

Titanium Alloy Radiation Damage Tests

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²Facility For Rare Isotope Beams

May 19, 2015

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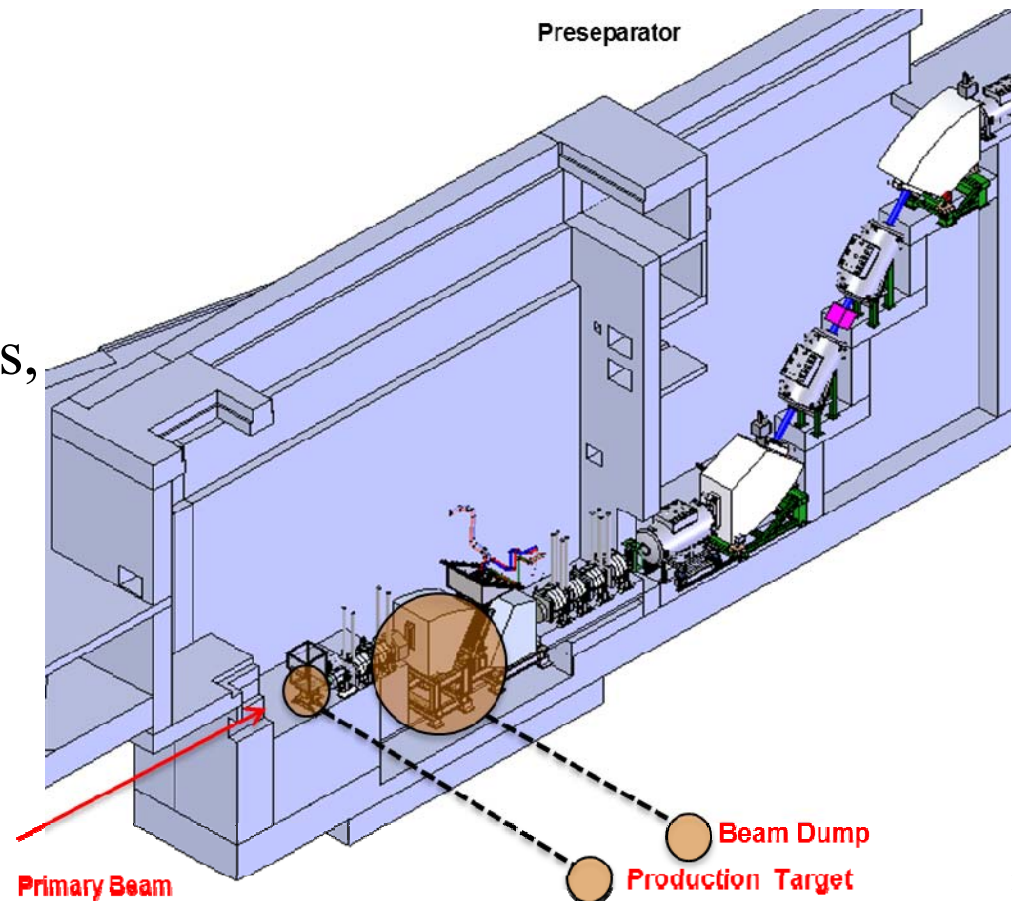
**FACILITY FOR
RARE ISOTOPE BEAMS**

Outline

- 1. Introduction**
- 2. Microstructure characterization**
- 3. Experimental Methods**
- 4. Irradiation damage in Ti-6Al-4V: Literature review**
- 5. Microstructure characterization**
- 6. Hardness measurements**
- 7. Conclusion**

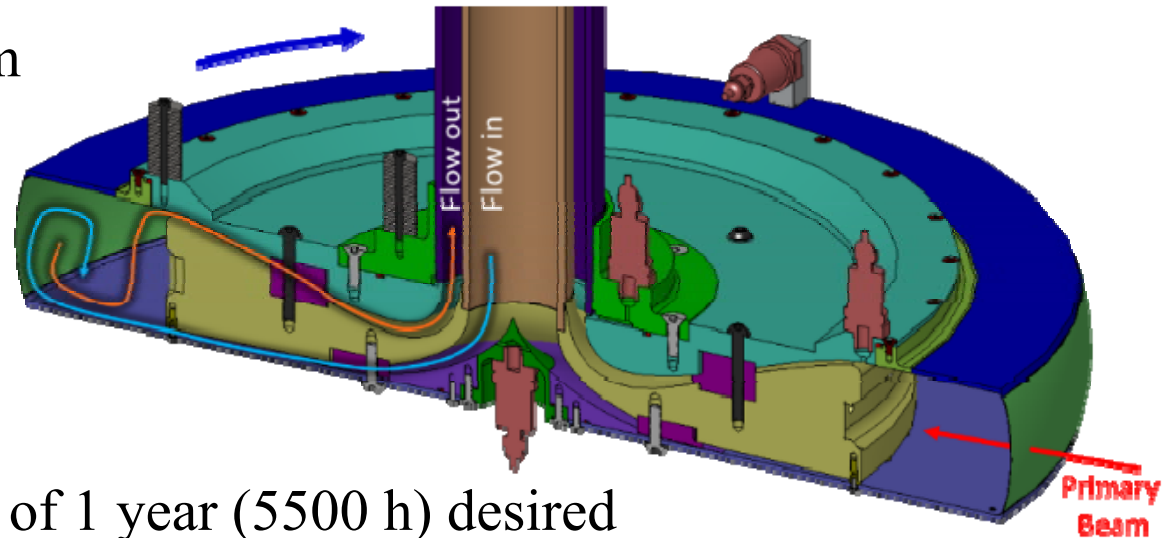
Facility for Rare Isotope Beams at Michigan State University

