

# USPAS Course on Photocathode Physics

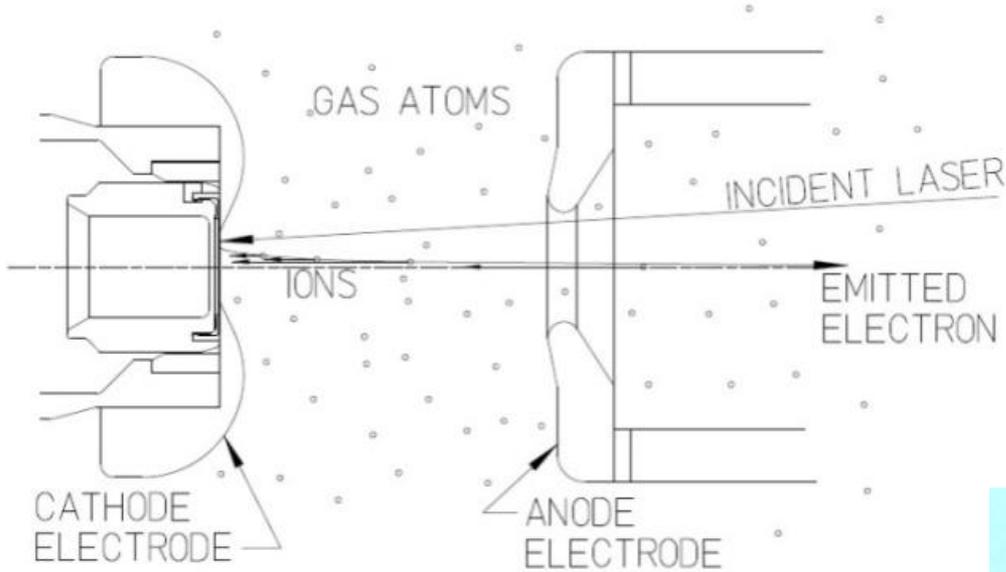
John Smedley, BNL and Matt Poelker, TJNAF

## Lecture 8 Practical Matters

## Lecture 8:

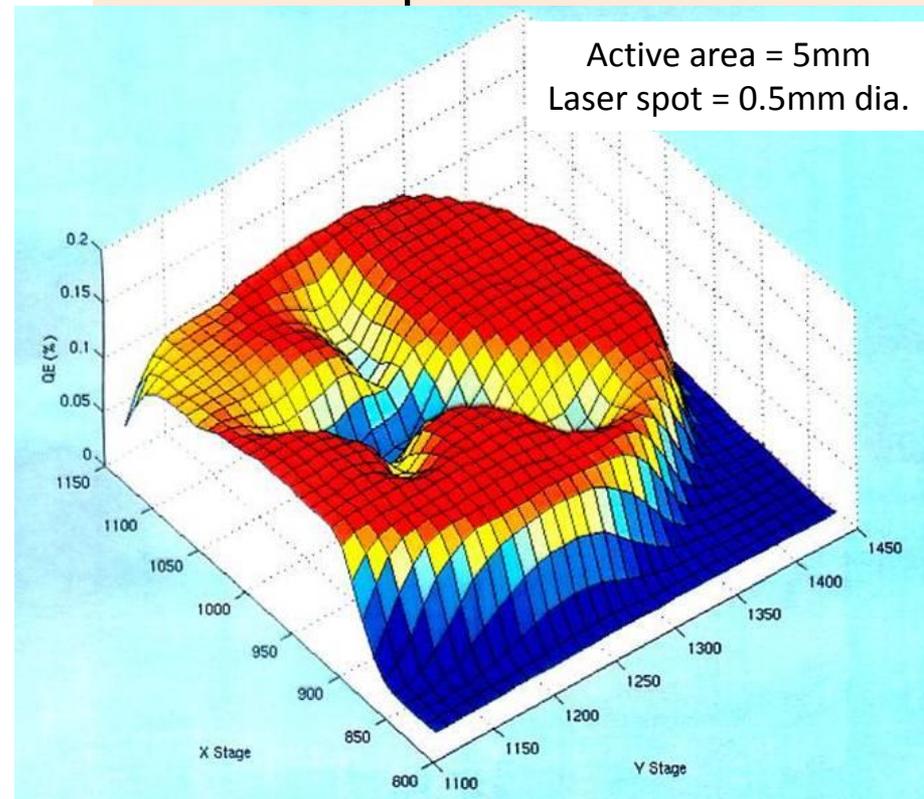
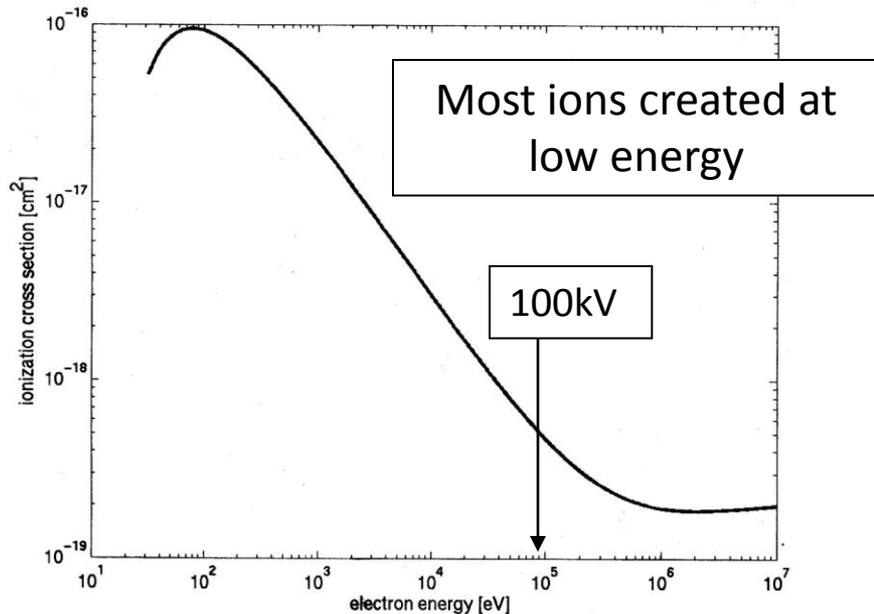
- Ion Bombardment
- High Voltage: avoiding breakdown and field emission
- A clean photocathode
- Vacuum Hot Filament Gauges

# Imperfect Vacuum = Finite Lifetime

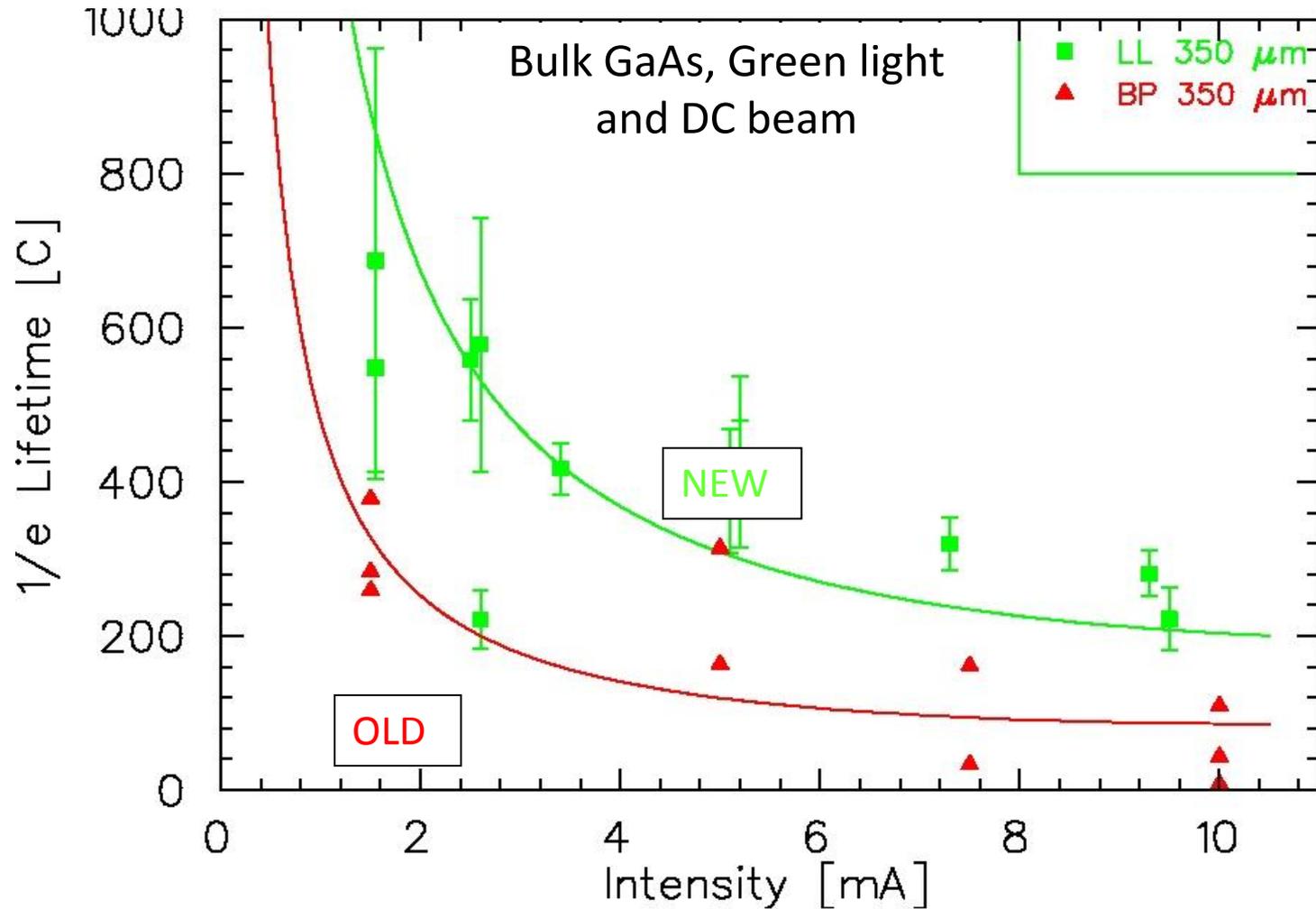


- What about while you run beam?
- Ion bombardment – notice characteristic “trench” from laser spot to electrostatic center of photocathode

Ionization cross section for H<sub>2</sub>



# Compare NEW and OLD load locked guns



**Better Vacuum in New Gun  $\rightarrow$  better Lifetime!**

# But Sometimes Lifetime is Still Not Good!!

✓ OK, good vacuum. What else matters?

❖ Clean laser beam, no stray light

❖ Good orbit, proper electron beam optics

❖ No field emission from cathode

➤ Reduce the active area of photocathode

➤ Move the laser away from the electrostatic center

➤ Increase the size of the laser beam

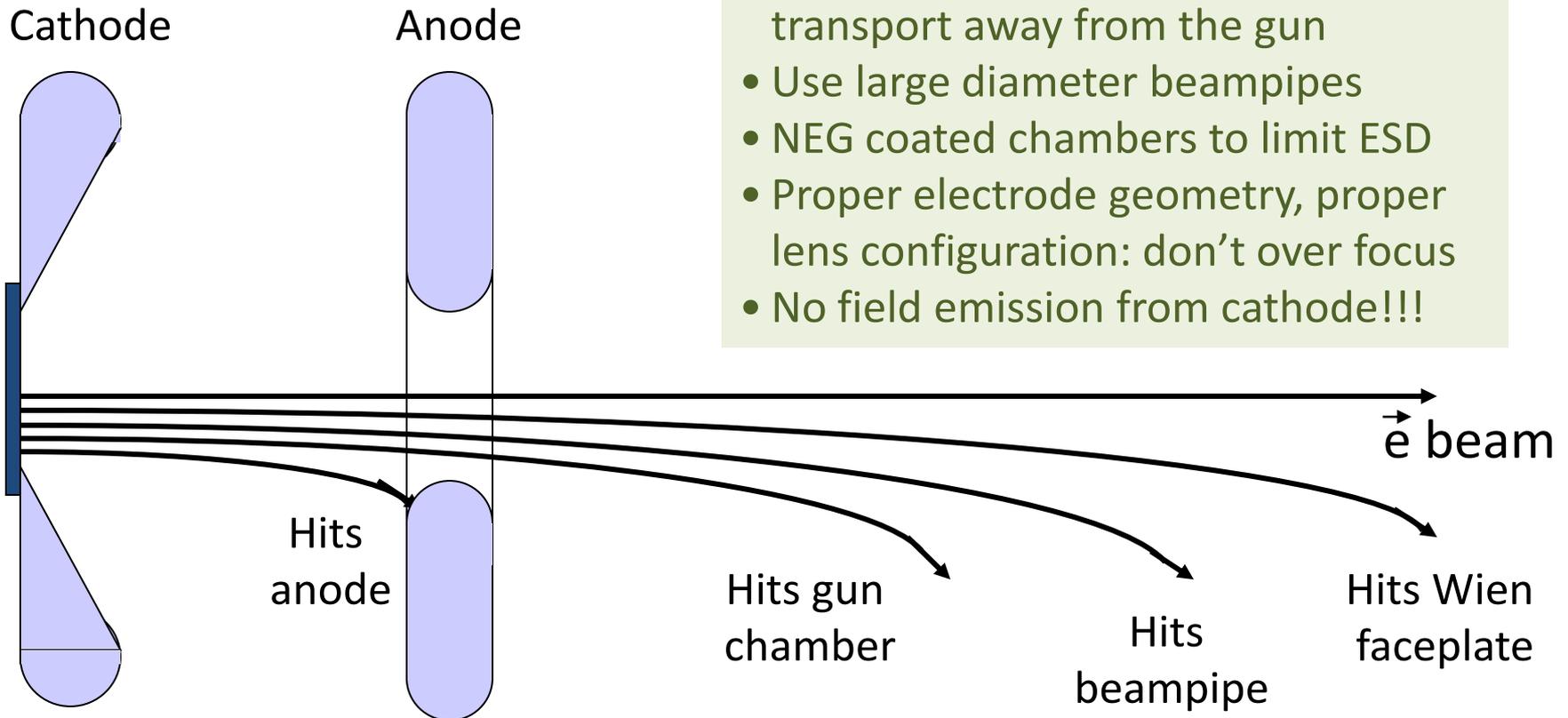
➤ Apply bias to the anode

➤ Operate at Higher Bias Voltage?

