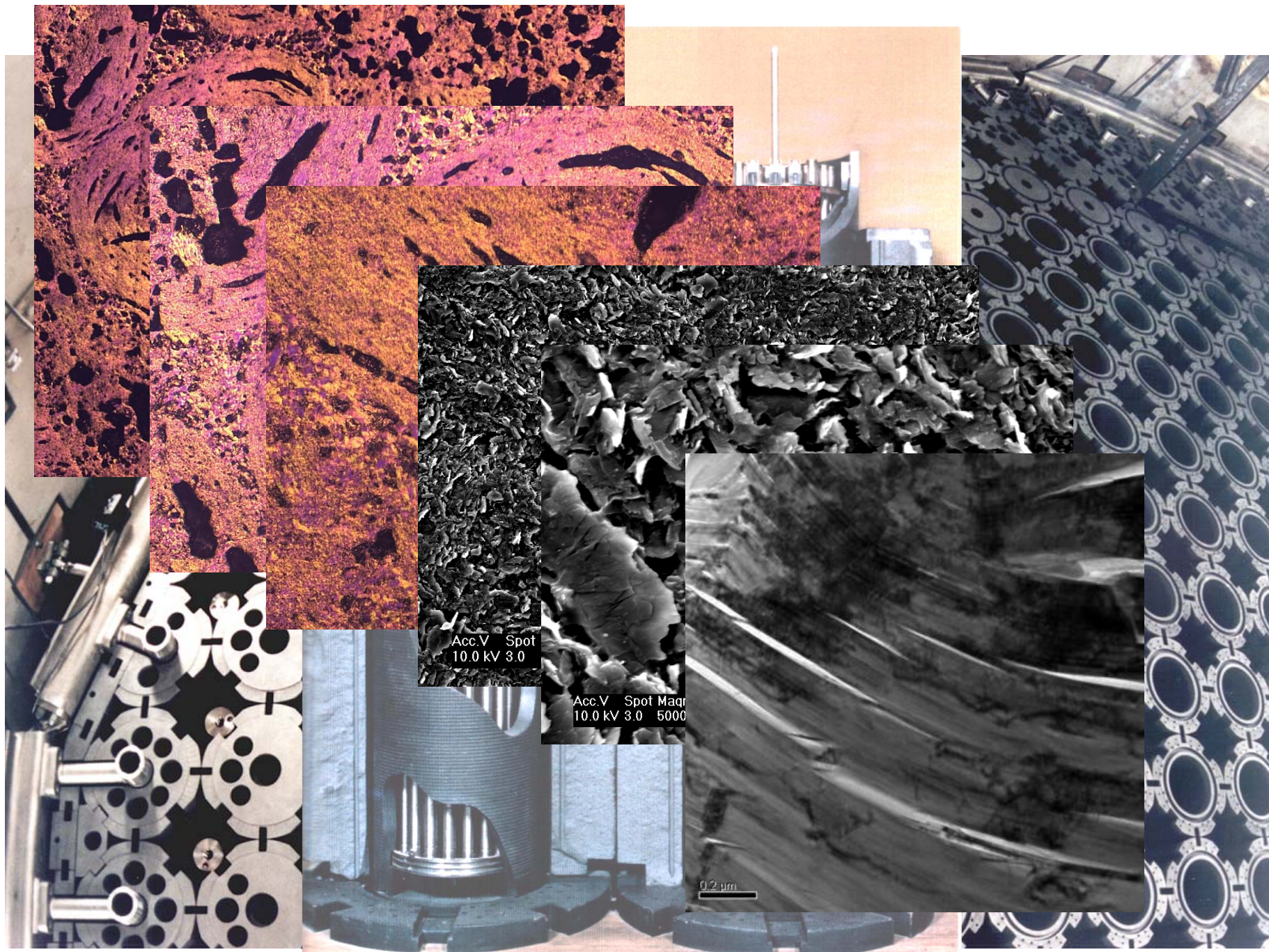
Gilsocarbon



IG-110

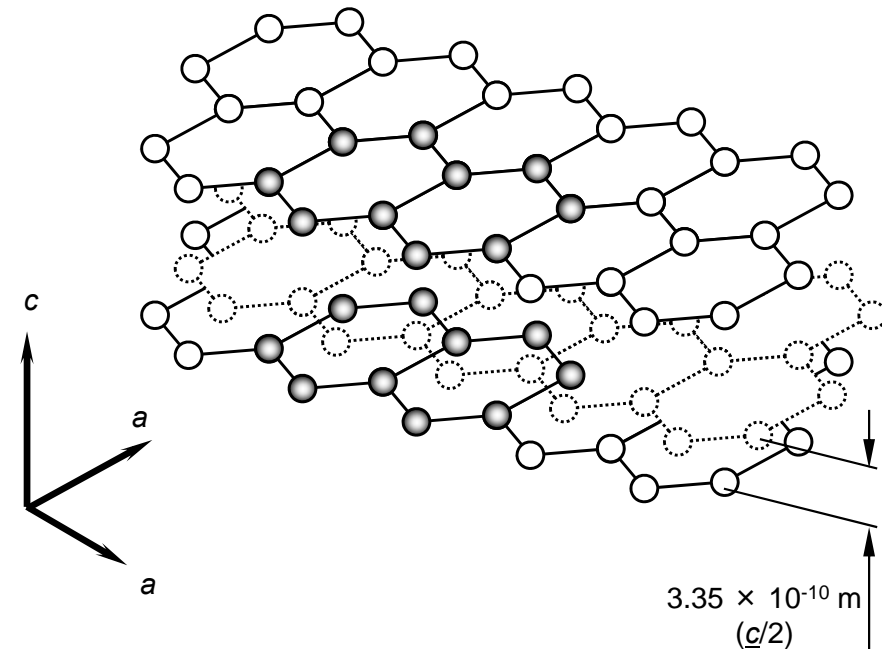
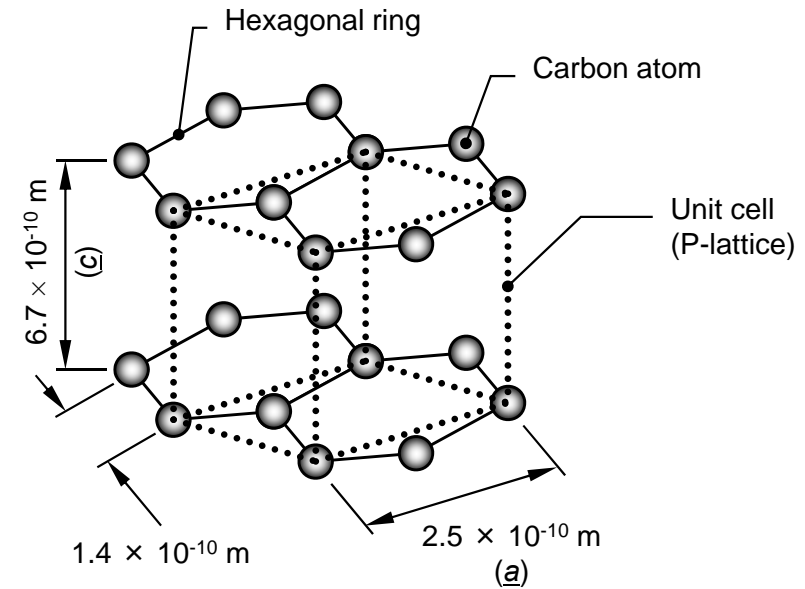


IG-430



Crystal structure

- lattice spacing
 - $a = 2.4612 \times 10^{-10} \text{ m}$
 - $c = 6.7079 \times 10^{-10} \text{ m}$
- alternately stacked planes
 - $335 \times 10^{-12} \text{ m}$
- density
 - 2.66 g/cm^3
- CTE
 - $\alpha_a = -1.25 \times 10^{-6} \text{ K}^{-1} (20\text{-}120^\circ\text{C})$
 - $\alpha_c = 26 \times 10^{-6} \text{ K}^{-1} (20\text{-}120^\circ\text{C})$