- The FRIB at Michigan State University is a new generation accelerator with high power heavy ion beams.
- It will provide primary beams from O to U with an energy of 200 MeV/u for heavy ion beams, and higher energies for lighter beams.
- Beam Dump
 - Up to 325 kW



FRIB Beam Dump

- Water-filled rotating drum beam dump chosen for FRIB baseline



- FRIB conditions:
 - Beam Dump lifetime of 1 year (5500 h) desired
 - Estimated cumulative dpa after one year of use ~ 9 dpa with a fluence of 10^{15} ions.cm⁻²
 - Se from 0.08 keV/nm (with O beam) to 12.6 keV/nm (with U beam)
 - Ti-6Al-4V and Ti-6Al-4V-1B were chosen as candidate materials
 - The current study addresses the radiation damage challenge and focuses on understanding Swift Heavy Ion (SHI) effects on Ti-alloy that can limit beam dump lifetime



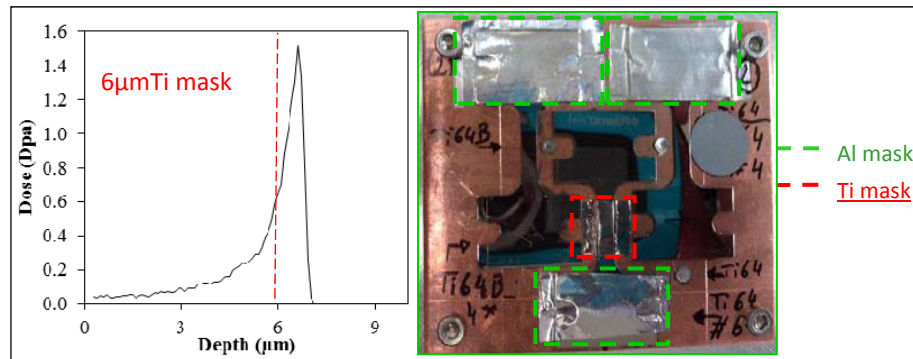
Irradiation set up



- Two main irradiation experiments with Ti-6Al-4V and Ti-6Al-4V-1B samples were performed at the IRRSUD beamline facility at the GANIL-CIMAP Laboratory, Caen France.
- The IRRSUD beam line was chosen due to comparable S_e values to the FRIB conditions (0.08 -13 keV.nm⁻¹) without the activation of the sample (> coulomb barrier)

Beam	Energy (MeV/u)	Ranges (μm)	S_e (keV.nm ⁻¹)	Temperature (°C)	Fluence (ions.cm ⁻²)
³⁶ Ar	1	6.8	7.5	25 - 350	10 ¹⁵
¹³¹ Xe	1.4	8.5	19.7	25 - 350	2-7. 10 ¹⁴

The SRIM-2013 calculation of the dose in a Ti-6Al-4V sample for the ³⁶Ar @36 MeV beam with a fluence of 10¹⁵ ions.cm⁻²



Irradiation set up



Ti-alloys irradiations at CIMAP and NSCL

Facilities	Beam	Energy [MeV]	Range [μm]	S_e [keV/nm]	Fluence [ions/cm ²]	Max dpa in sample	Date	Number of samples	Type
IRRSUD	⁸² Kr	25	4.73	9.9	5.10 ¹¹ - 5.10 ¹² - 2.10 ¹⁴	0.6	Jul-2013	6	Foils
	¹³¹ Xe	92	8.5	19.7	2.10 ¹¹	0.001	Jul-2013	2	Foils
	⁸² Kr	45	6.43	13.1	5.10 ¹¹ - 5.10 ¹³	0.16	Jul-2013	4	Foils
	⁸² Kr	45	6.43	13.1	2.10 ¹⁴ 2.5.10 ¹⁵	8	Oct-2013	6	Foils
	³⁶ Ar	36	6.8	7.5	10 ¹⁵	1.5	Dec-2013	23	TEM and dogbone
	¹³¹ Xe	92	8.5	19.7	2 10 ¹⁴ 7 10 ¹⁴	3.5	June-2014	6	Dogbone
NSCL	⁴⁰ Ca	2000	800	1.5	6 10 ¹²	10 ⁻⁵	Aug-2013	1 x Ti64	Dogbone