# Good beam versus Bad Beam

The beam that doesn't make it to the experiment only serves to degrade vacuum. This leads to ion-bombardment and QE decay

- Eliminate stray light
- Generate only electrons you can transport away from the gun
- Use large diameter beampipes
- NEG coated chambers to limit ESD
- Proper electrode geometry, proper lens configuration: don't over focus
- No field emission from cathode!!!

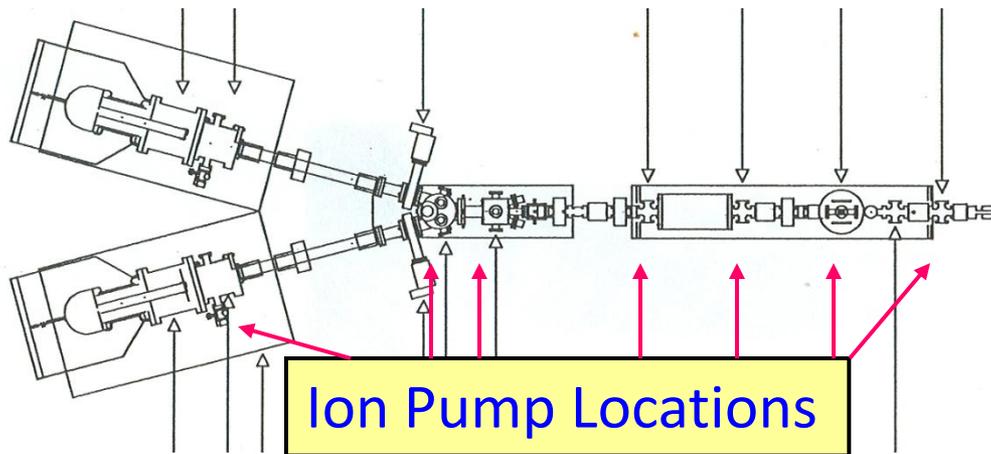


# “Free” beam loss monitoring

Designed and constructed by J. Hansknecht

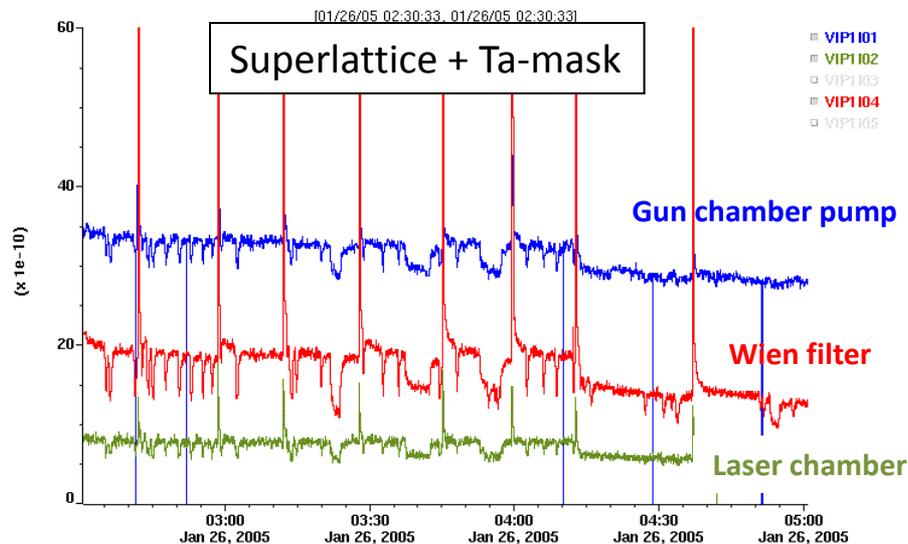
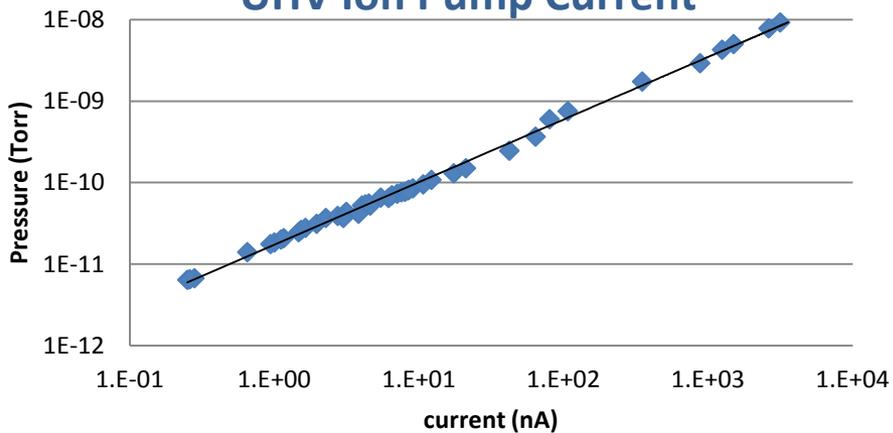


UHV Ion Pump Power Supplies

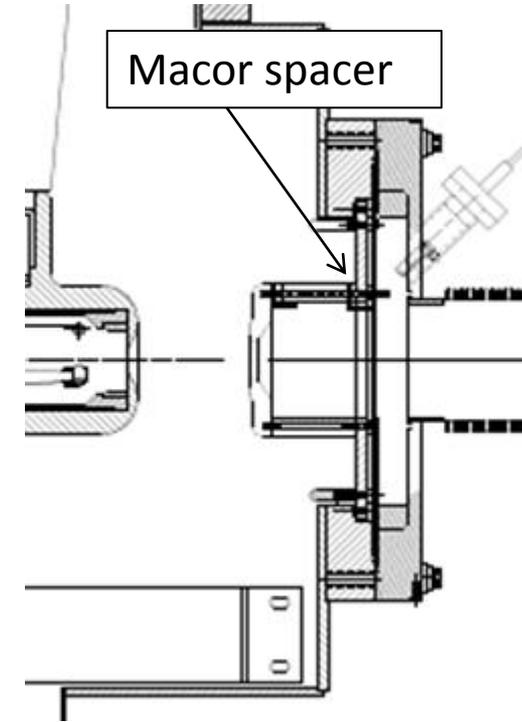
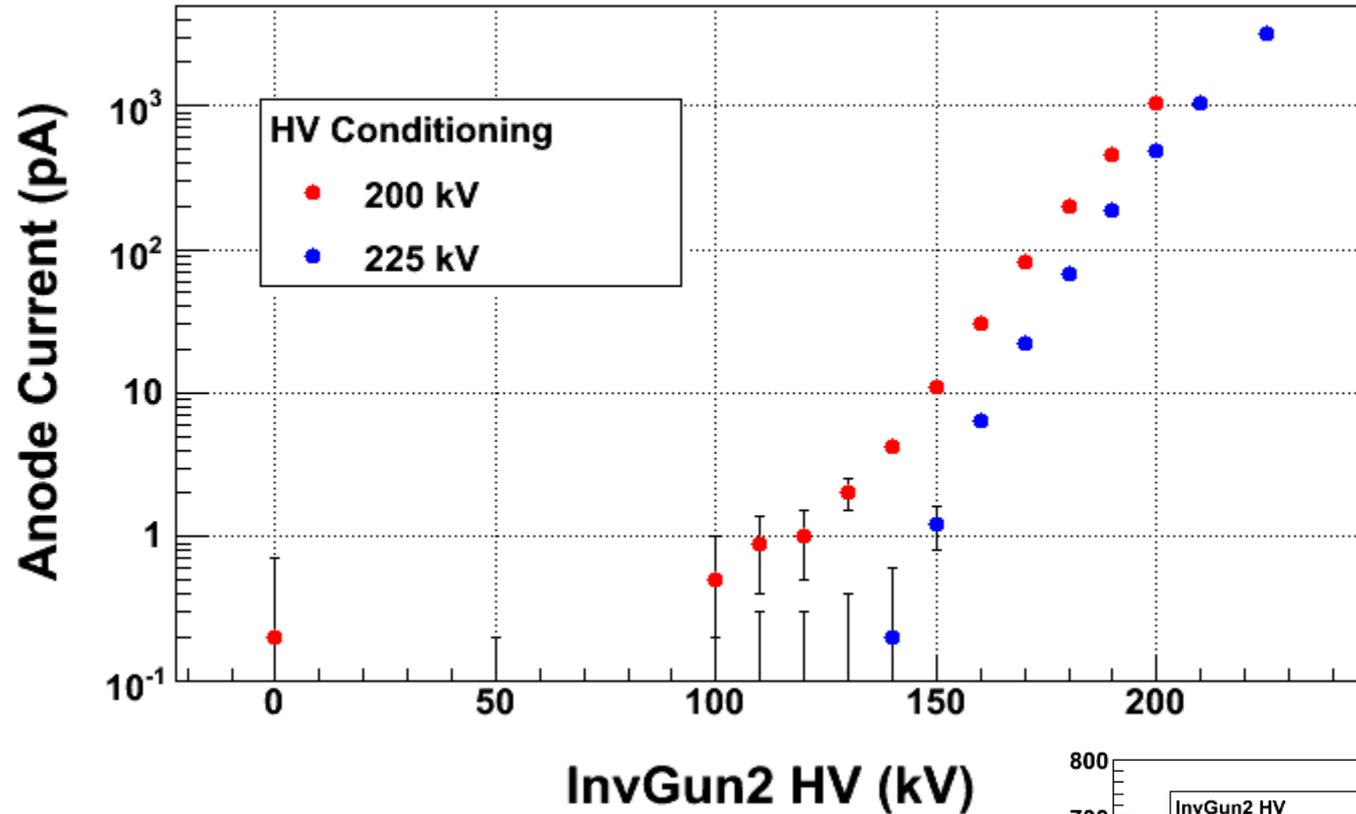


Ion Pumps detect bad orbit and beamloss

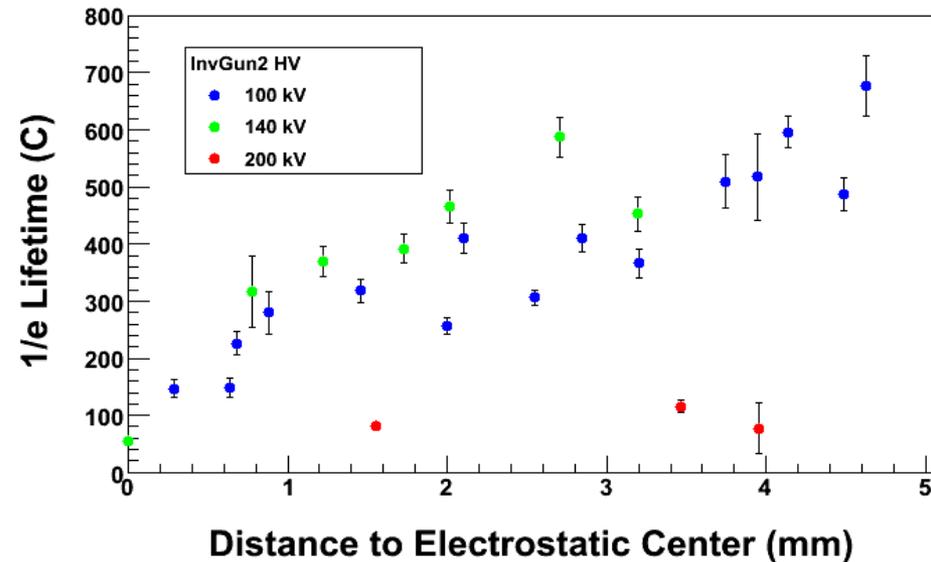
Extractor Gauge Pressure vs. UHV Ion Pump Current