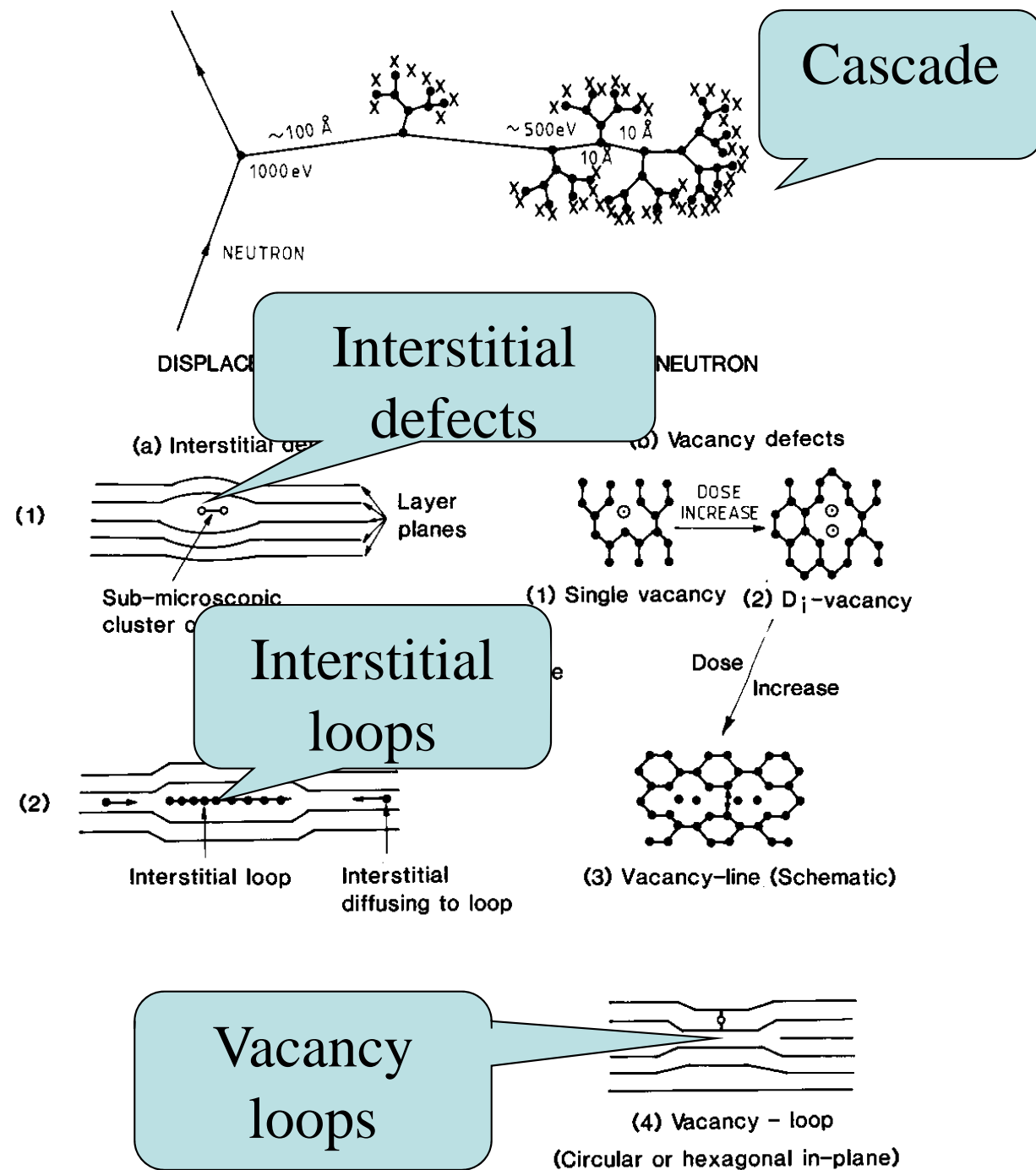
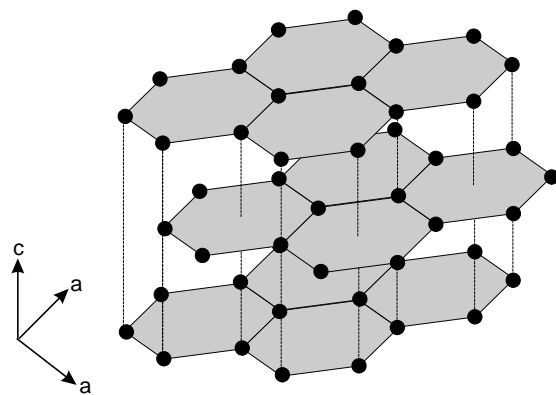
Irradiation damage to graphite Crystallites

- Damage leads to crystal changes:
 - Stored energy (Significant below irradiation temperatures 150°C, insignificant above 350°C)
 - Dimensional changes
 - Thermal conductivity changes
 - Modulus changes
 - Strength changes?
 - No Coefficient of Thermal Expansion (CTE) changes above ~300°C
 - Irradiation creep (when under stress)

Fast Neutron Damage

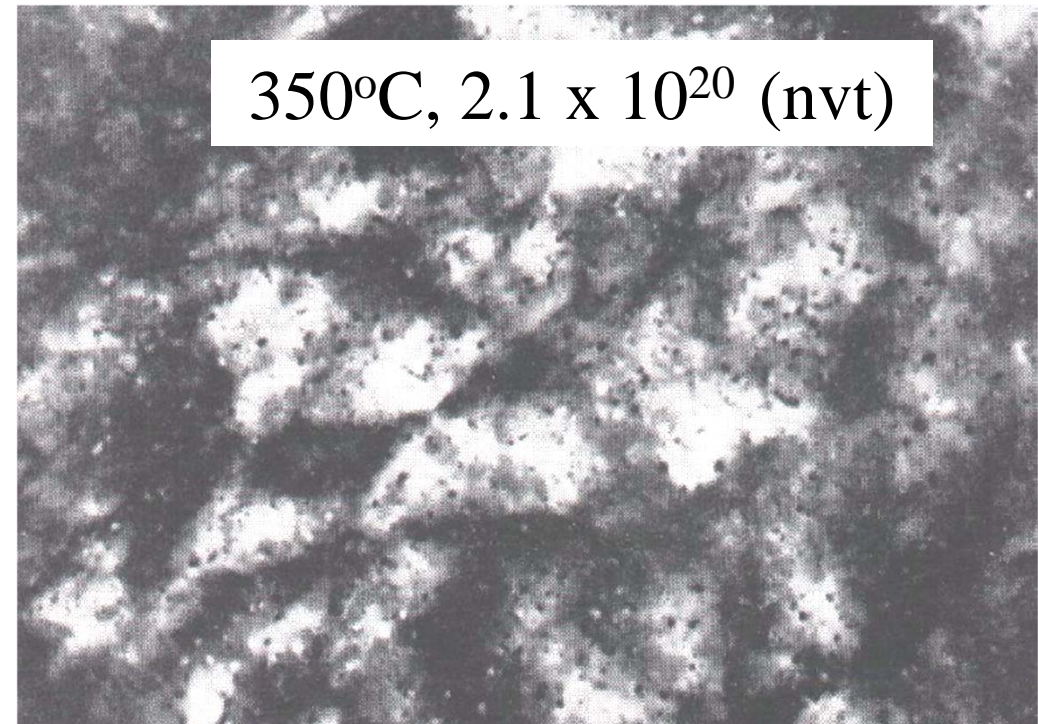
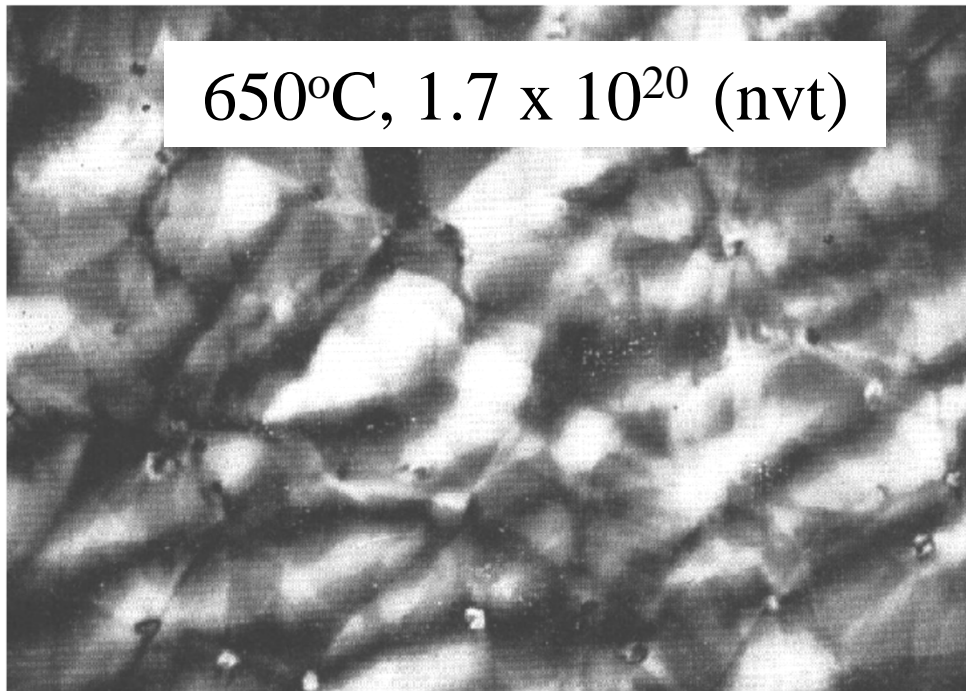
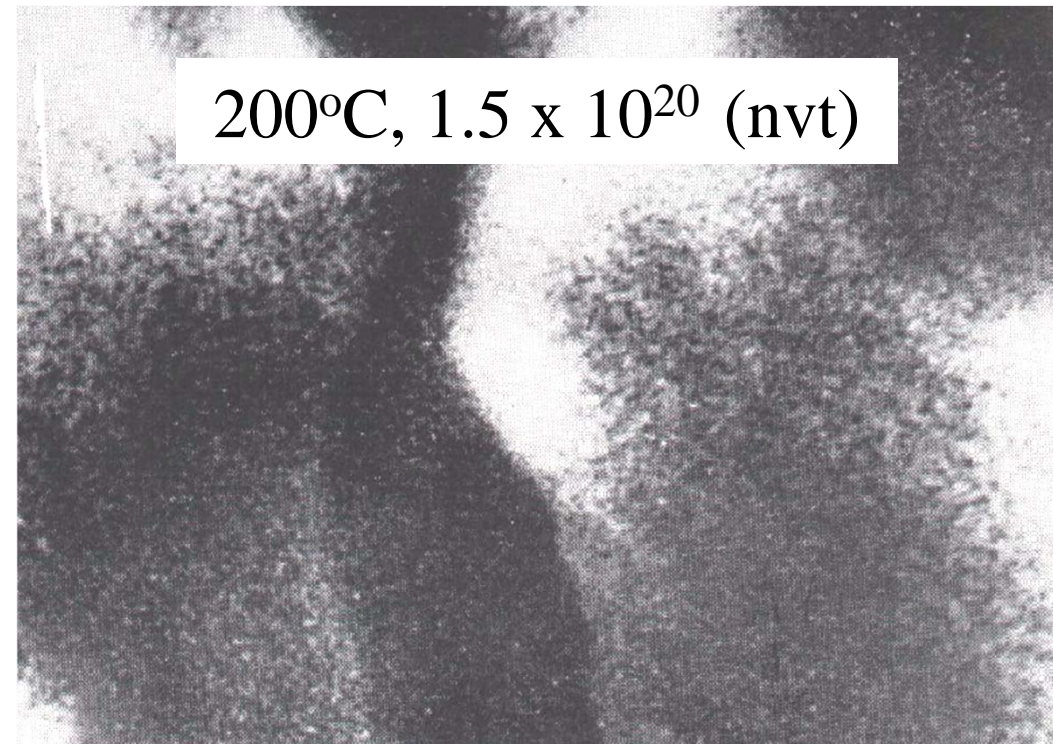
- Thermal reactor neutron energies up to 10MeV, average 2MeV
- About 60eV to permanently displace a carbon atom from the lattice
- Most damage due to fast neutron energies > 0.1 MeV
- Cascade caused by primary and secondary knock-ons
- Interstitial and vacancy loops are formed
- Size of loops depends on irradiation annealing
- Change in crystallite behaviour at an irradiation temperature of about 250°C
- A measure of damage is irradiation “dose” of “fluence” units:
- displacements per atom “dpa”
 - n/cm^2 - Equivalent DIDO Dose (EDND)
 - n/cm^2 – with energies greater than 0.18MeV ($E_n > 0.18\text{MeV}$)
 - nvt – neutron velocity time