FRIB conditions

- Estimated cumulative dpa after one year of use ~9 dpa with a fluence of 10¹⁵ ions/cm²
- S_e from 0.08 keV/nm (with O beam) and 12.6 keV/nm (with U beam)

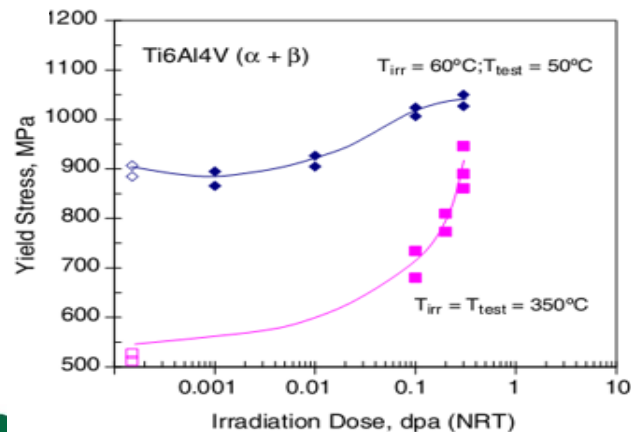


Irradiation damage in Ti-6Al-4V



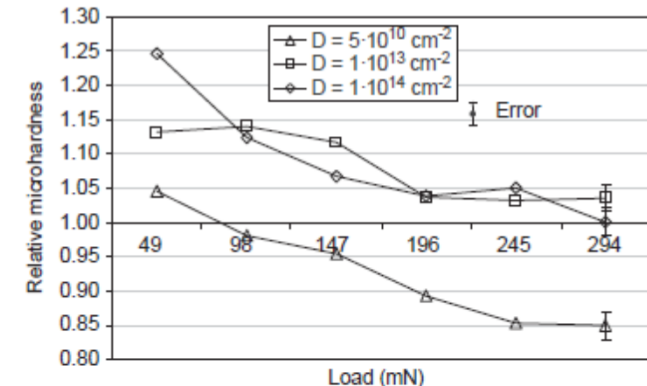
Effect of dose and temperature on the microstructure of **neutron** irradiated Ti-6Al-4V (Tähtinen *et al.*, Sastry *et al.*, Peterson)

Temperature and dose level	Microstructure change observations
50°C, 0.3 dpa	A high concentration of uniformly distributed defect clusters in the α -phase
350°C, 0.3 dpa	Dislocation loops Vanadium precipitates
450°C, Dose 2.1 and 32 dpa	Dislocation loops β -phase precipitates in α phase
550°C 32 dpa	Extensive void formation Coarse β -precipitates



Different hardening mechanisms operate at 50°C than at 350°C.

P. Budzynski, V. A. Skuratov, and T. Kochanski, "Mechanical properties of the alloy Ti-6Al-4V irradiated with swift Kr ion," *Tribol. Int.*, vol. 42, no. 7, pp. 1067–1073, Jul. 2009.



Relative micro-hardness in Ti-6Al-4V irradiated with swift 250MeV Kr⁺²⁶ at different fluences



Dose dependence of yield strength of Ti-6Al-4V irradiated with neutrons

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Tähtinen *et al.* / *Journal of Nuclear Materials*, 367-370 (2007), 627–632

Sastry *et al.* / *Fourth International Conference on Titanium*, Kyoto, Japan, 1980, vol. 1, p. p. 651.

D.T. Peterson, / *Effects of Radiation on Materials: 11th International Symposium*, Philadelphia, PA, 1982, p. p. 260.