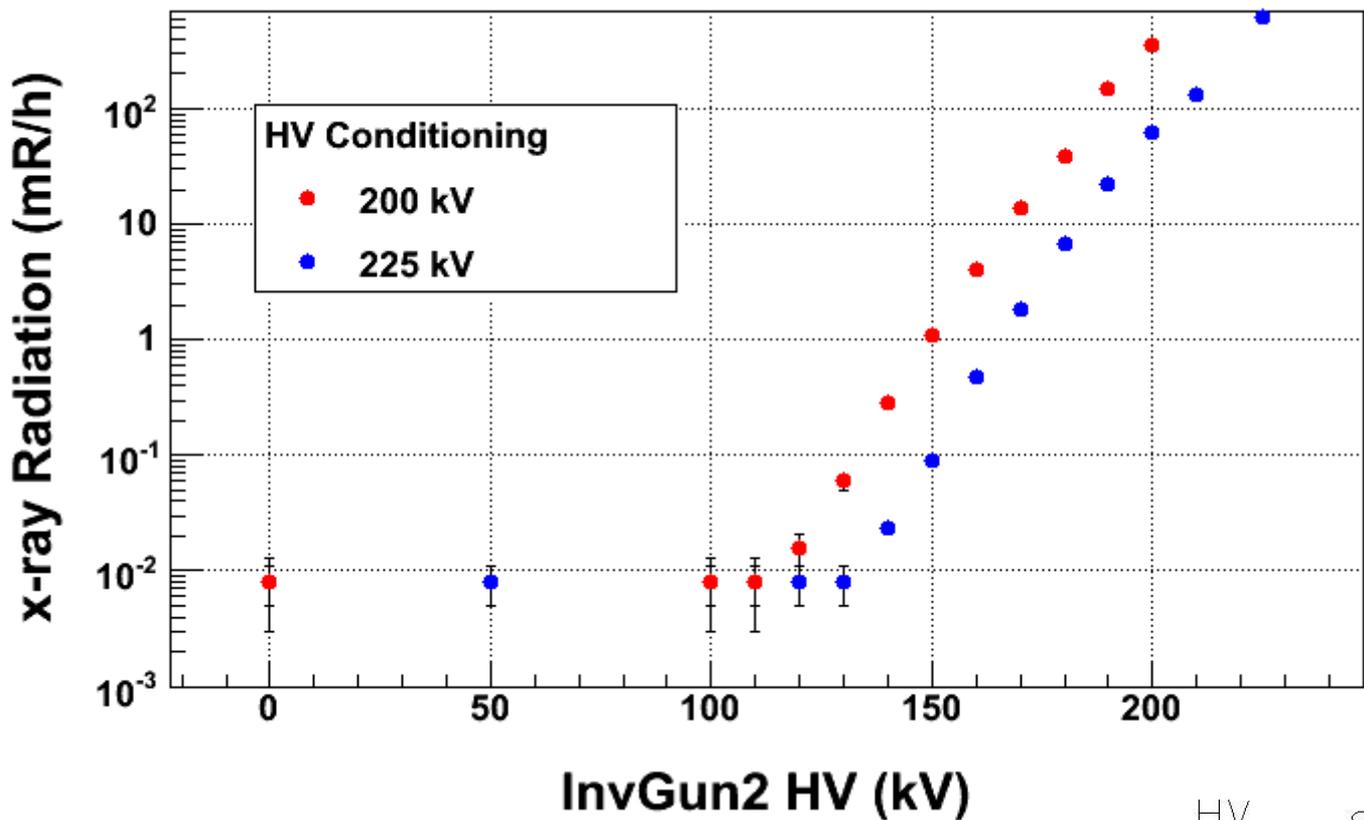
# Field Emission measured at (floating) anode versus Gun Bias Voltage



How much field emission is acceptable?  
unfortunately, it seems if you can measure it, it's too much



Anode won't always capture all FE.... Better to look for x-rays....

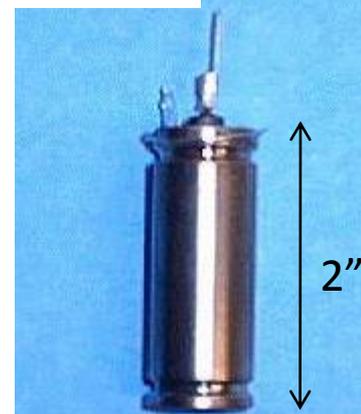


CANBERRA ADM 616 with Model IP100 Ion Chamber Detector



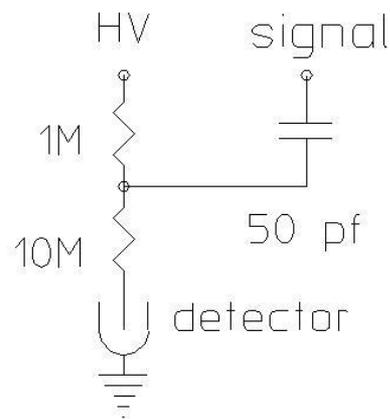
OCEANSIDE, NEW YORK, USA

LND 712

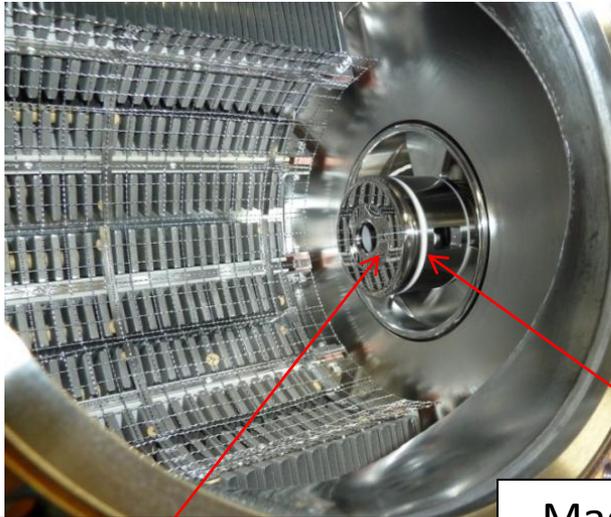


50\$

Built an inexpensive radiation monitoring system: lots of GM tubes, powered by one HV supply and data stream to computer via RS232



# HV "Conditioning": sometimes it works



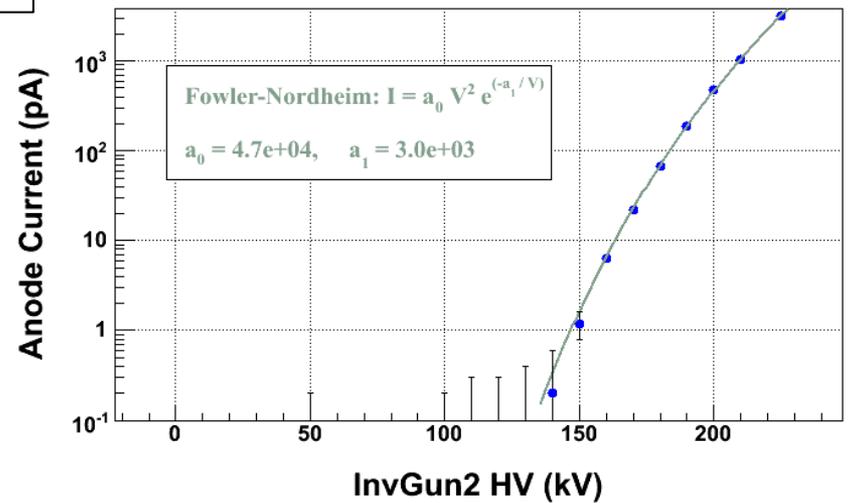
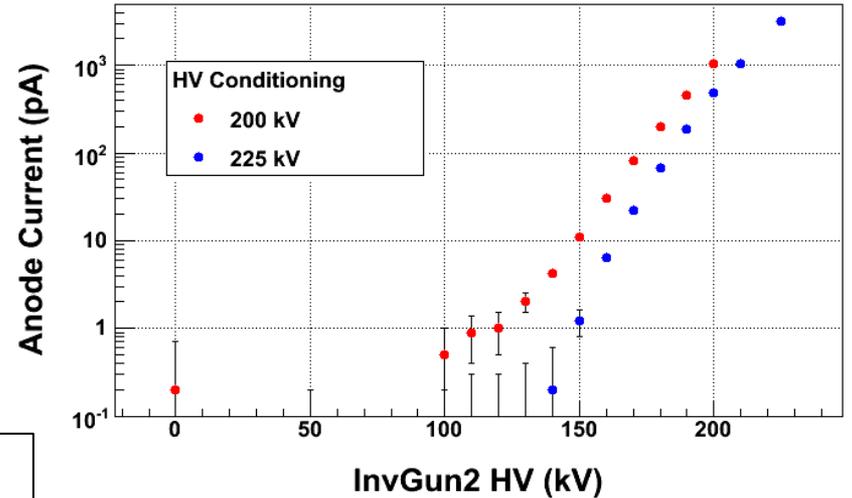
Floating Anode connected to Pico-ammeter