Formation of interstitial and vacancy loops



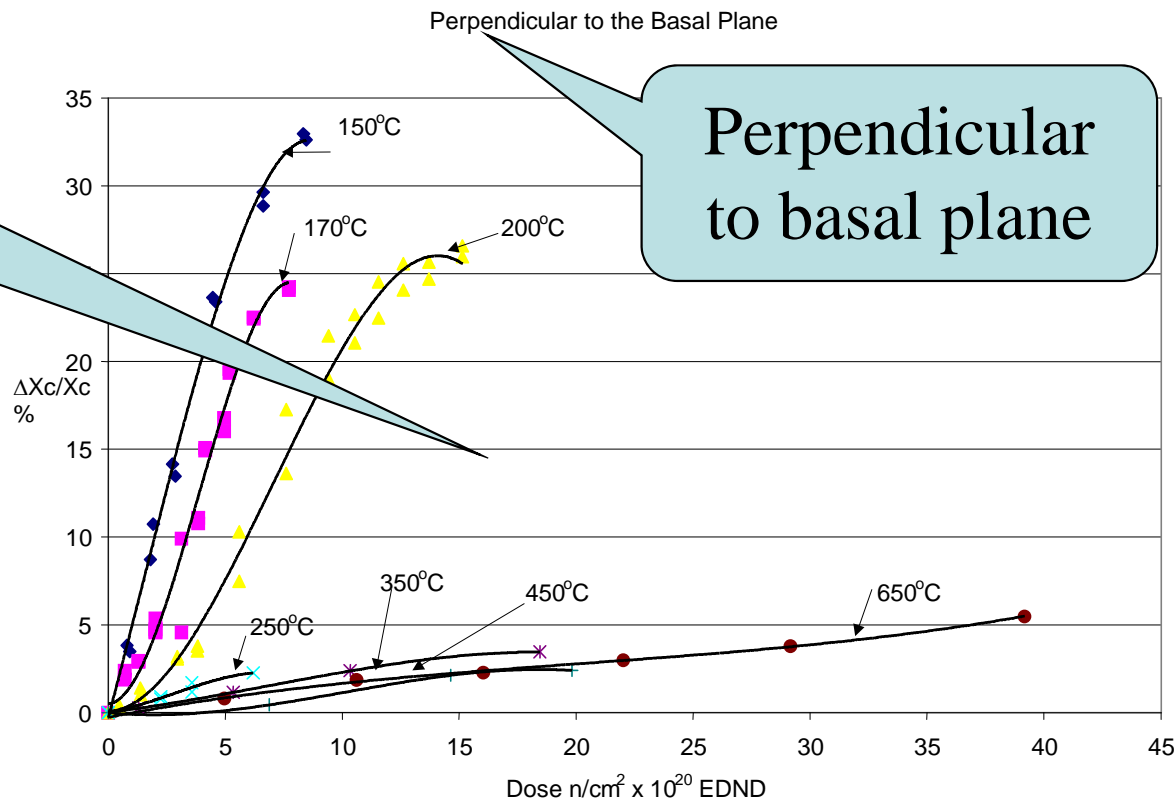
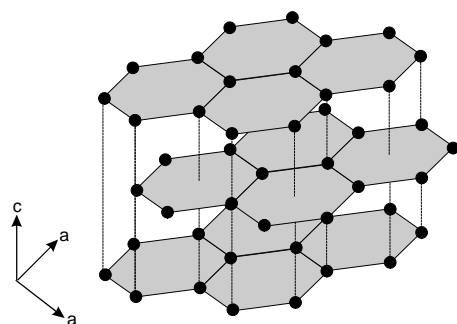
Irradiation defects in graphite crystals (HOPG)

(x 20,000)