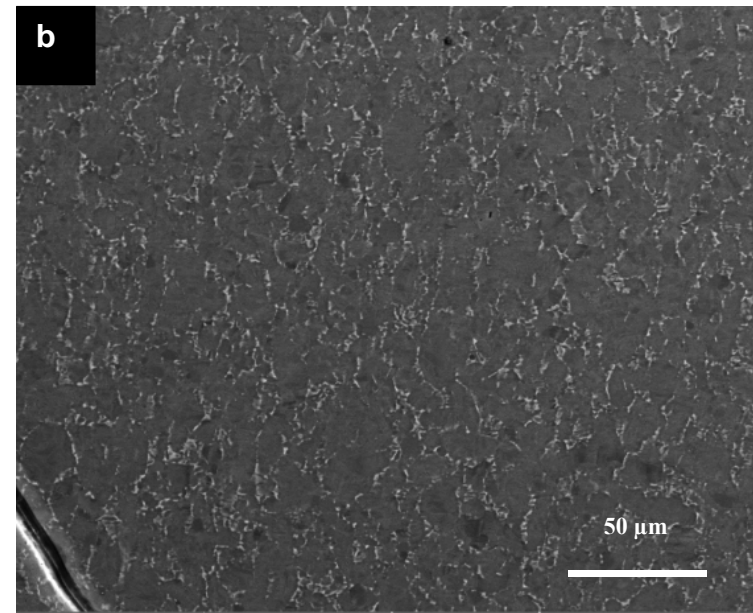
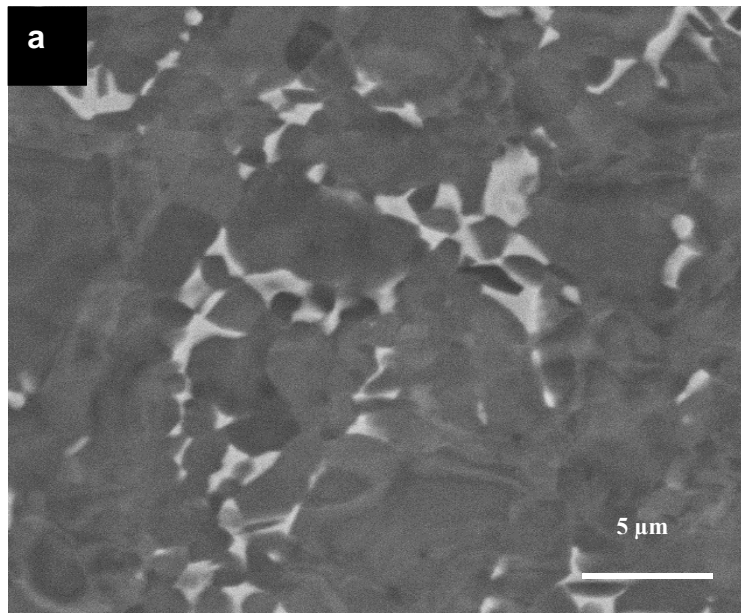
Microstructure of the as-received materials

Ti-6Al-4V:

Lenticular α -phase with mostly an intergranular β -phase. Intra-granular β -phase was also observed.

The volume fraction of the β -phase was ~ 6.6 vol.% and the α -phase ~ 93.4 vol.%.

The grain size of the α -phase ranged between $5 \sim 20 \mu\text{m}$.



BSE images of the initial microstructure of Ti-6Al-4V (a) higher and (b) lower magnification

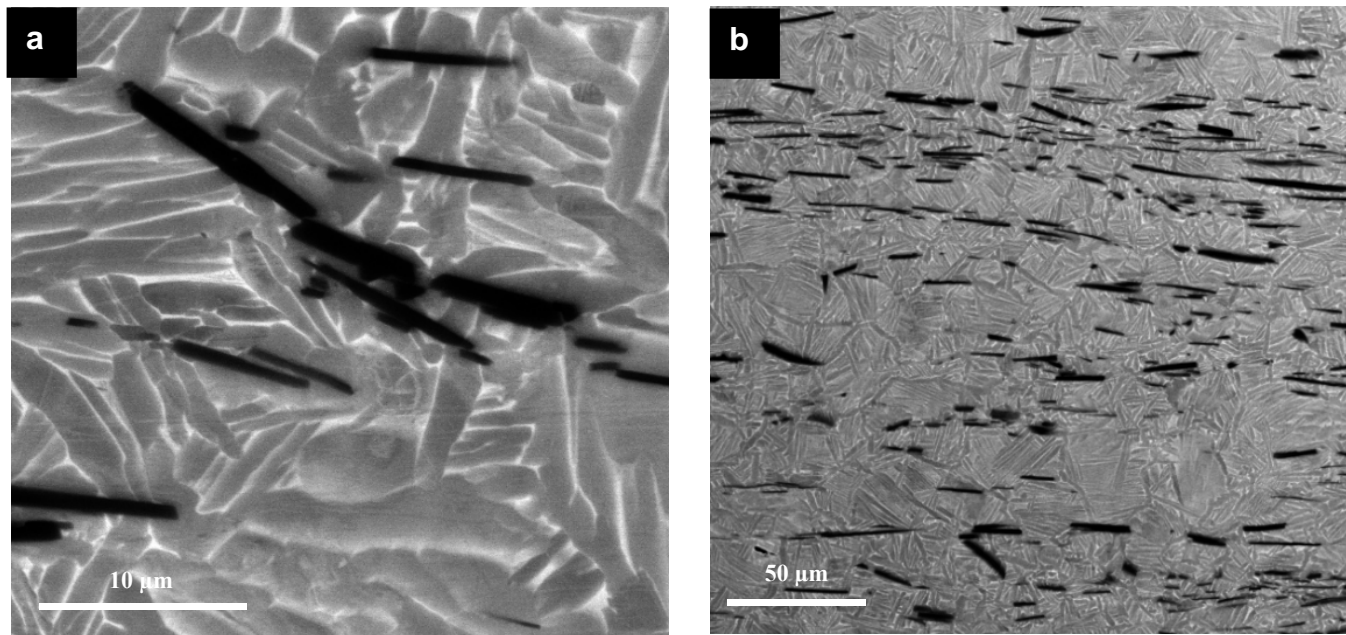


Microstructure of the as-received materials

Ti-6Al-4V-1B

The microstructure contained both an equiaxed ($7.4\mu\text{m}$) and lenticular α -phase; total volume percent α -phase was $\sim 79\%$.