Macor glass-ceramic spacer



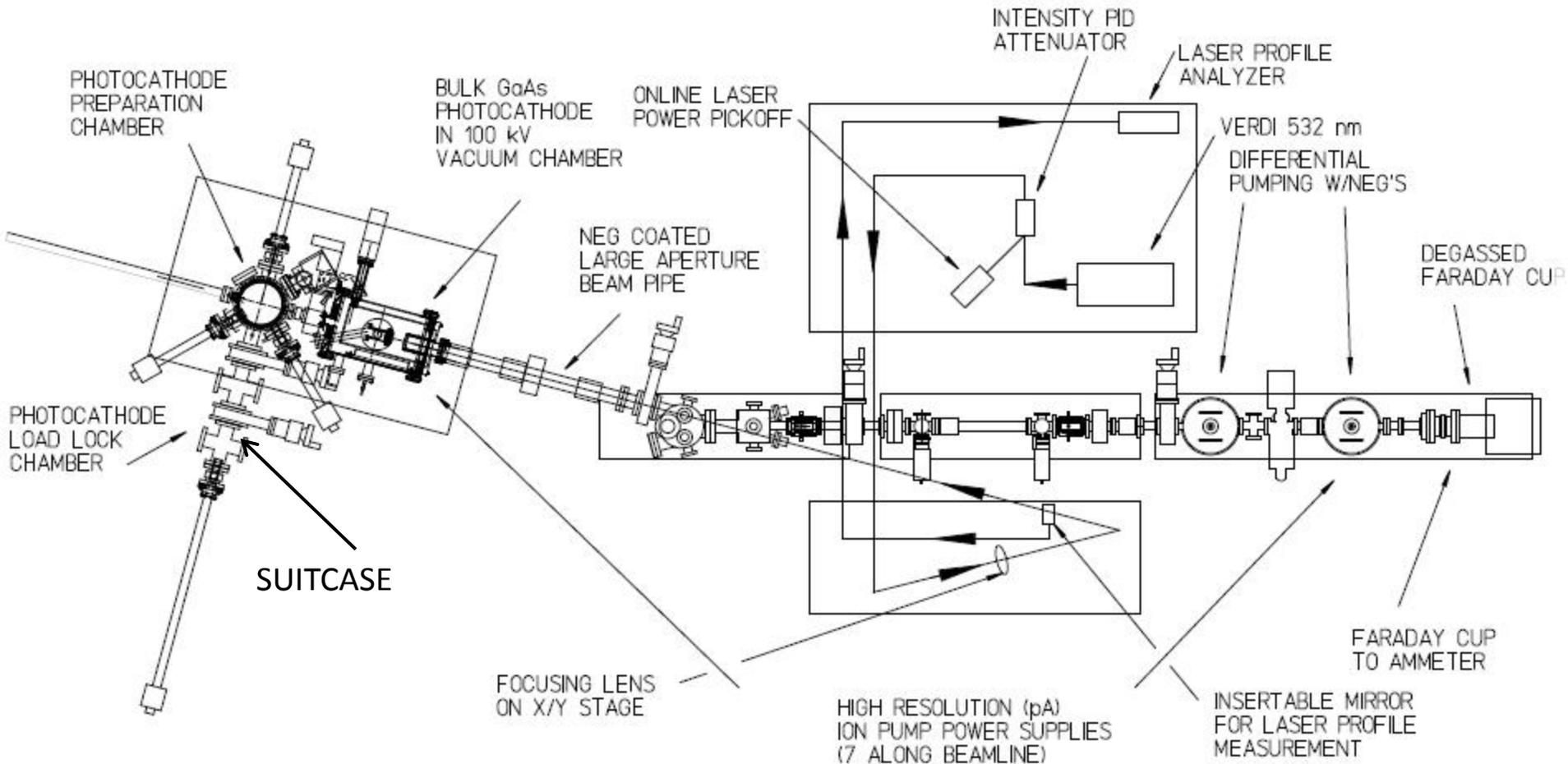
100 MΩ Conditioning Resistor

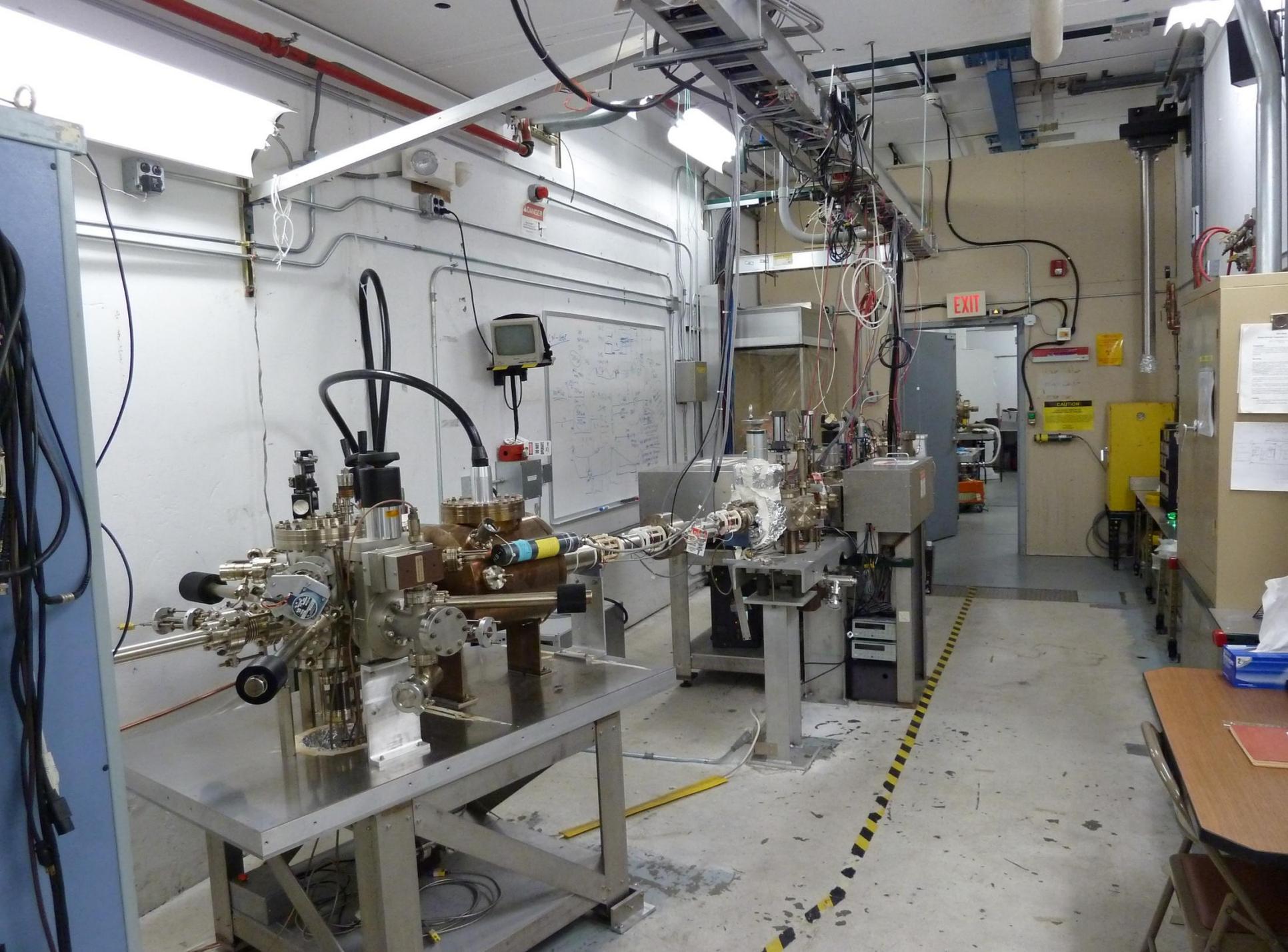
Oil Tank



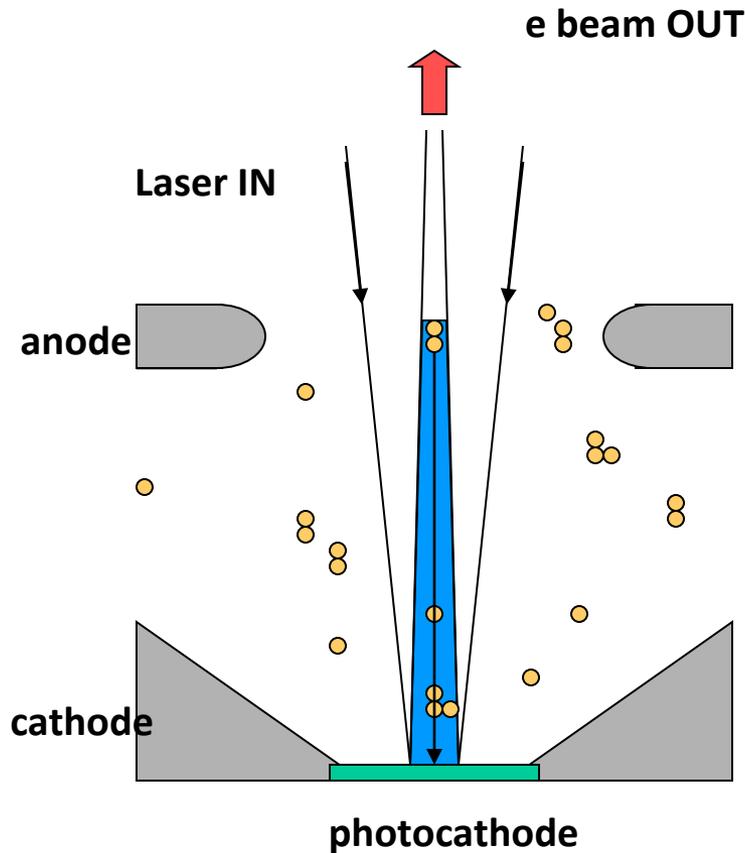
A Short for Beam Delivery

# Lifetime Experiments at the Injector Test Cave

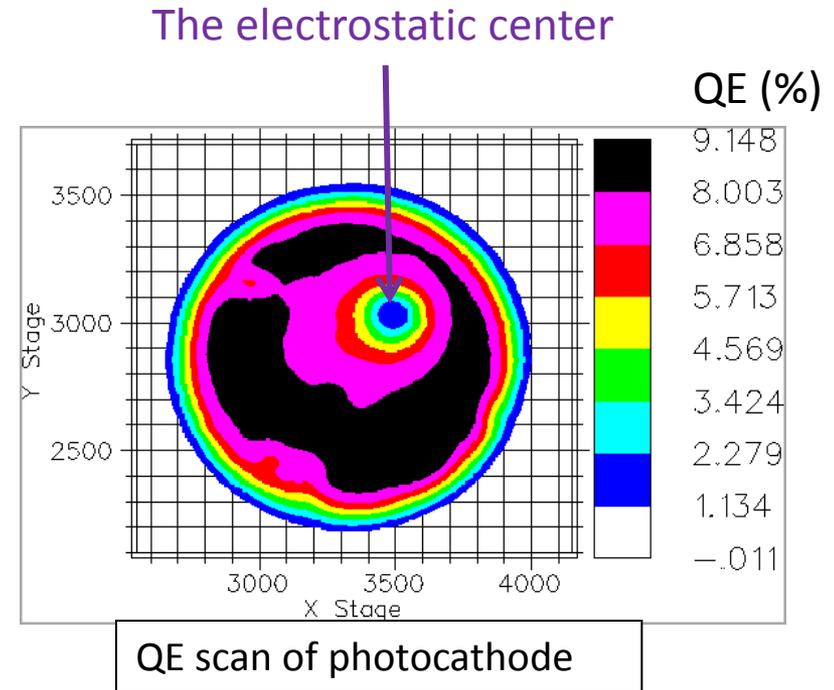




# Imperfect Vacuum and Ion Bombardment



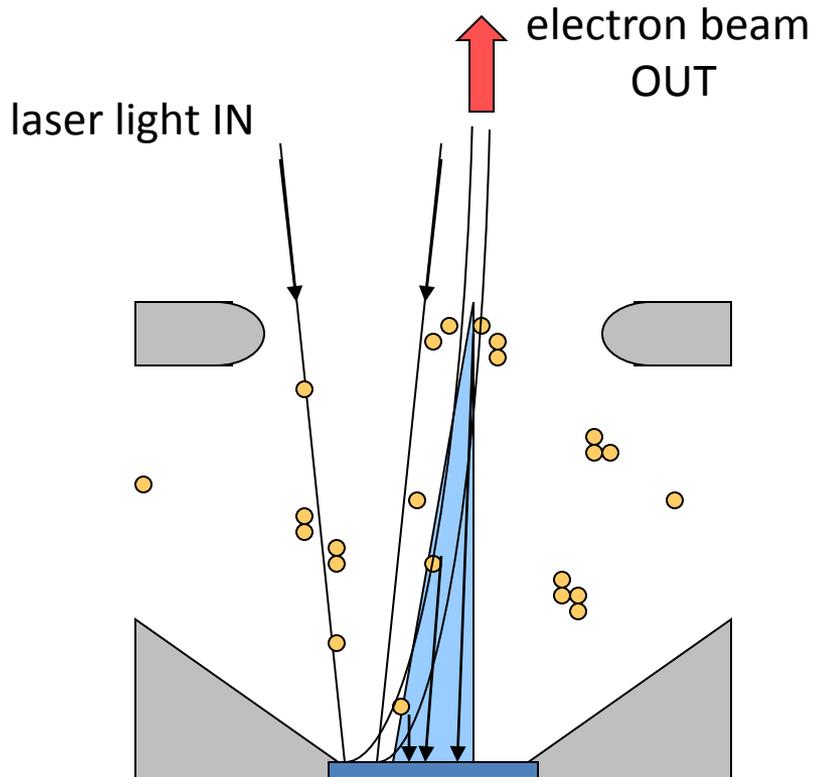
Electron beam makes ions,  
that are attracted to the EC  
of the photocathode



I mentioned other factors can limit lifetime:  
Field emission, photocathode material, laser  
wavelength, laser radial position on  
photocathode, beam optics, gun voltage

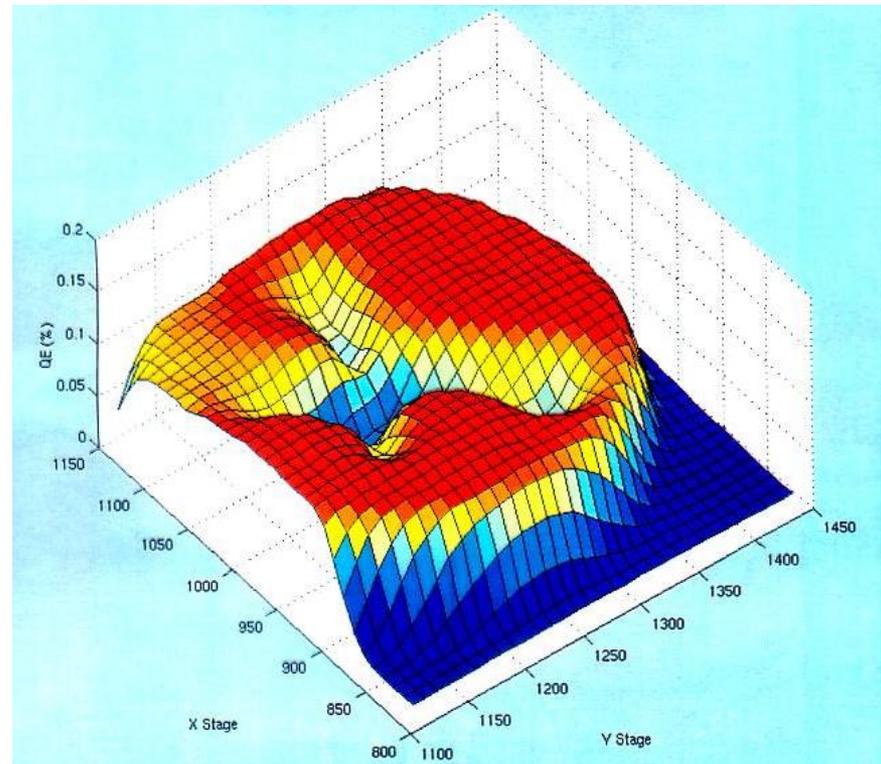
# Avoid the Electrostatic Center (EC)