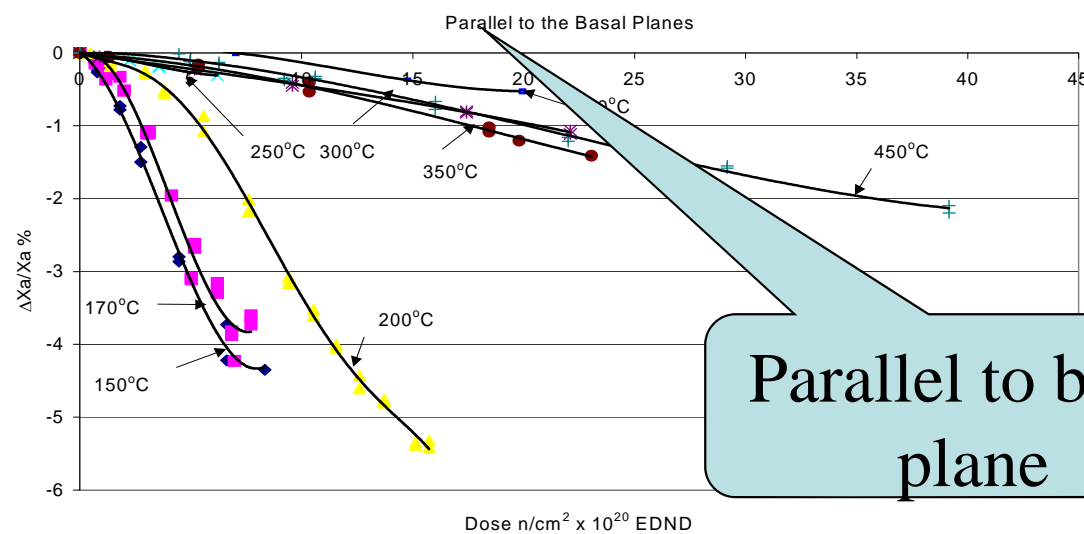


Significant change in rate between 200 and 250°C

Crystal Dimensional Changes measured in HOPG with increasing Dose

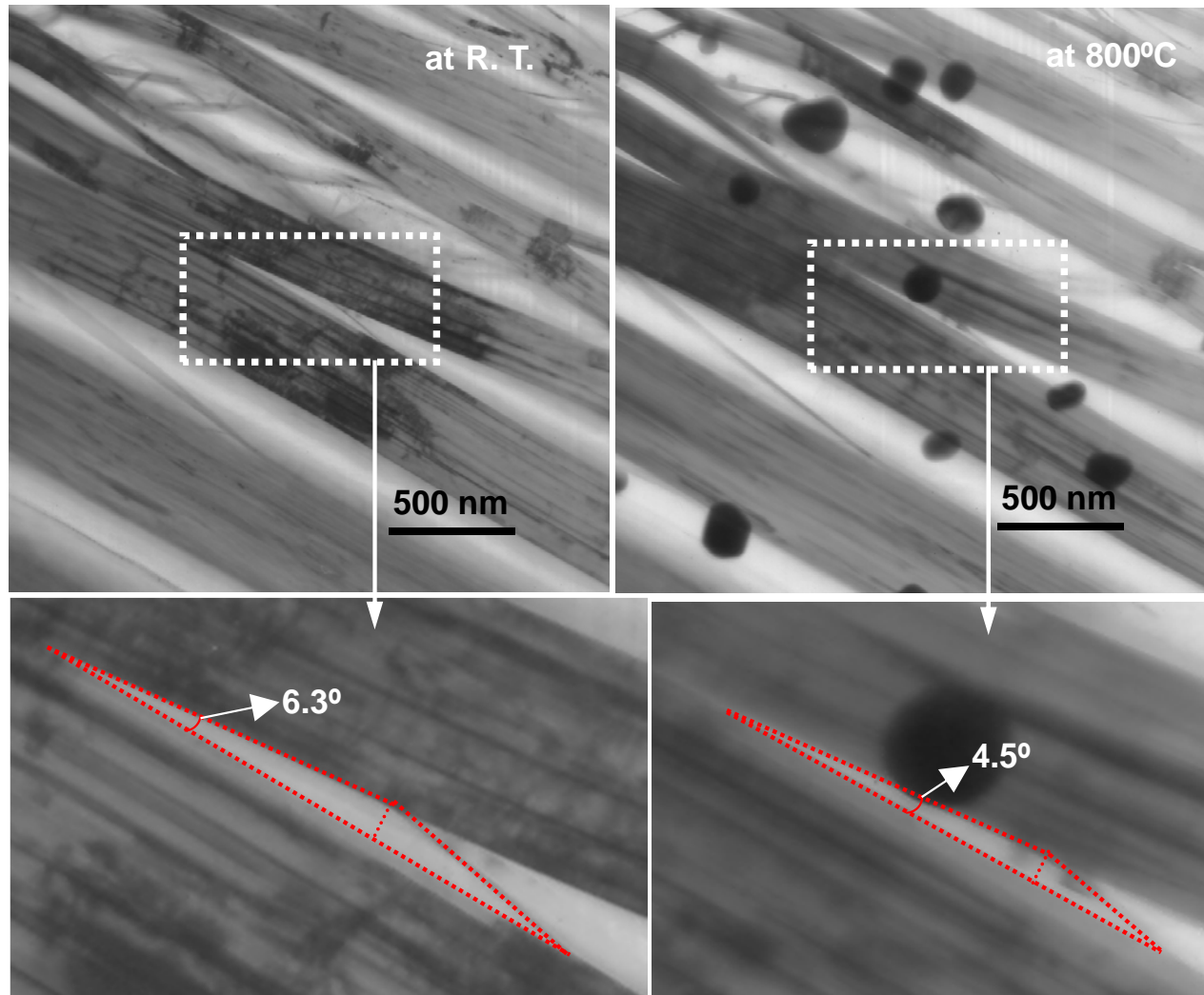


Perpendicular to basal plane



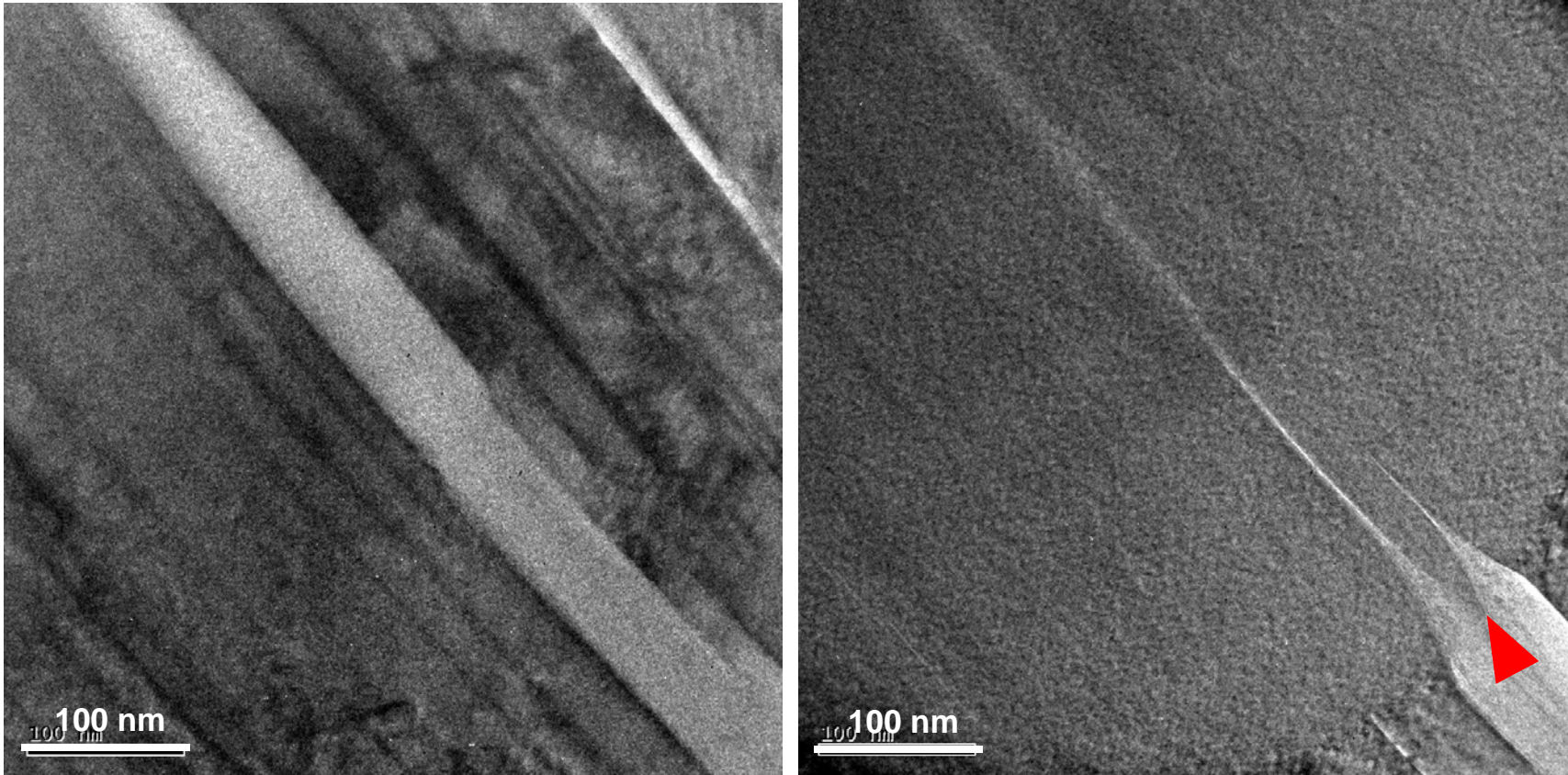
Parallel to basal plane

TEM: *In situ* heating



Upon heating, a gradual closure of cracks was observed because of the thermal expansion of the graphite crystallites surrounding the cracks.

TEM *In situ* electron irradiation



Closure of a crack in Gilsocarbon after In-situ electron irradiation. The feature with bright contrast does not disappear completely. Note a small part of crack (indicated by arrow), which was covered by the electron beam has not closed completely

Radiolytic Oxidation

- Two types of oxidation can occur in CO_2 .
 - Thermal oxidation is a purely chemical reaction between graphite and CO_2 .
 - Reaction is endothermic, is negligible below about 625°C and is not important up to 675°C .
 - Only an issue for HTRs
- Radiolytic oxidation occurs when CO_2 is decomposed by fast neutron and gamma radiation (radiolysis) to form CO and an active oxidising species which attacks the graphite porous structure.
 - Radiolytic oxidation occurs predominantly within the graphite pores.
 - Overall component geometry stays essentially the same

Radiolytic Oxidation

- The mechanism of radiolytic oxidation is:

- Gas Phase

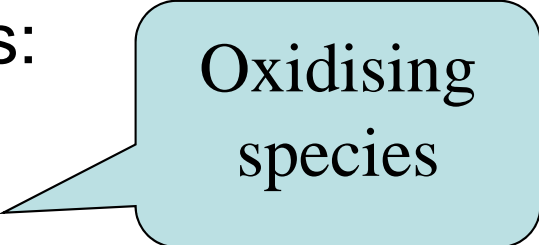


- Graphite Pore Surface



- Definition

- G_{-c} is the number of carbon atoms gasified by the oxidising species produced by the absorption of 100eV of energy in the CO_2 contained within the graphite pores.



Oxidising
species

Irradiation Damage in Polycrystalline Graphite

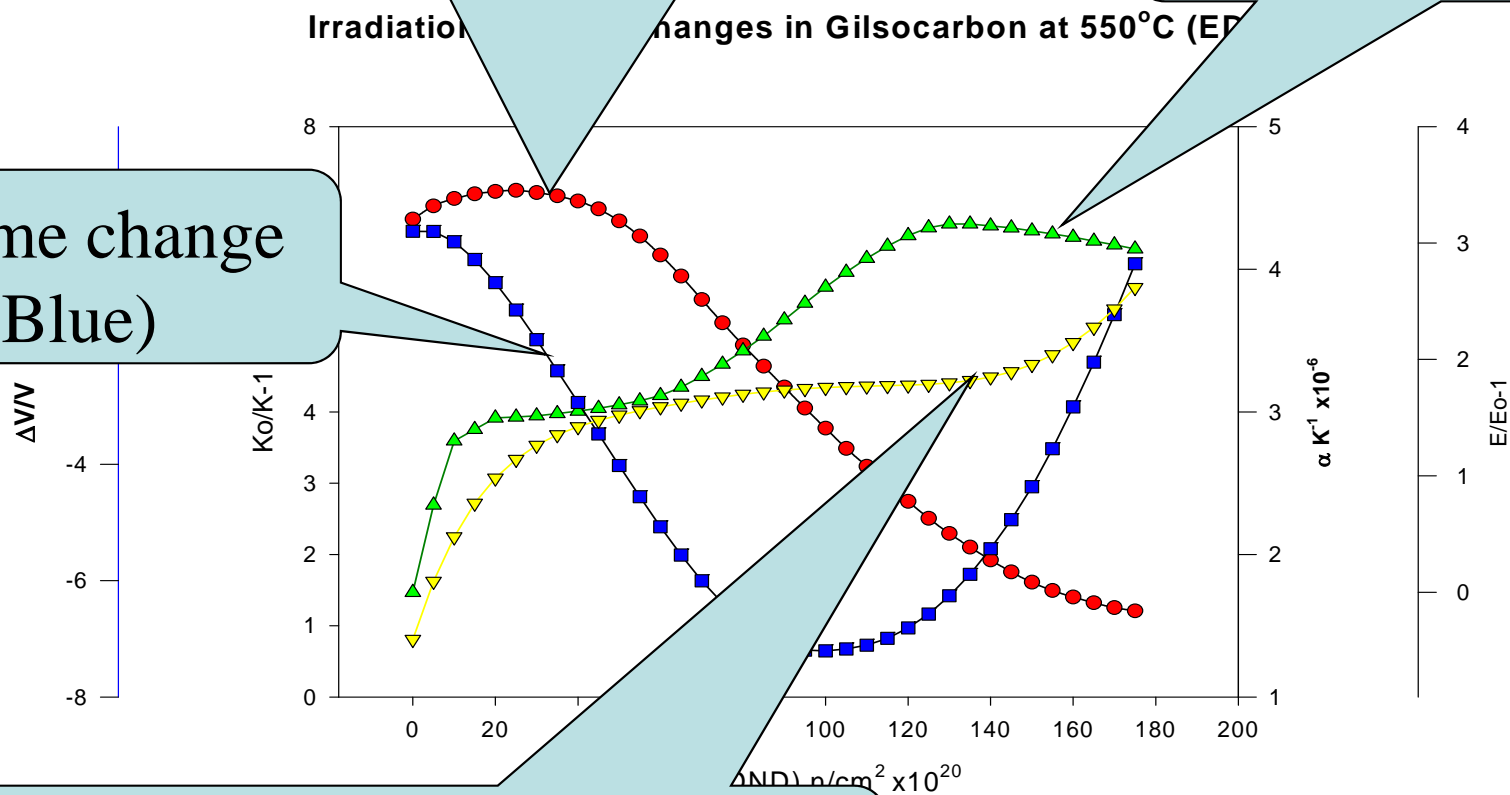
- Crystal changes modify polycrystalline dimensions and properties through the microstructure
 - Stored Energy – Only significant below 150°C, negligible at 350°C
 - Dimensional changes
 - CTE
 - Young's modulus
 - Strength
 - Thermal conductivity
 - Irradiation creep (when under stress)
- Radiolytic oxidation further modifies these properties
- Semi-isotropic graphite is considered in the next section