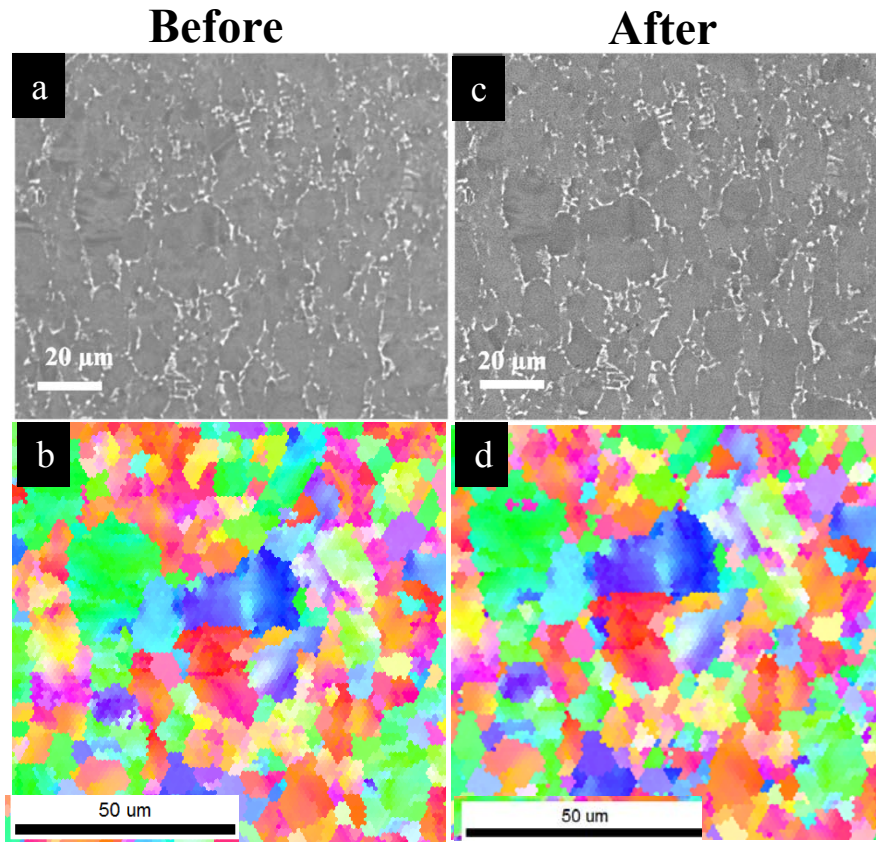
The β -phase volume percent was ~ 15 vol.% while the TiB phase volume percent was ~ 5.9 vol.%(Chen *et al.*)



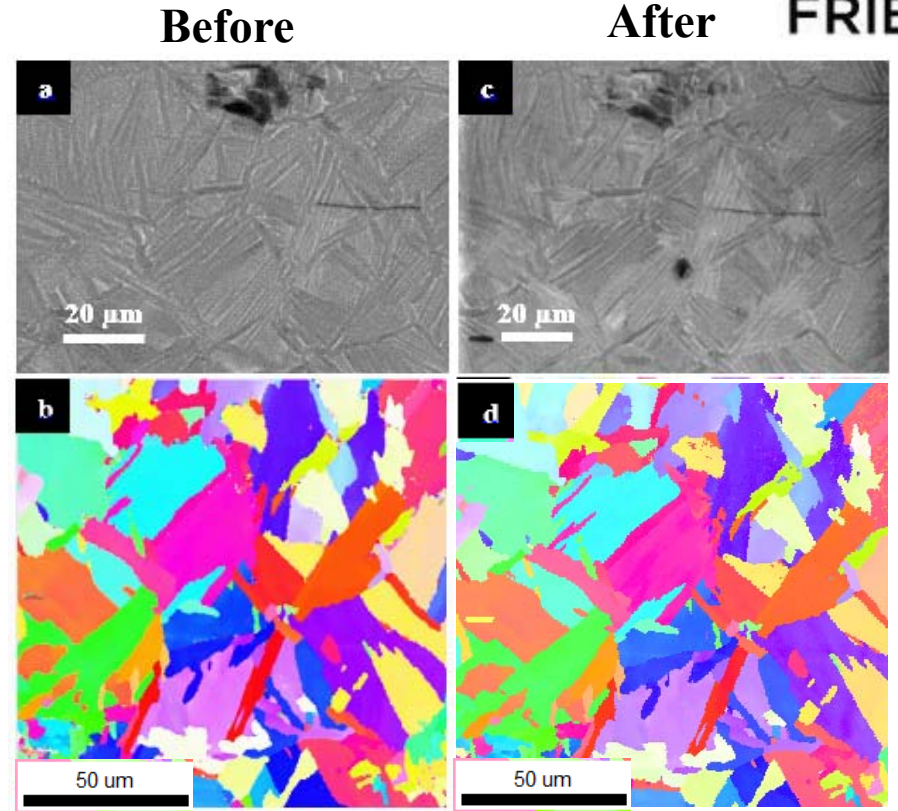
BSE images of the initial microstructure of Ti-6Al-4V-1B (a) higher and (b) lower magnification