We don't run beam from electrostatic center



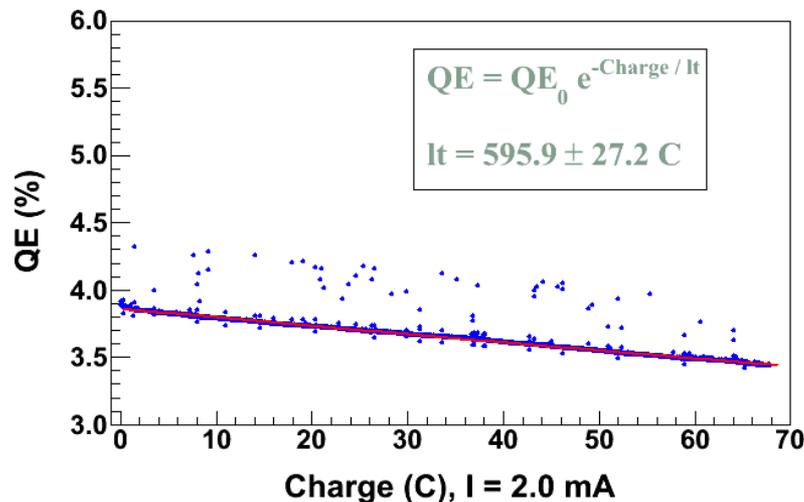
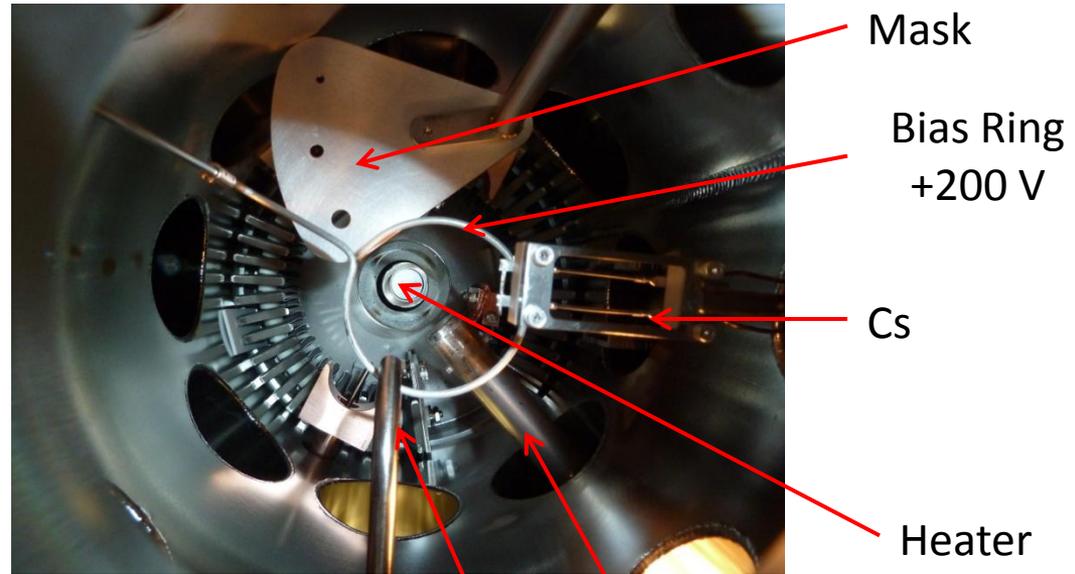
Ions create QE trough to electrostatic center

- characteristic QE "trench" from laser spot to EC. Ions are attracted to EC
- Laser spot size  $\sim 0.5$  mm and can be moved to different locations on the photocathode.
- QE can be restored, but takes about 8 hours to heat and reactivate



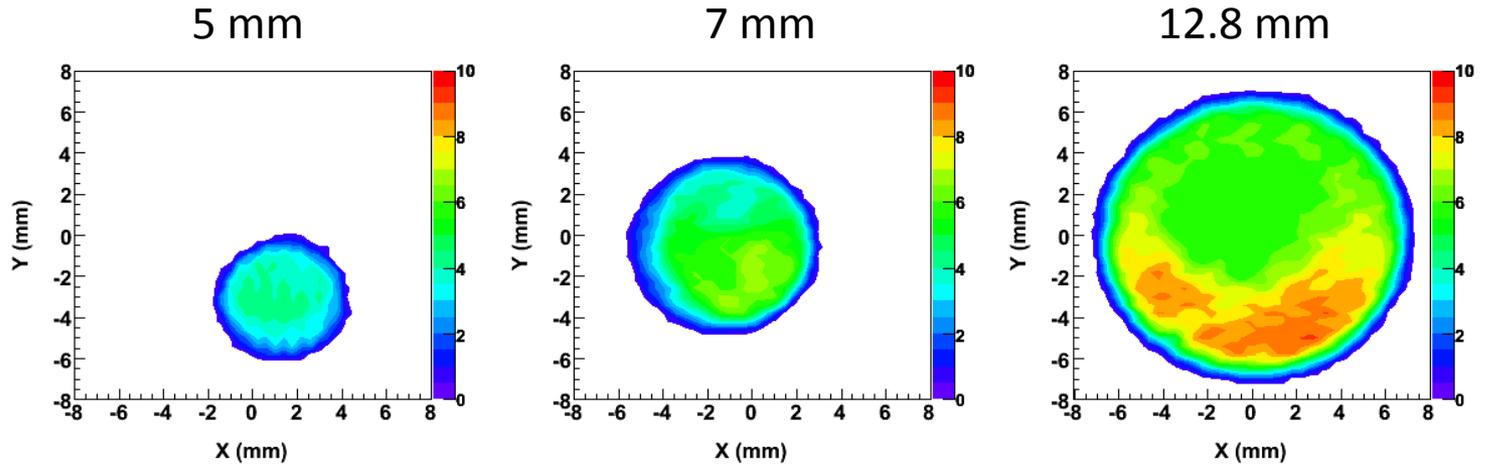
# Lifetime vs. Laser Position and Active Area

- I. Activate with different Masks: 5 mm, 7 mm, and No Mask (12.8 mm)
- II. Measure Lifetime from different spots on Bulk GaAs with 532 nm green laser

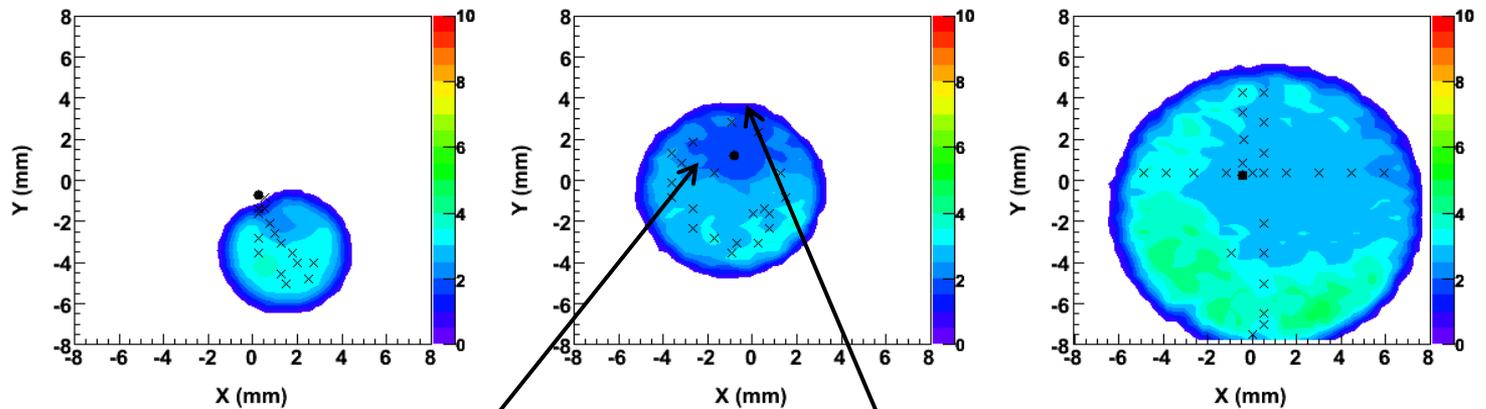


# Lifetime vs. Laser Position and Active Area

After Activation



After Lifetime Measurements



Spot

Electrostatic Center

# Lifetime vs. Laser Position and Active Area

Stray light, Spontaneous Emission from GaAs photocathode, and x-ray induced photoemission might be generating this “extra” beam

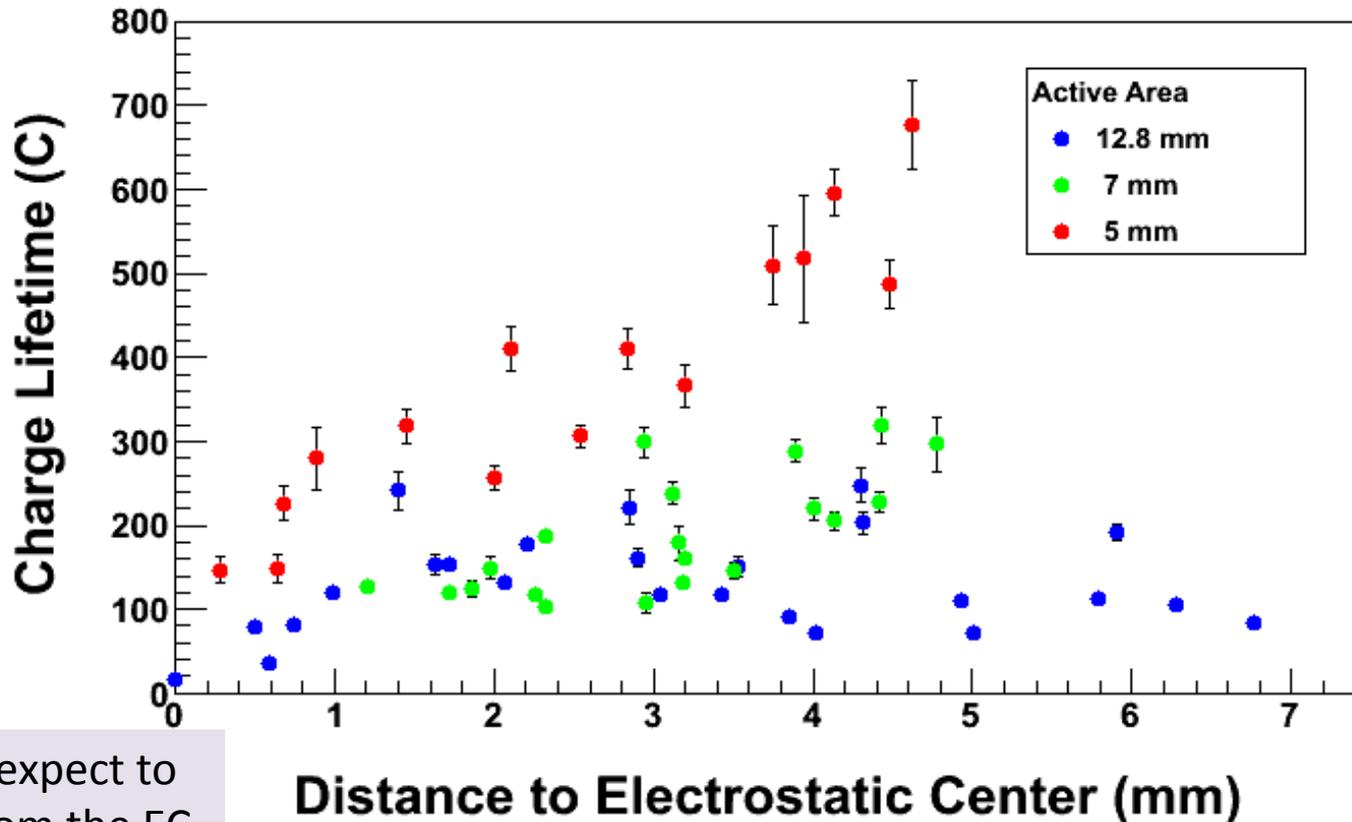
	I=0 (HV = 0, 100 kV)	I = 2 mA (Bulk GaAs, 532 nm, 350 $\mu$ m Laser Spot) (HV = 100 kV)		
		5 mm Active Area	7 mm Active Area	12.8 mm Active Area
Anode Current (pA)	0.0 $\pm$ 0.3	0.0 $\pm$ 0.3	0.0 $\pm$ 0.3	-100 – -1000
X-ray Detector (E-2 mR/h)	0.6 $\pm$ 0.3	1.5 $\pm$ 0.5	1.8 $\pm$ 0.5	3 – 7
Gun Vacuum (pA)	0	0	0	0 – 30
Y-Chamber Vacuum (nA)	3.0	3.0	3.0	4 – 20

# Lifetime vs. Laser Position and Active Area



Lesson: electrons from the edge of the photocathode strike the anode and vacuum chamber walls, degrading vacuum and limiting lifetime.