Graphite Irradiation Behaviour – Isotropic Gilsocarbon irradiated at 550°C

Coefficient of Thermal Expansion
change (Red)

Young's modulus
change (Green)

Volume change
(Blue)

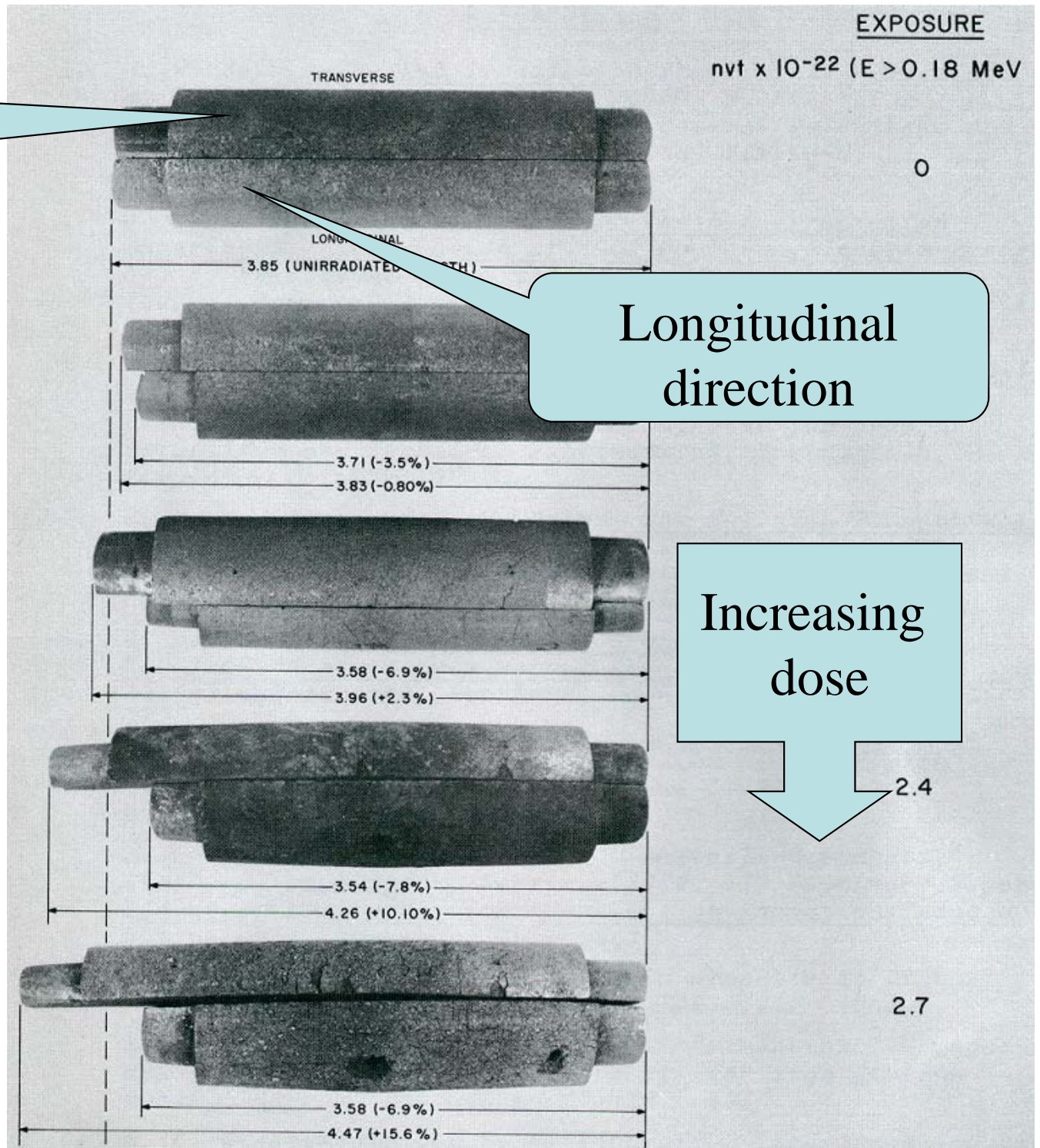


Thermal Resistivity change
(Yellow)

- Dose vs CTE
- ▲ Dose vs E/Eo-1
- Dose vs DV/V
- ▼ Dose vs Ko/K-1

Transverse direction

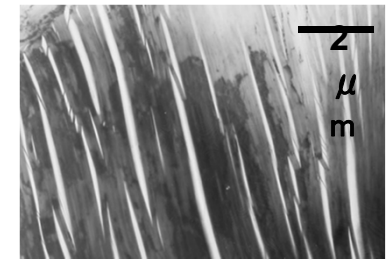
Shrinkage of CSF Graphite Irradiated at 800°C to various Irradiation Doses



Longitudinal direction

Increasing dose

Gilsocarbon Dimensional Changes



Gilsocarbon Dimensional change

Mrozowski cracks

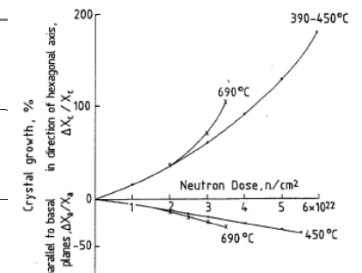
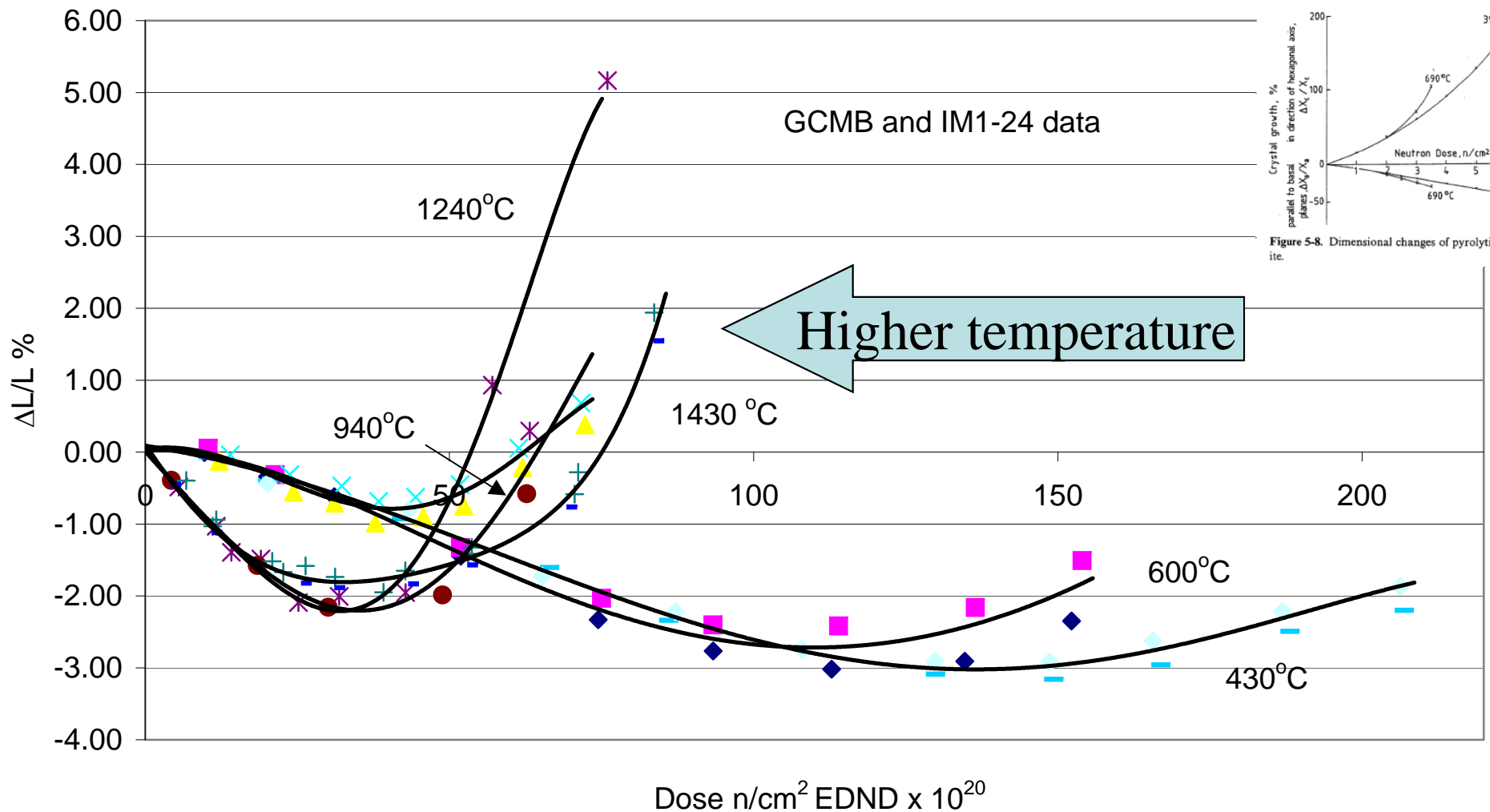
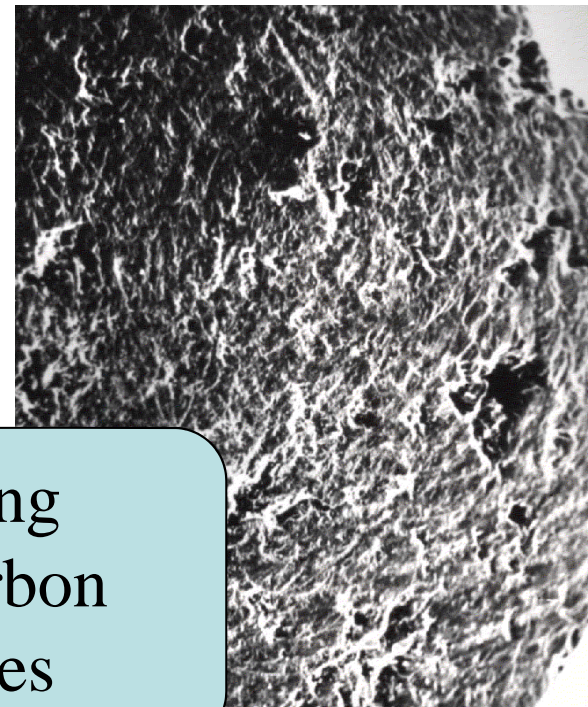