W. Chen et al / *Key Eng. Mater.*, vol. 436, pp. 195–203, May 2010.

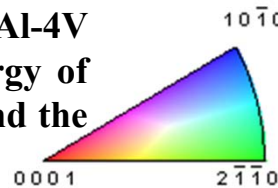
Microstructure Characterization



BSE images and IPF maps before (a,b) and after irradiation at the same area (c,d) in a Ti-6Al-4V sample irradiated with ^{131}Xe with an energy of 92 MeV. The fluence was $2 \cdot 10^{14}$ ions. cm^{-2} and the temperature 25°C



BSE images and IPF maps before (a,b) and after irradiation at the same area (c,d) in a Ti-6Al-4V-1B sample irradiated with ^{36}Ar with an energy of 36 MeV. The fluence was $1 \cdot 10^{15}$ ions. cm^{-2} and the temperature 350°C



➤ **No change in microstructure or grain orientation at the surface.**



Hardness measurements

Nano-indentation

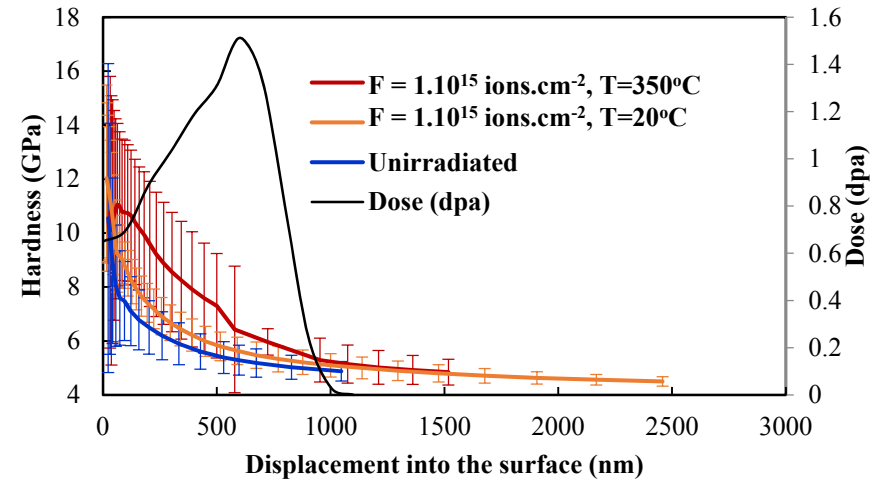
Obtain the properties of the materials in depth.



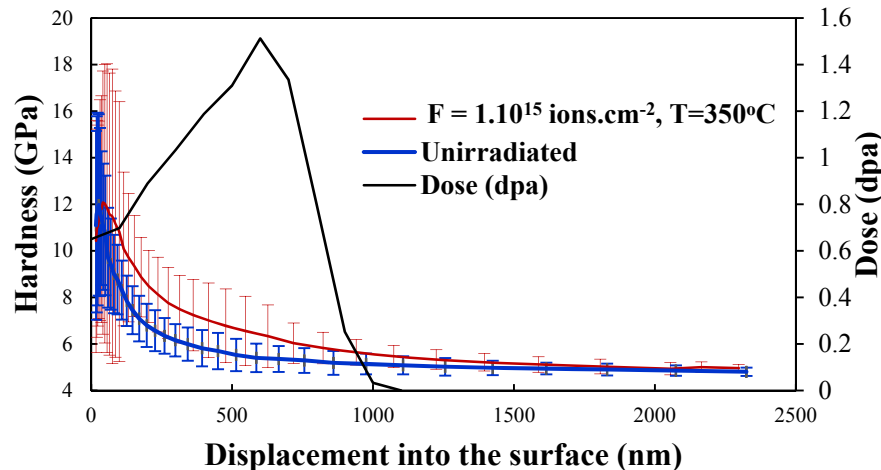
Parameters:

- Berkovich tip
- Strain rate : 0.05s^{-1}
- Poisson ratio=0.33
- Distance between indents: $50\mu\text{m}$

Ti-6Al-4V



Ti-6Al-4V-1B



Nano-indentation results for Ti-6Al-4V and Ti-6Al-4V-1B irradiated with ^{36}Ar @36 MeV at fluence of 1.10^{15} ions. cm^{-2} with the CP-Ti foil on the surface.