**Don't make beam from the edge of the photocathode!!!**

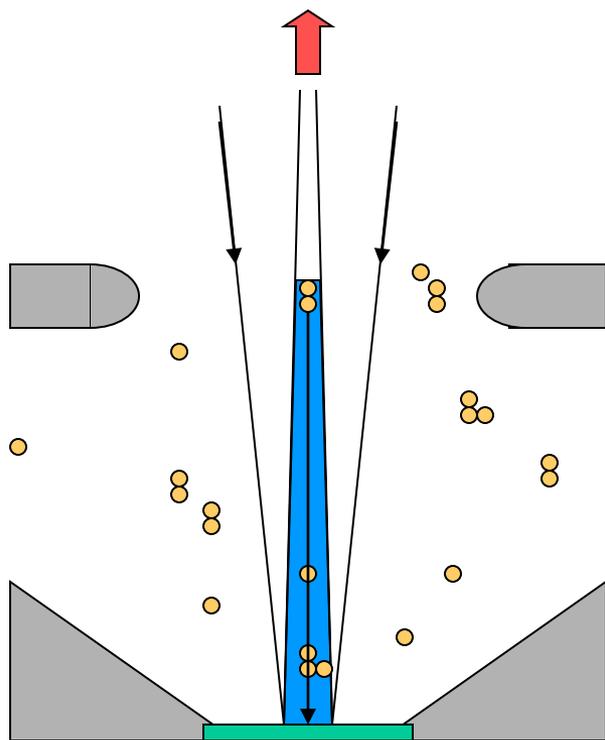


Also, don't expect to run beam from the EC

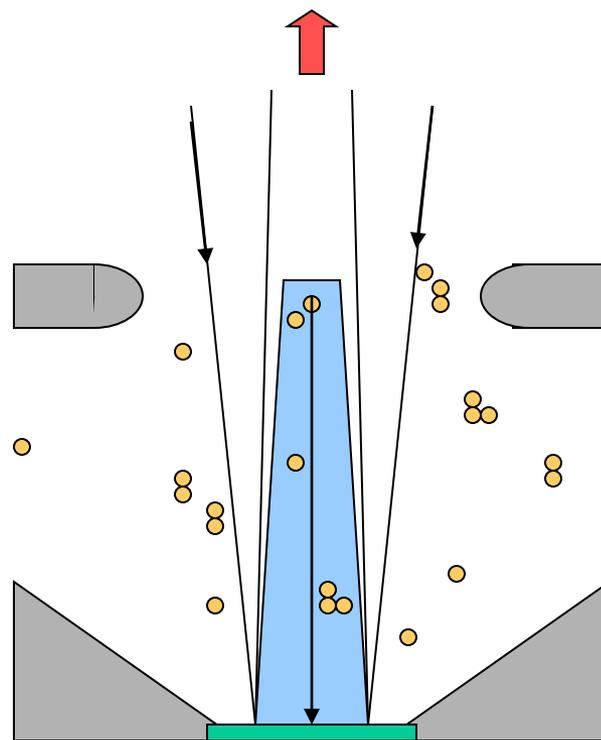
# Improve Lifetime with Larger Laser Spot?

(Best Solution – Improve Vacuum, but not easy)

Bigger laser spot, same # electrons, same # ions



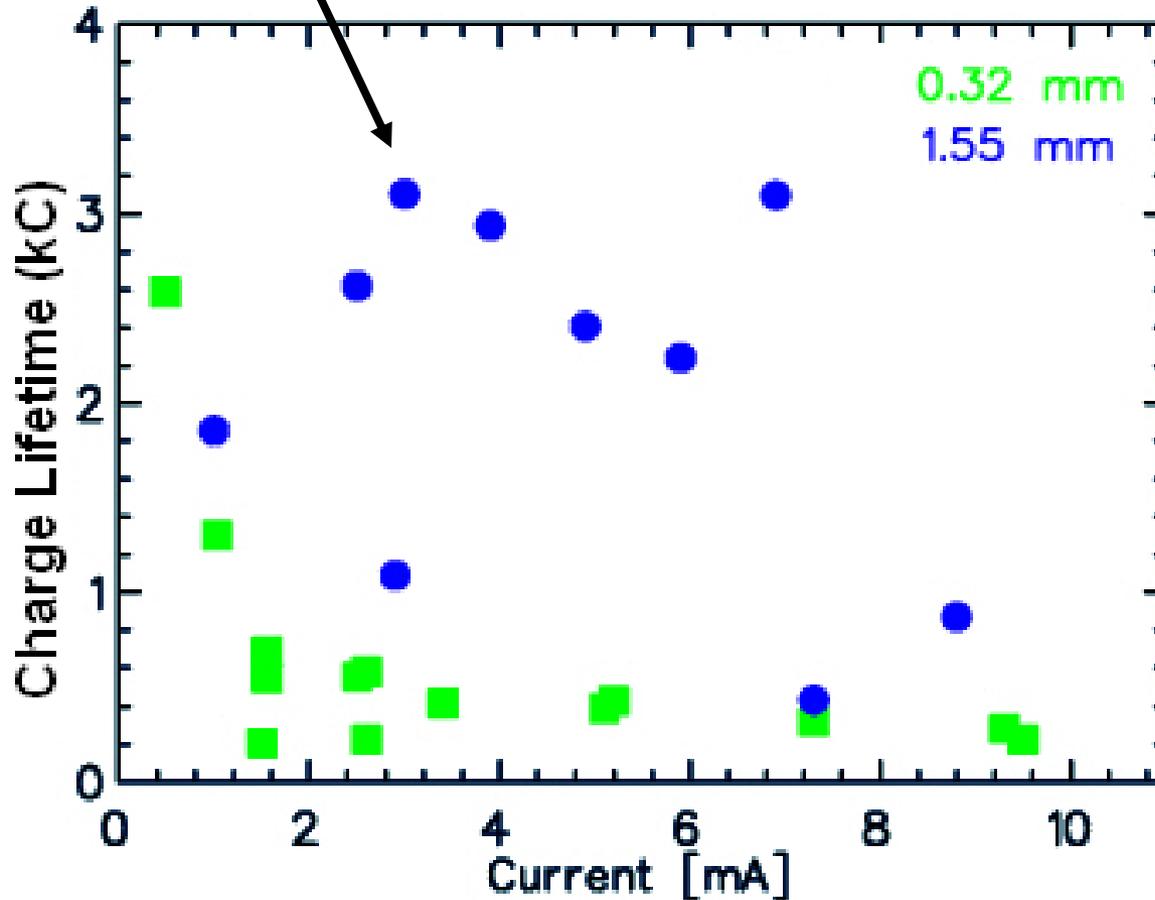
Ionized residual gas strikes photocathode



Ion damage distributed over larger area

# Lifetime with Large/Small Laser Spots

Tough to measure large Coulomb lifetimes with only 100-200 C runs!

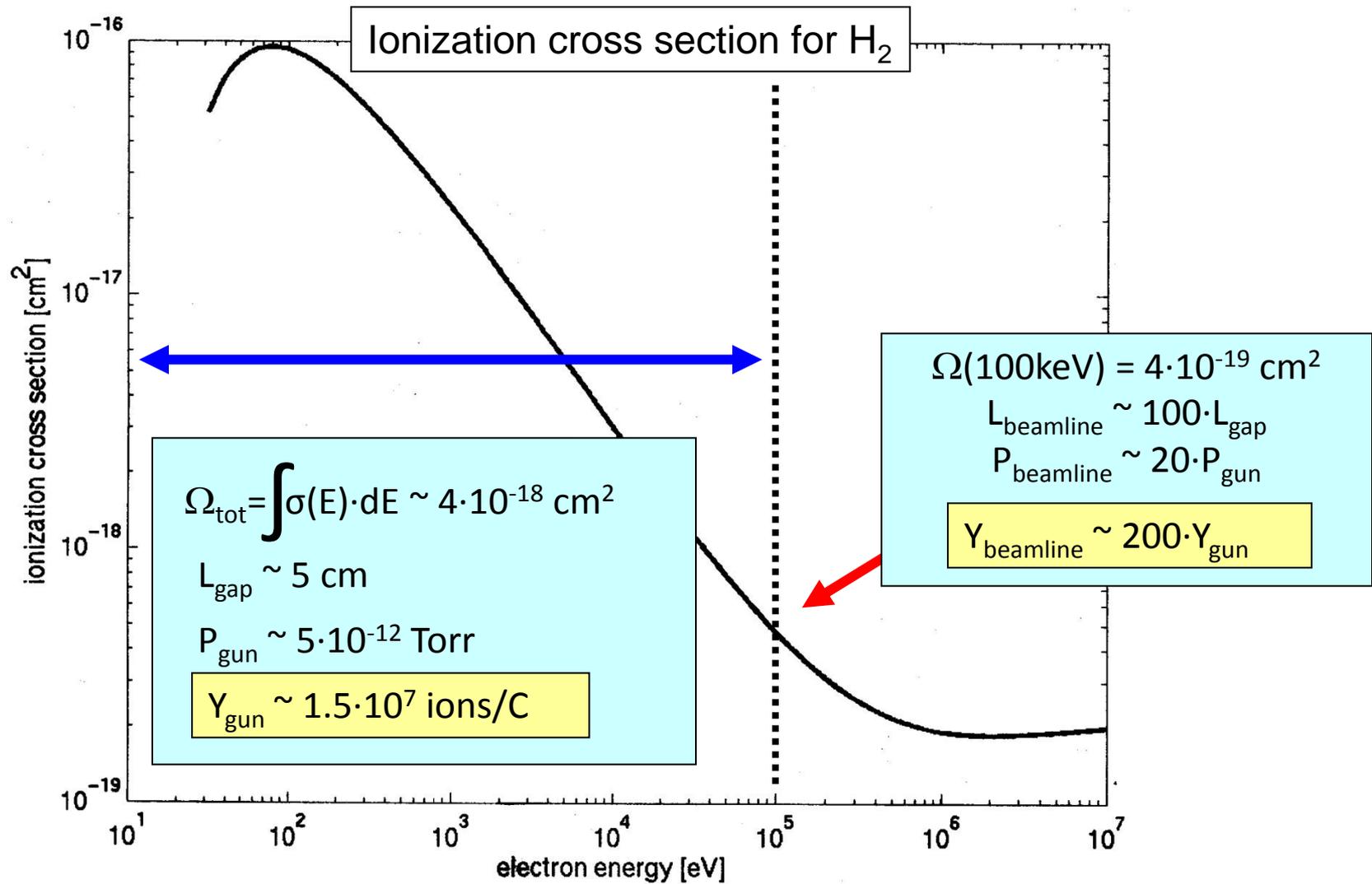


Factor of 5 to 10 improvement with larger laser spot size

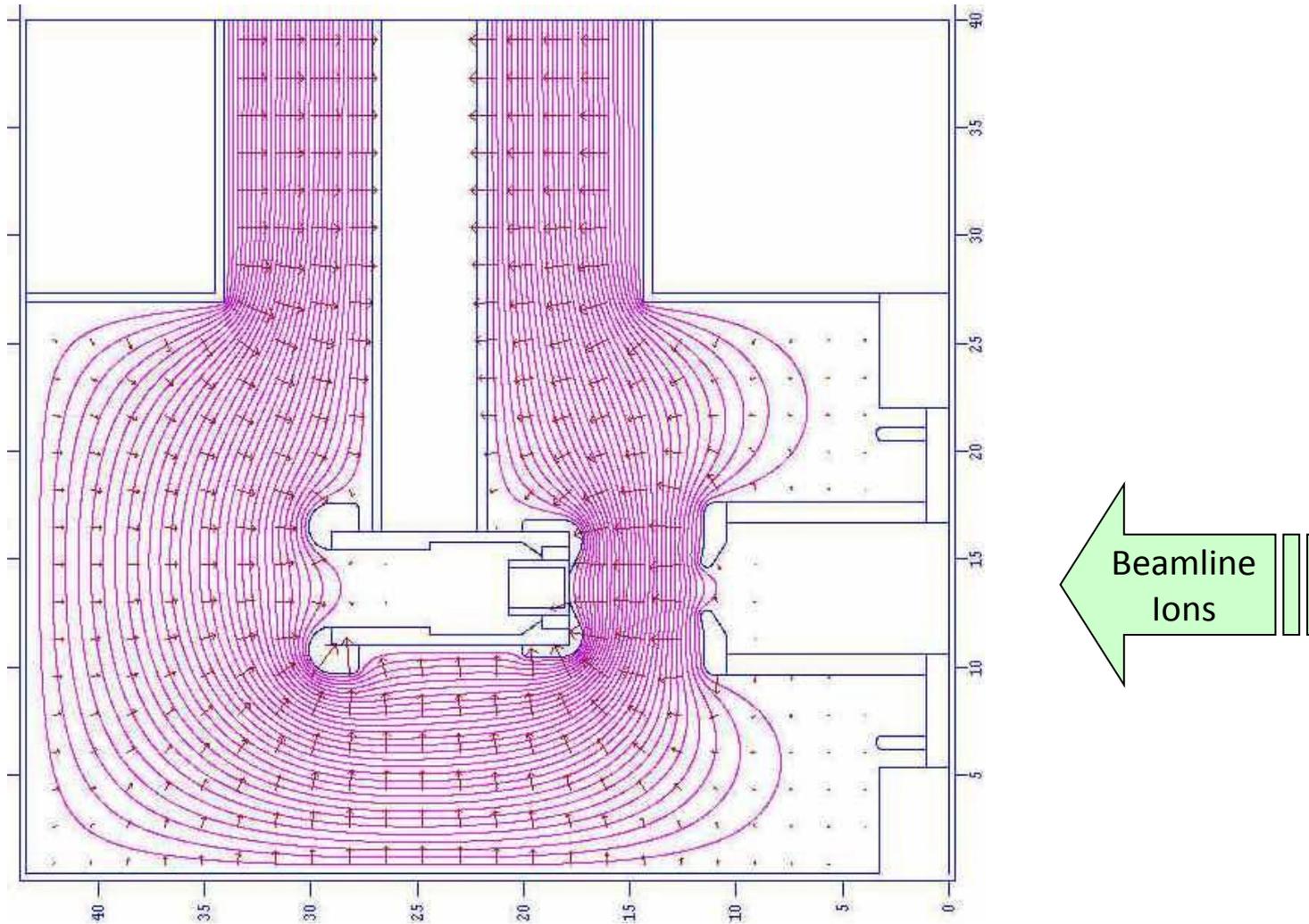
Expectation:

$$\left[ \frac{1500}{350} \right]^2 \approx 18$$

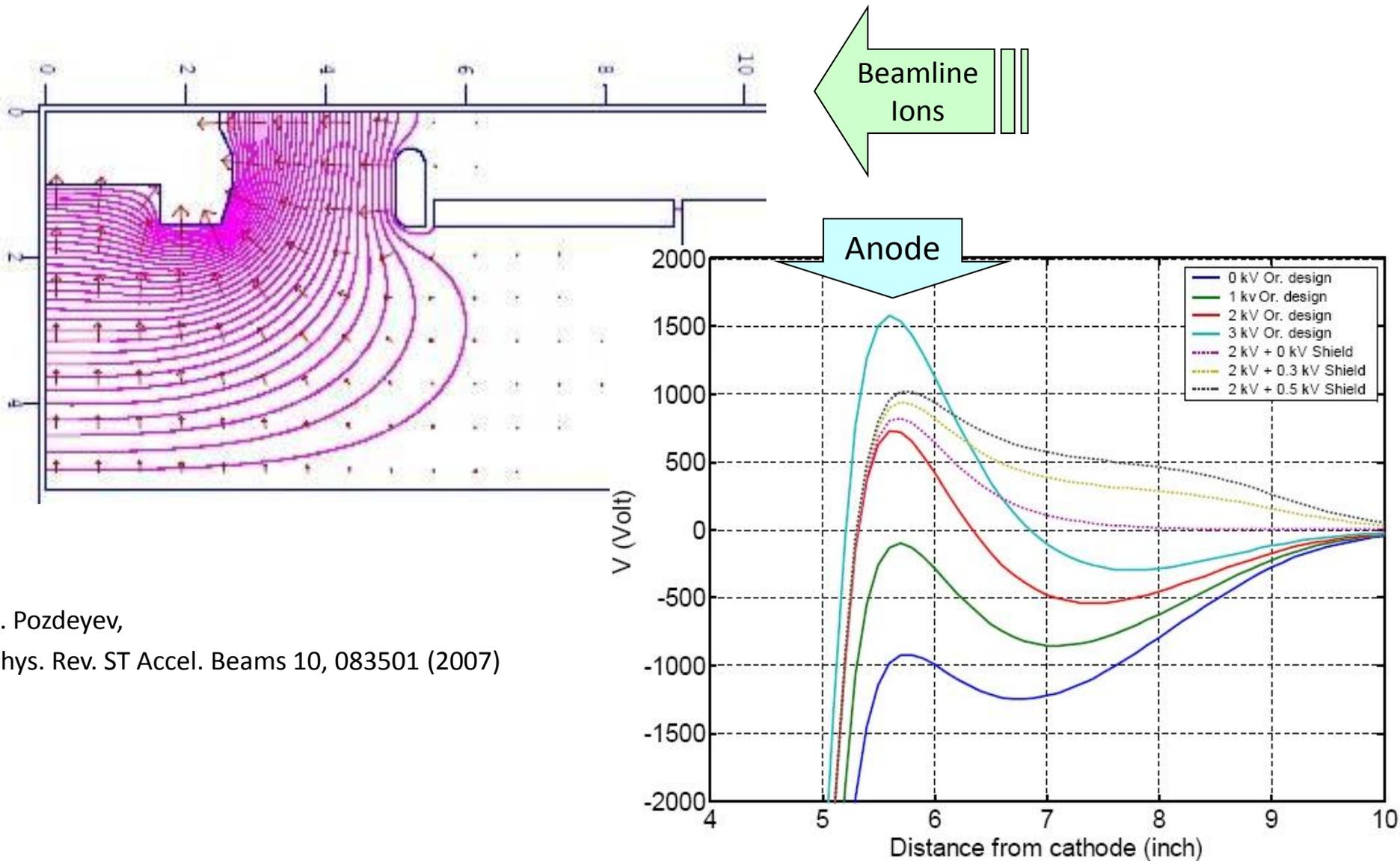
# What about Ions Created Downstream of Anode?



# Modifying the HV Chamber Anode Structure

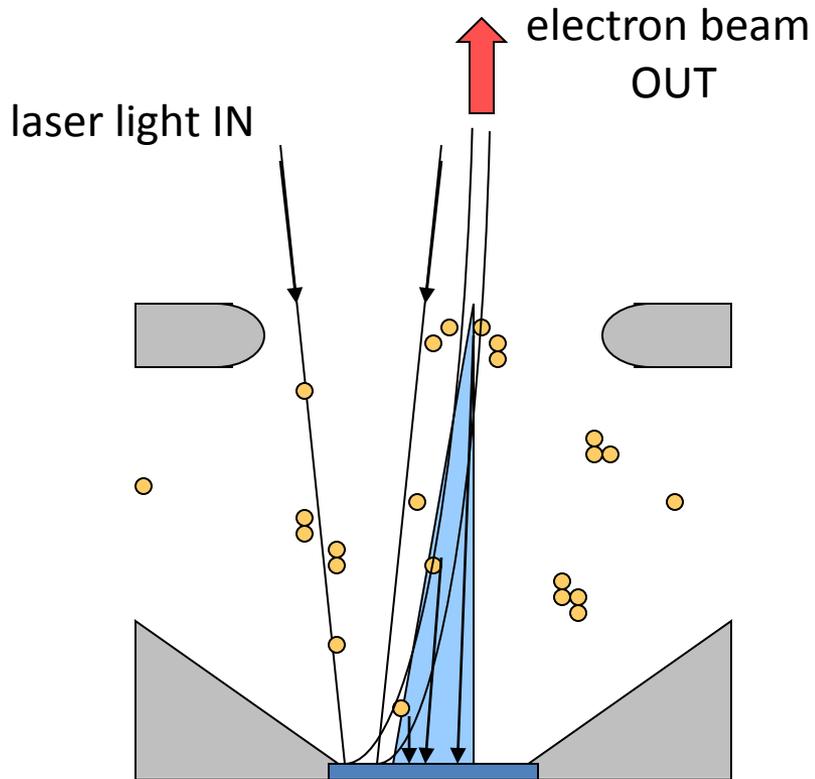


# Limiting Ionized Gas from HV Chamber

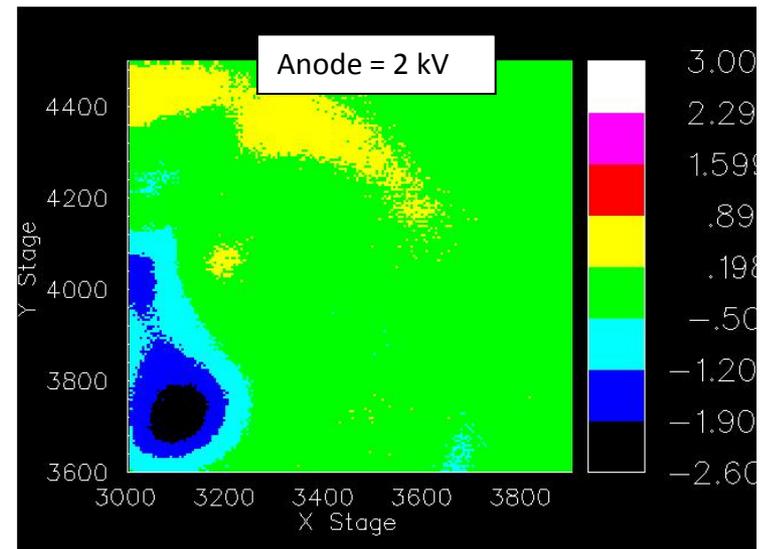
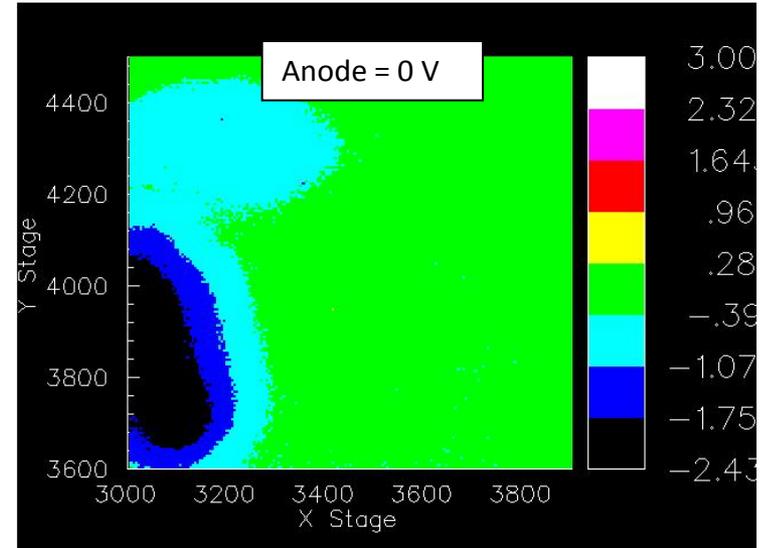