Figure 5-8. Dimensional changes of pyrolytic graphite.



Unirradiated Gilsocarbon Specimens

7mm long by
m di



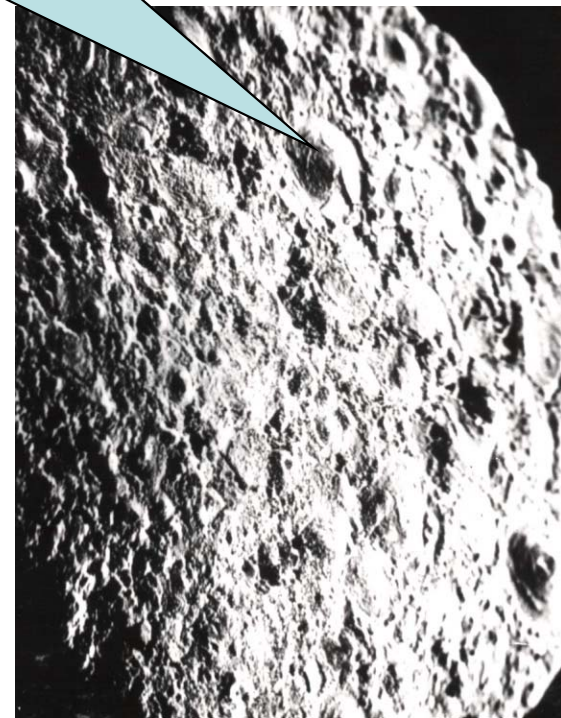
Swelling Gilsocarbon particles

Swelling Gilsocarbon particles



$285 \times 10^{20} \text{ n/cm}^2$
EDND

+0.9% $\Delta V/V_0$

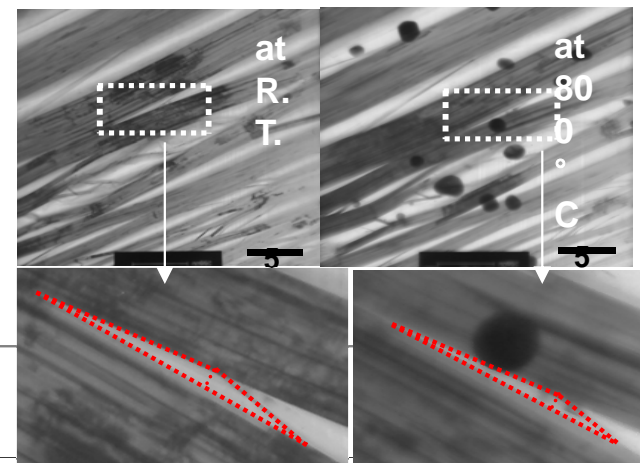
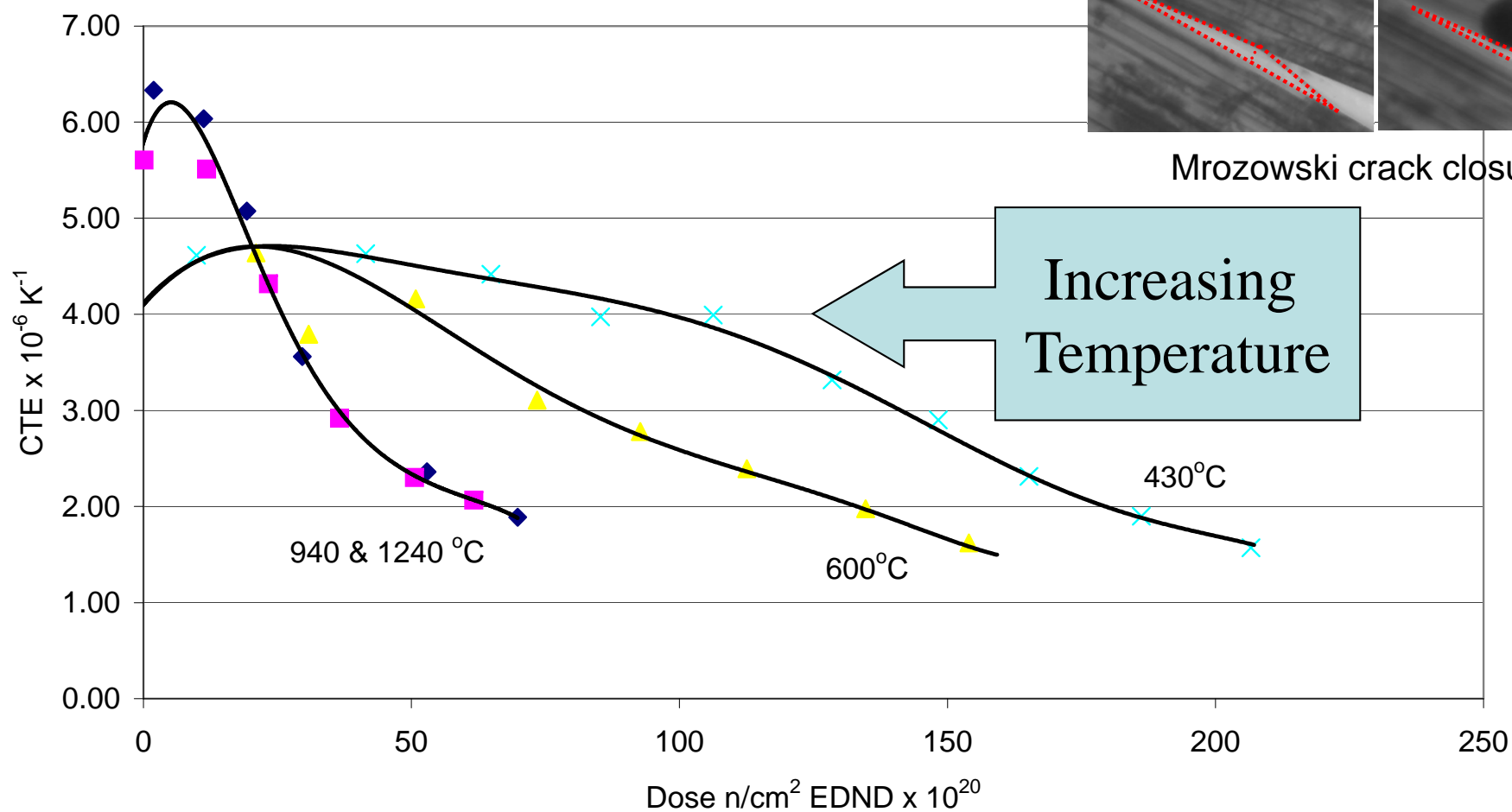


Gilsocarbon irradiated to $271 \times 10^{20} \text{ n/cm}^2$
EDND 33% $\Delta V/V_0$