Boron addition to Ti-6Al-4V did not change its irradiation resistance

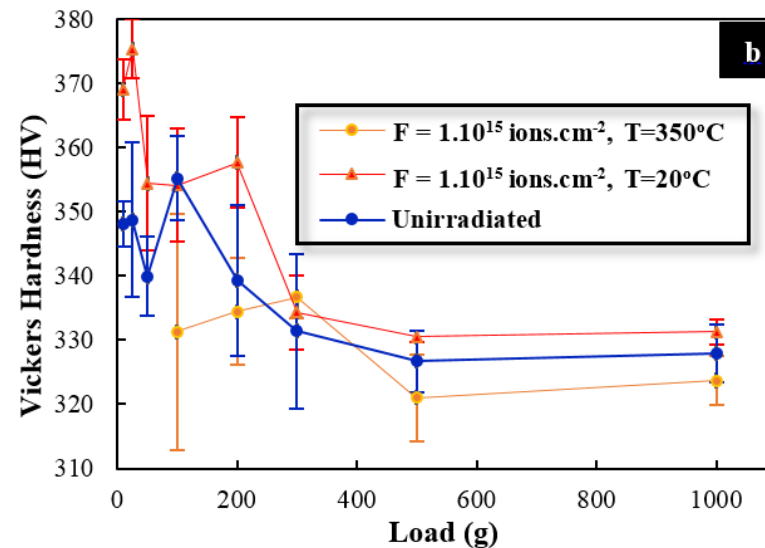
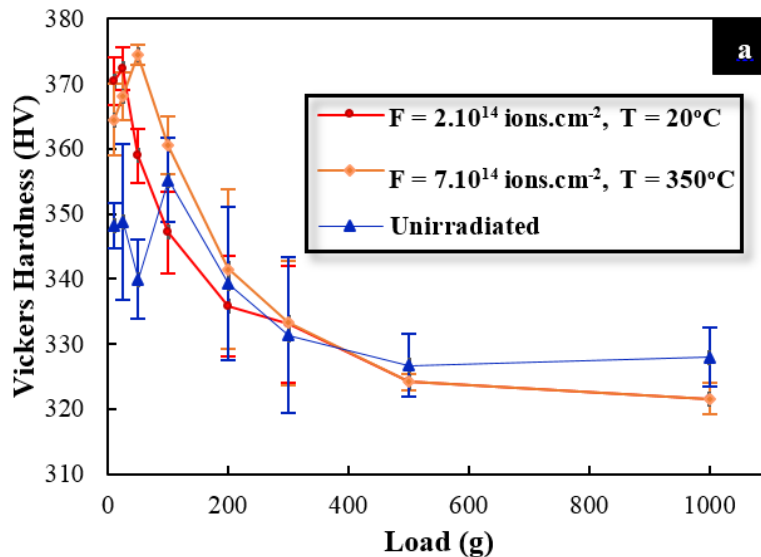
- A slight increase in hardness observed for the sample irradiated with a higher fluence (1.10^{15} ions. cm^{-2}) and lower temperature ($T = 350^\circ\text{C}$) for the higher doses



Hardness measurements

Vickers Hardness

- Vickers hardness was performed on 4 irradiated Ti-6Al-4V samples.



Vickers Hardness measurements for Ti-6Al-4V irradiated with: a) ¹³¹Xe @ 92 MeV and b) ³⁶Ar @ 36 MeV

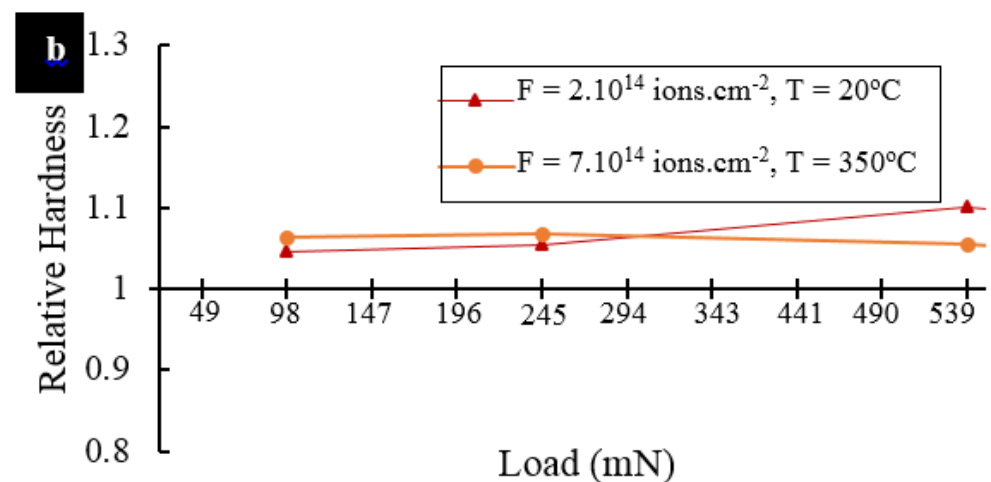
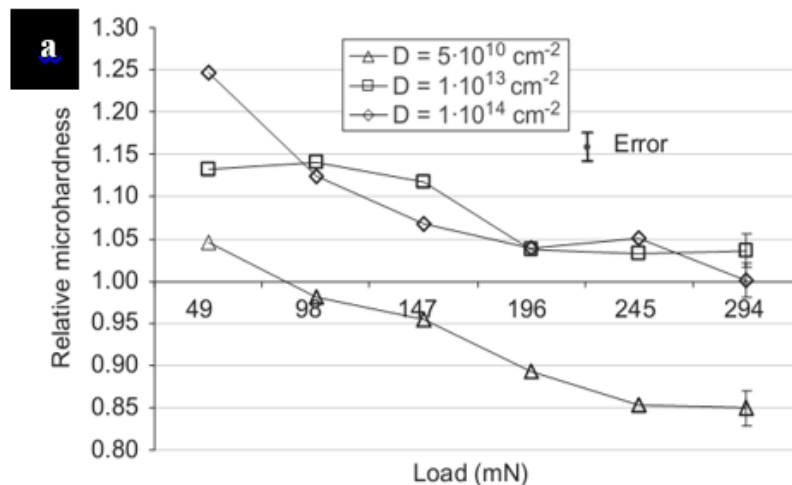
- The large scatter is due to the presence of two phases in the material
- A slight increase in hardness was observed for the sample irradiated with a higher fluence at lower loads (< 50g) (depth~ 1.6μm)