Gilsocarbon Coefficient of Thermal Expansion

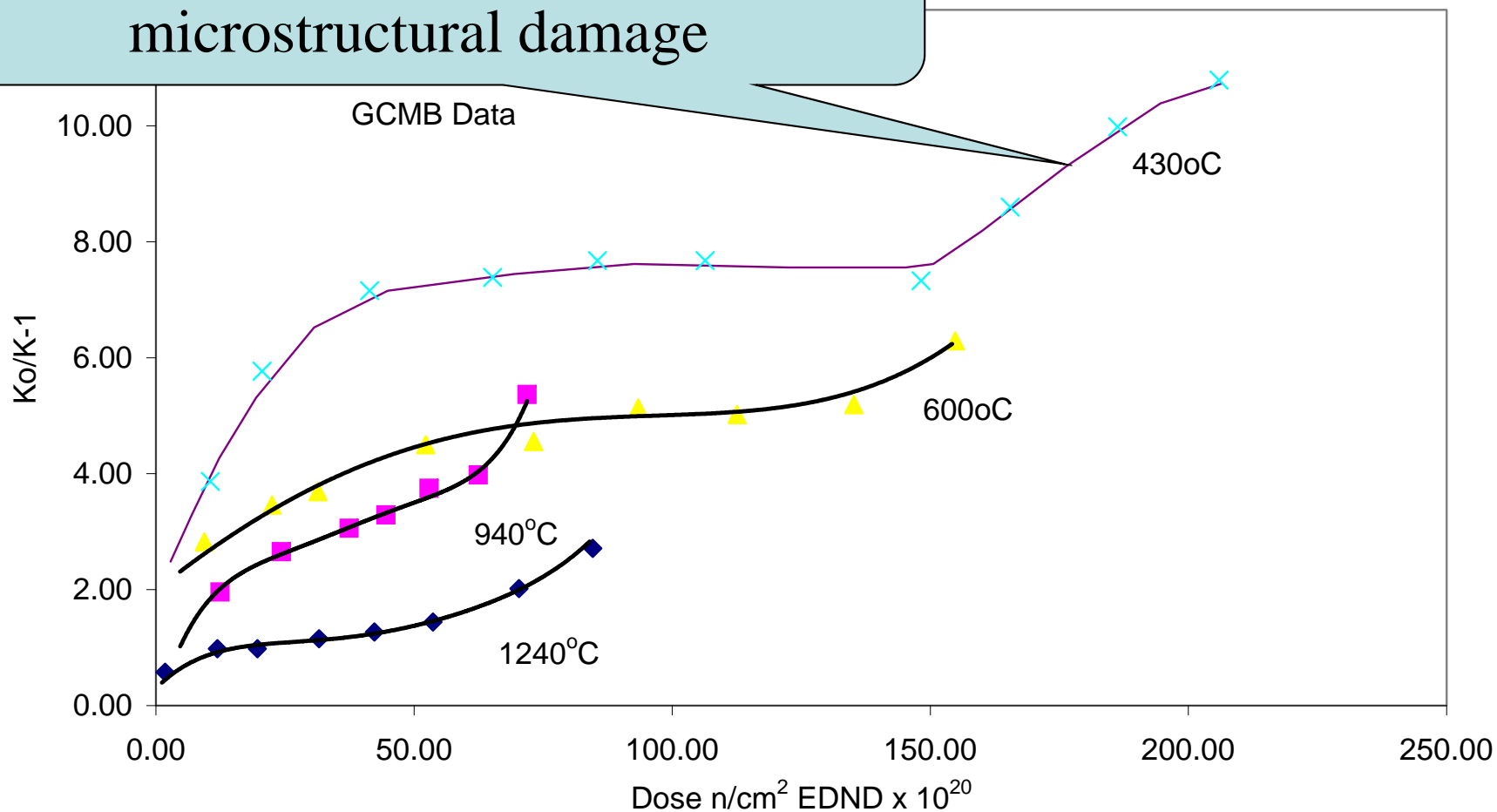
Gilsocarbon Coefficient of Thermal Expansion



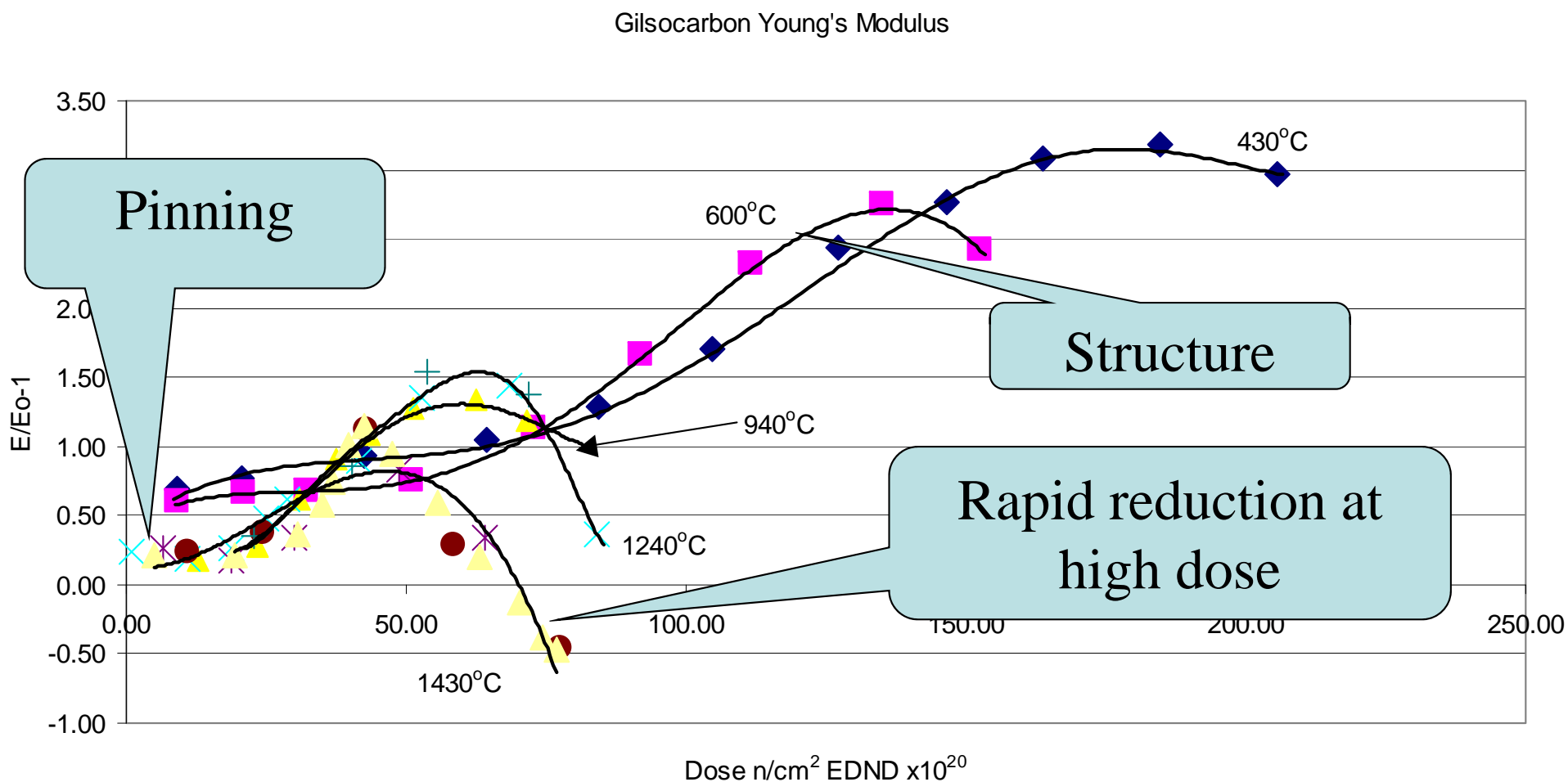
Mrozowski crack closure

Gilsocarbon Thermal Resistivity

High dose secondary increase due to microstructural damage



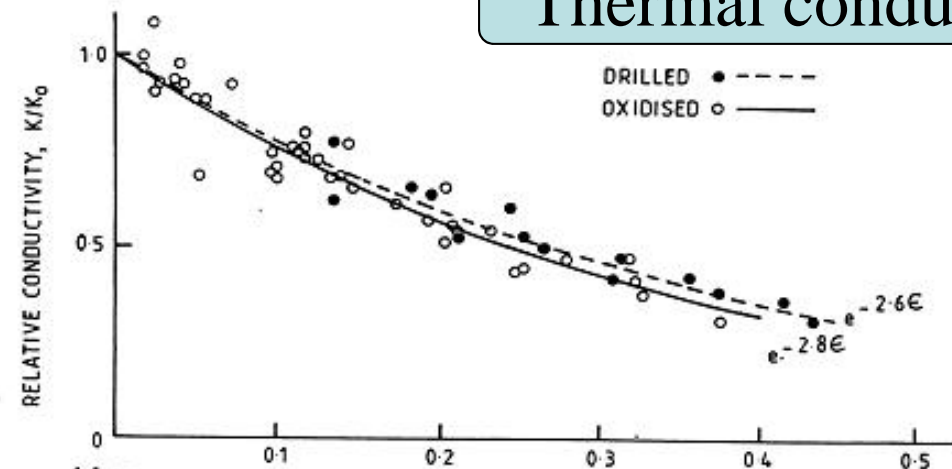
Gilsocarbon Change Young's Modulus



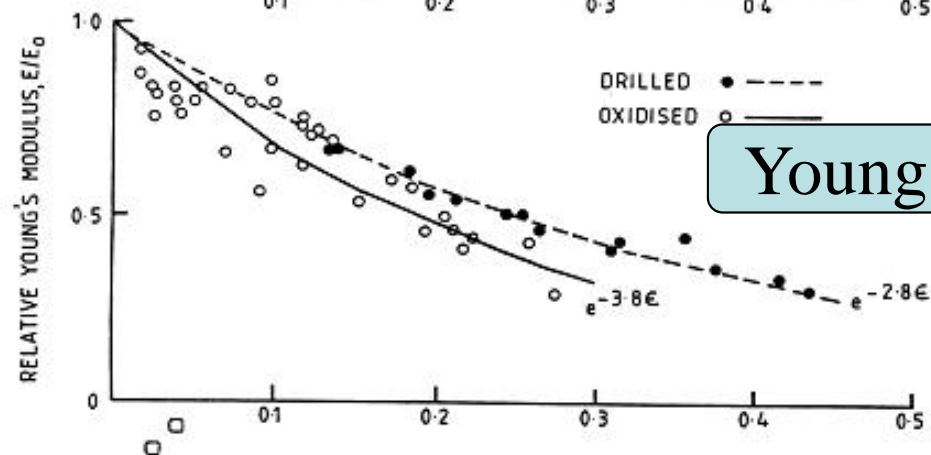
Reduction in properties due to radiolytic oxidation

- The black symbols are drilled specimens indicating the loss of section is a major factor

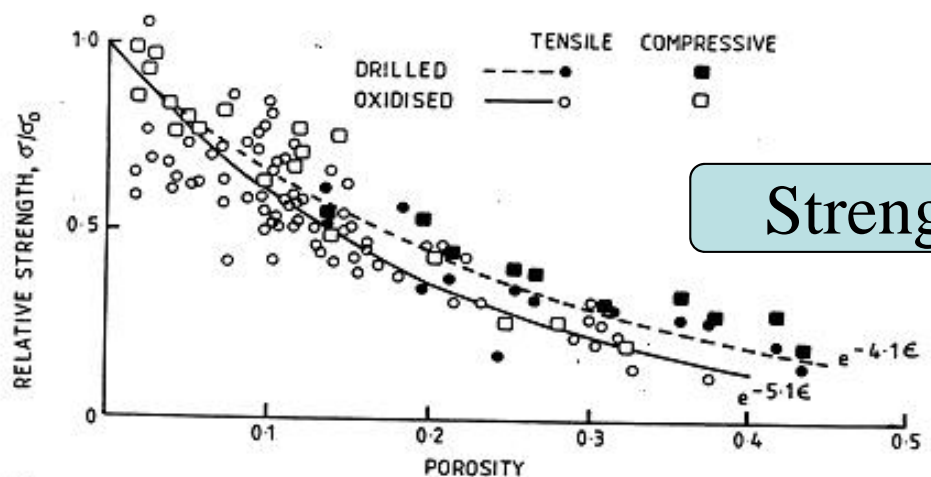
Thermal conductivity



Young's modulus



Strength



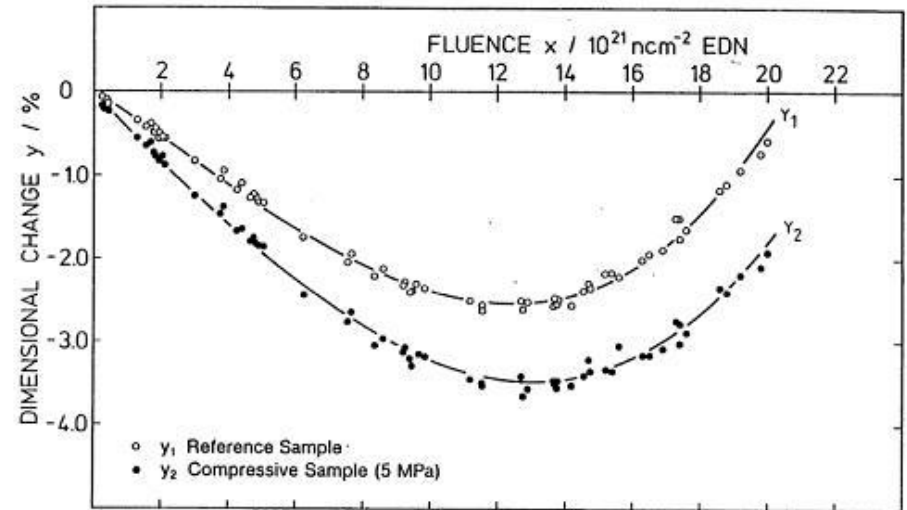
Irradiation Creep in Graphite

- Due to fast neutron irradiation
- Significantly reduces stresses in nuclear graphite components
- Definition
 - The difference in dimensions between a stressed sample and a sample having the same properties as that sample when unstressed

Dimensional Change Under Load

Example ATR-2E Graphite

- Under compressive load shrinkage is increased
 - Upper right
- Under tensile load shrinkage is decreased
 - Lower right
- There is also a lateral (Poisson's) effect
 - Below



DIMENSIONAL CHANGES OF ATR-2E AT 500°C UNDER COMPRESSIVE LOAD

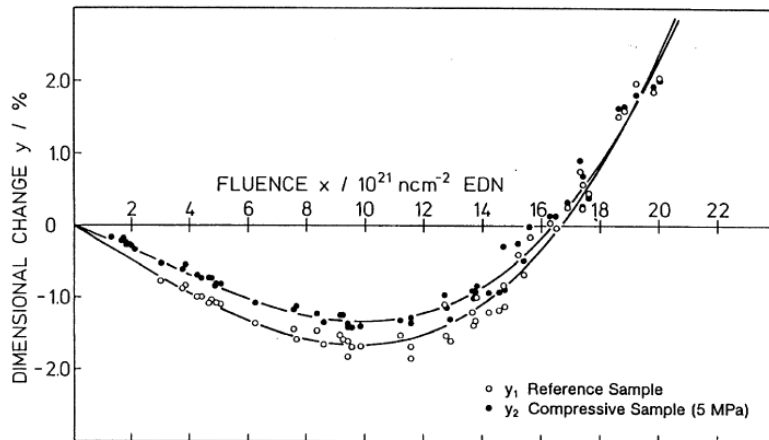
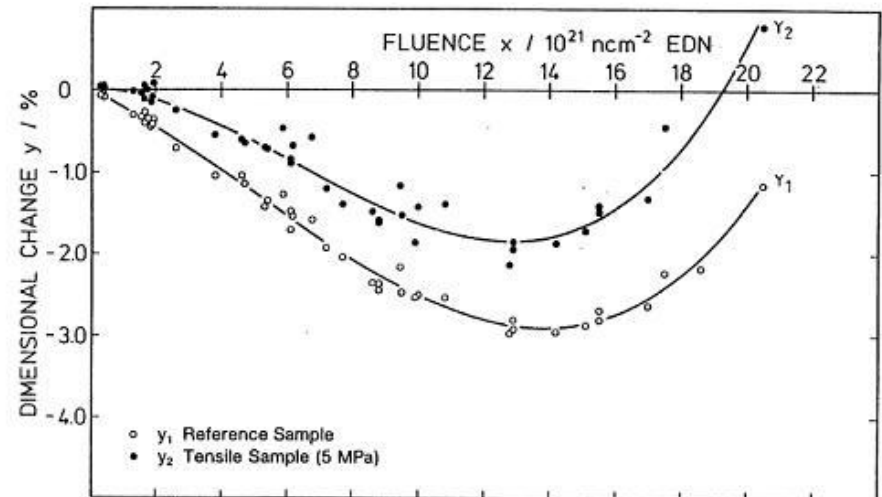


FIG. 18. DIMENSIONAL CHANGES OF ATR-2E AT 500°C UNDER COMPRESSIVE LOAD (TRANSVERSE DIRECTION) (REF. 37)

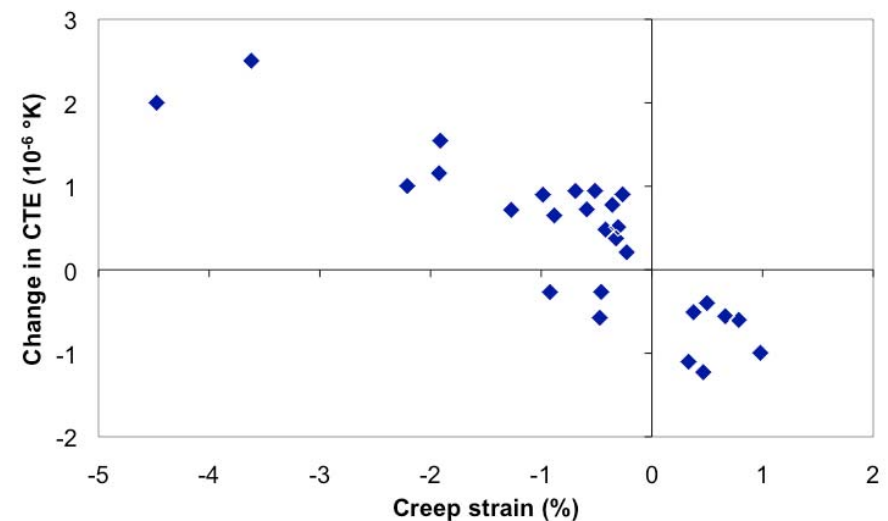
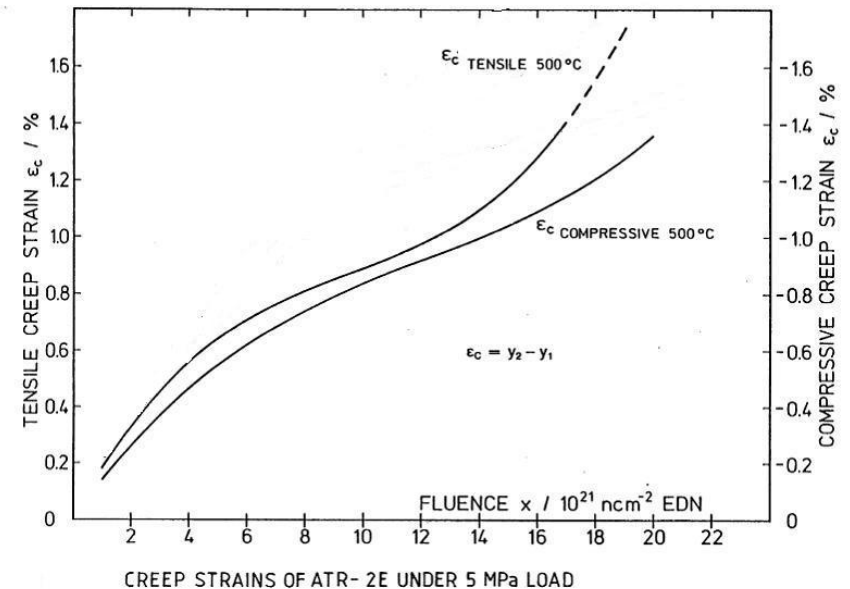


DIMENSIONAL CHANGES OF ATR-2E AT 500°C UNDER TENSILE LOAD

Irradiation Creep Curves

Example ATR-2E (500°C)

- Irradiation creep curve can be simply obtained by subtraction of the unloaded dimensional change curve from the crept dimensional change curve
- However, for assessments this would require data for a range of temperatures and fast neutron fluence covering all the expected conditions.
- In addition changes to the Coefficient of Thermal Expansion (CTE) and Young's modulus have been observed.



Issues to consider

- Properties
 - thermal conductivity
 - thermal shock resistance
 - modulus of elasticity
 - tensile strength
 - CTE
 - dimensional change & irradiation creep
 - initial compressive stress
- Protons versus neutrons
 - dose rate effect (pulsed versus continuous)
 - helium production
- POCO
 - historical experience