Hardness measurements

Vickers Hardness

- The lower irradiation damage observed in our investigated Ti-6Al-4V samples compared to results reported by Budzynski et al. (2009) could be explained by
 - The difference in microstructure: larger grains ($\sim 100\mu\text{m}$)
 - The gs was $5\text{-}20\mu\text{m}$ in our material and gbs act as sinks for radiation-induced-effects



Relative micro-hardness of the Ti-6Al-4V alloy as a function of applied load for Ti-6Al-4V irradiated with: a) Kr⁺²⁶@350 MeV (Budzynski et al. 2009) and b) ¹³¹Xe @ 92 MeV.

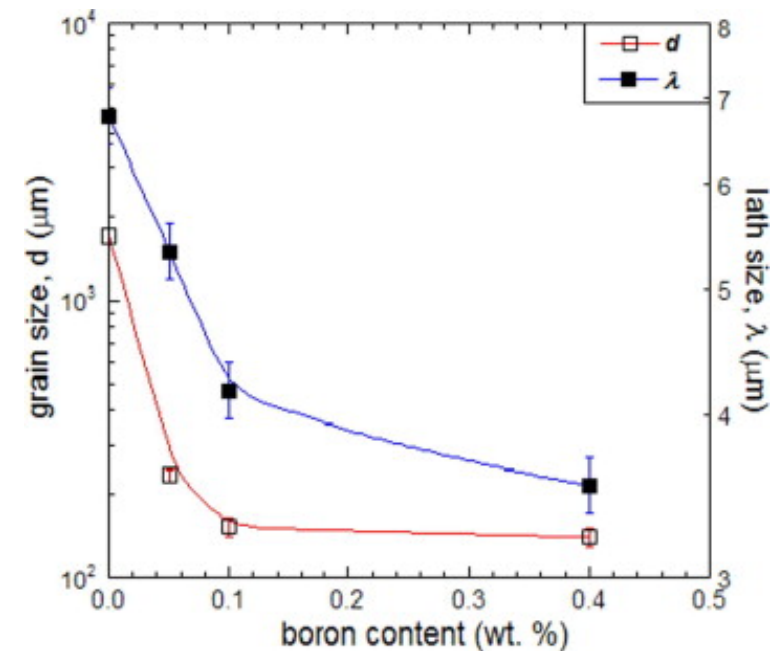
P. Budzynski, V. A. Skuratov, and T. Kochanski, "Mechanical properties of the alloy Ti-6Al-4V irradiated with swift Kr ion," *Tribol. Int.*, vol. 42, no. 7, pp. 1067-1073, Jul. 2009.



Discussion



- Effect of the microstructure in the irradiation resistance of this Ti-alloy.
- Effect of the small grains (5-20 μm)
- Boron addition causes grain refinement
- Thermomechanical processing can improve its properties



Variation of prior β grain size, d , and the α lath size, λ , in Ti64 with wt.% B addition (Sen *et al.*)



Conclusion

- The analyzed hardness and nano-indentation suggest a higher irradiation damage resistivity in the two studied Ti-alloys than reported in literature for Ti-6Al-4V.
- Slight differences in the microstructure caused by the thermomechanical processing may be responsible for this difference.
- 1% boron addition to Ti-6Al-4V didn't degrade the radiation resistance
- Ongoing and Future work:
 - ❖ Irradiation creep test
 - ❖ In-situ tensile tests and slip trace analysis: Deformation mechanisms
 - ❖ X-ray diffraction: Investigate phase transformation
 - ❖ Effect of the microstructure on the irradiation damage in Ti-alloys



Acknowledgements

- MSU Department of Chemical Engineering and Material Science
- FRIB
 - Mikhail Avilov
 - Reginald Ronningen
- GANIL-CIMAP
 - Florent Durantel
 - Clara Grygiel
 - Isabelle Monnet
 - Florent Moisy
 - Marcel Toulemonde



Thank you for your attention

FRIB construction area – October 27 2014