E. Pozdeyev,  
Phys. Rev. ST Accel. Beams 10, 083501 (2007)

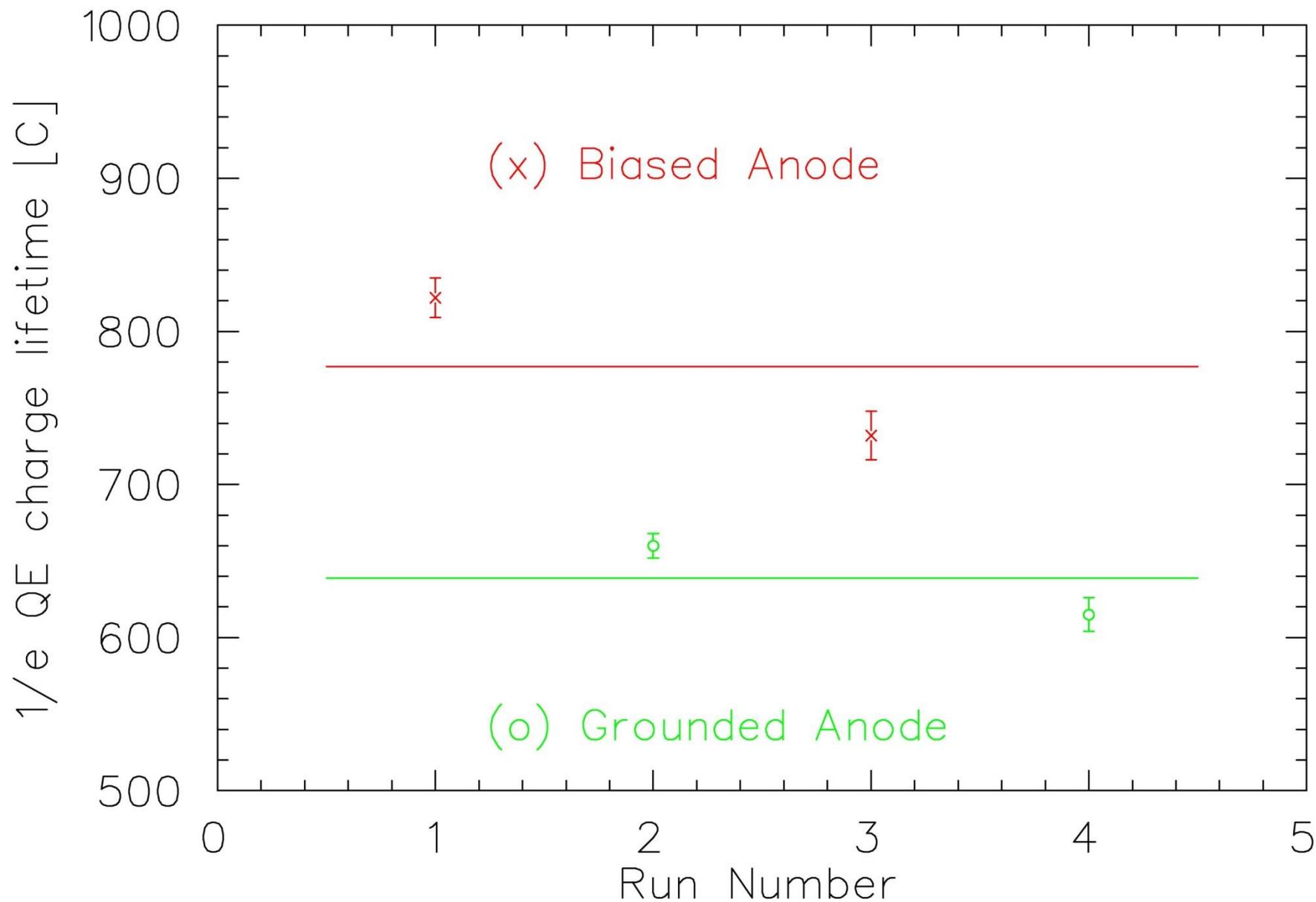
# Unbiased vs. Biased Running at 5mA



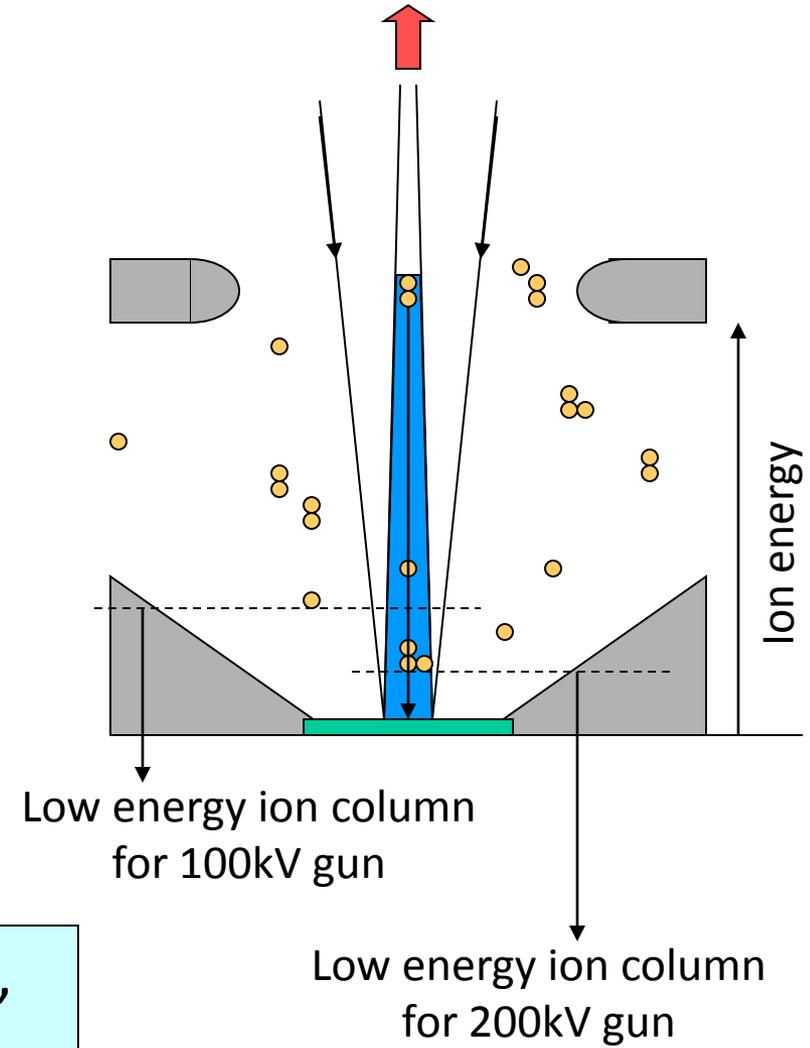
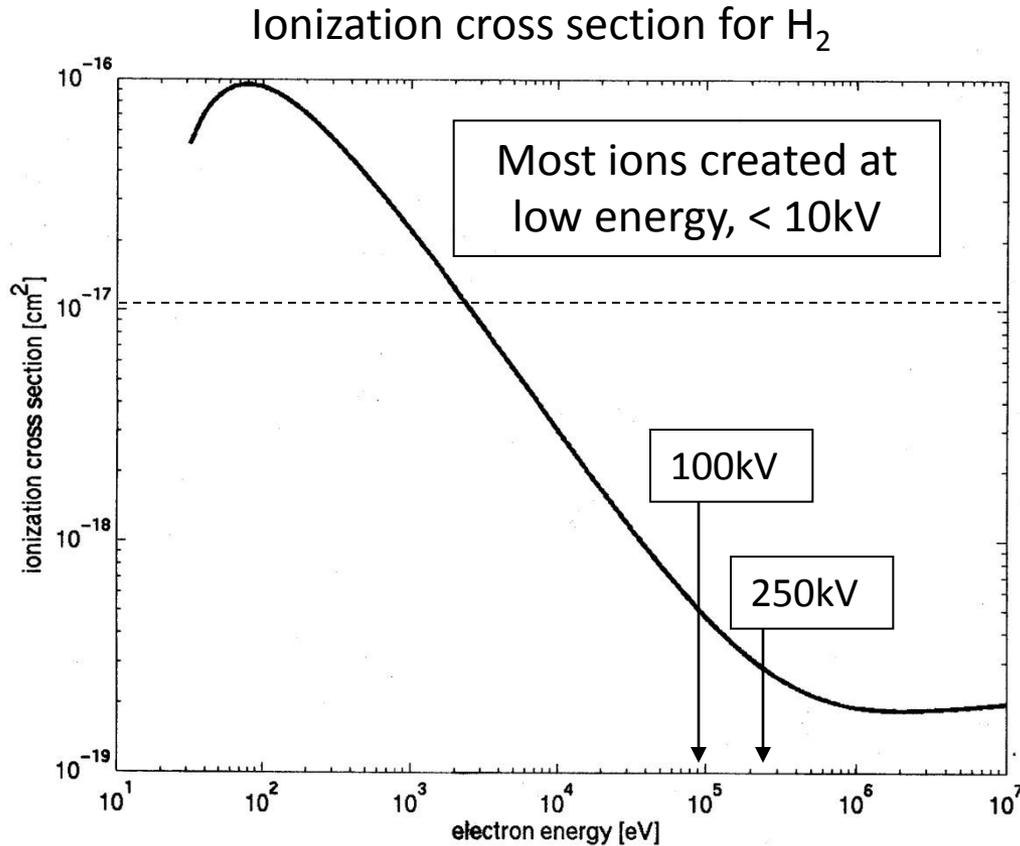
Ions create QE trough to electrostatic center



# Photocathode Lifetime at "EC" at 2mA

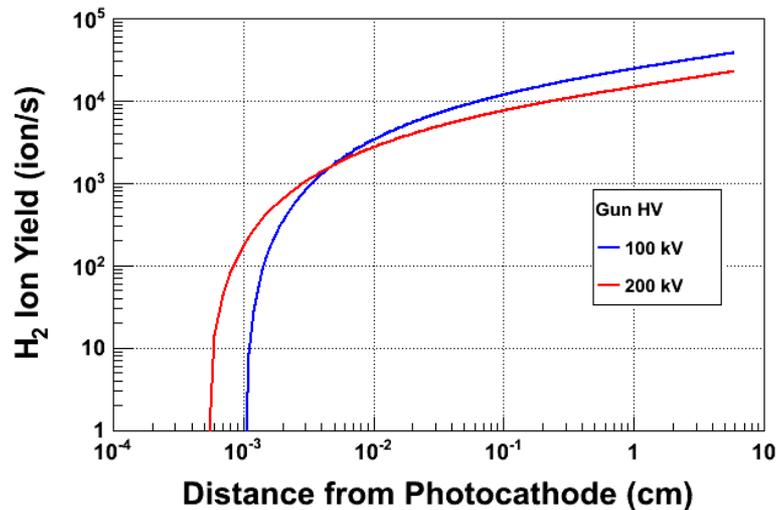
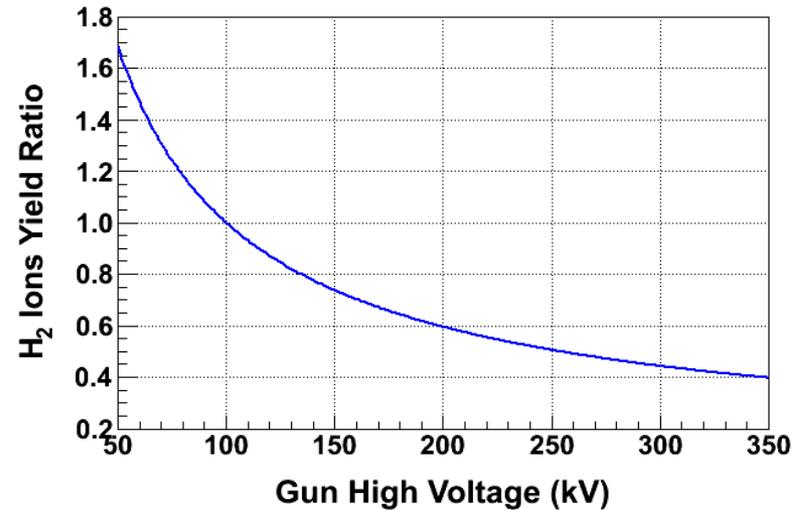
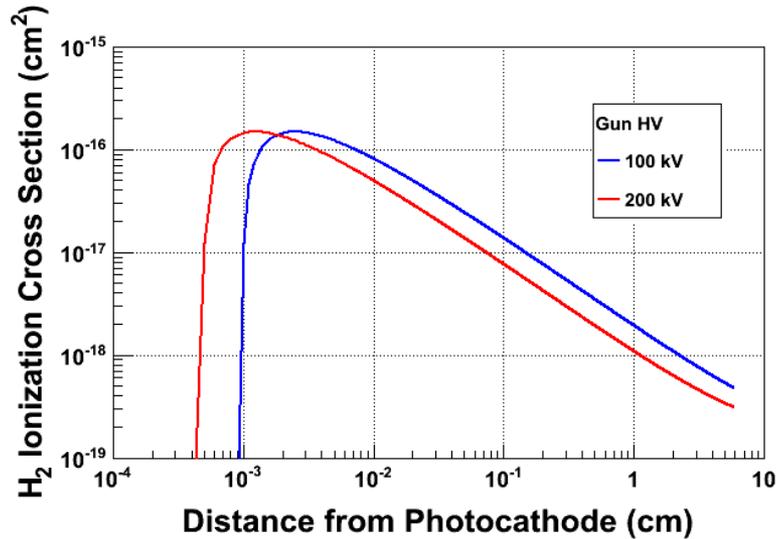


# Improve Lifetime with Higher Bias Voltage?



Hypothesis: Double the gun voltage, halve the # of “bad” ions, improve lifetime by 2

# Prolong Photocathode Charge Lifetime



At 200 kV, only 60% of ions are created compared to 100 kV, longer lifetime

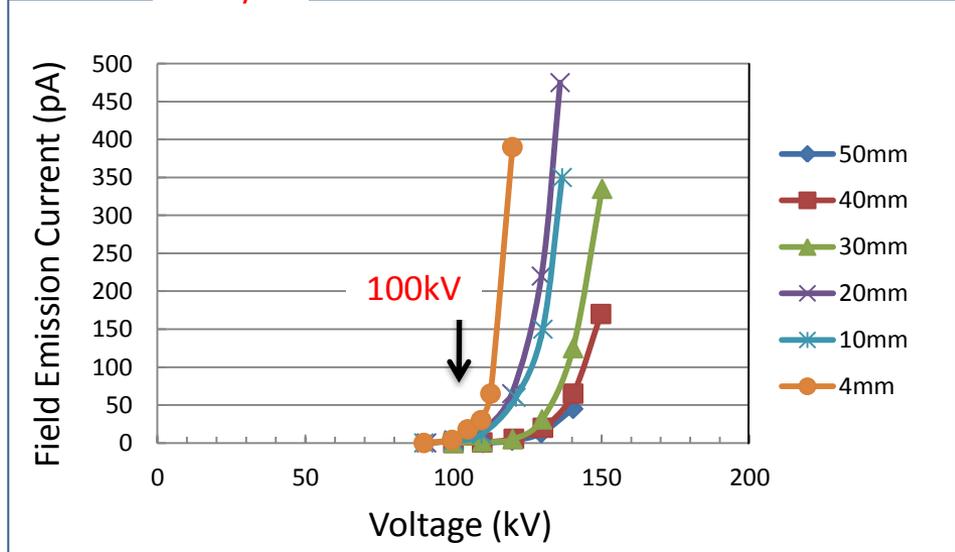
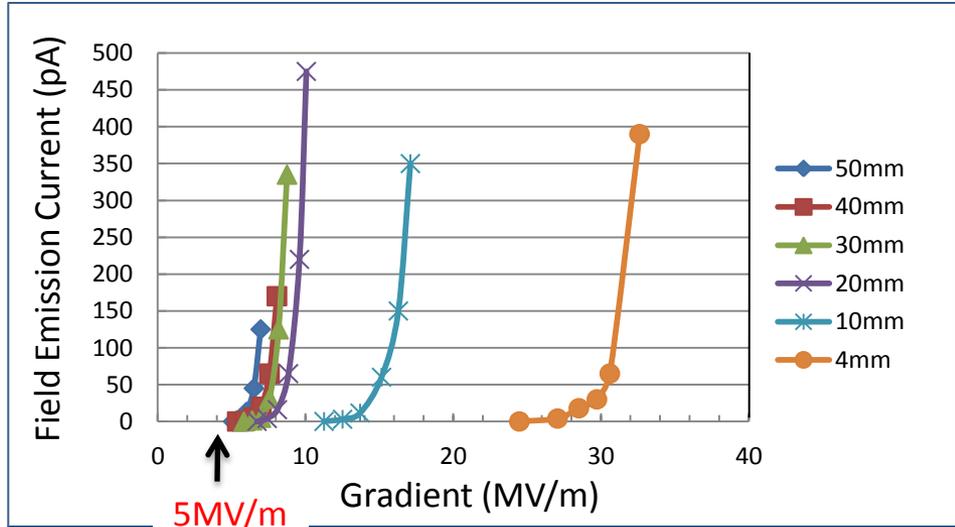
Beam Current: 2.0 mA  
Vacuum:  $8.0 \times 10^{-12}$  Torr

# Field Emission – A Very Important Issue



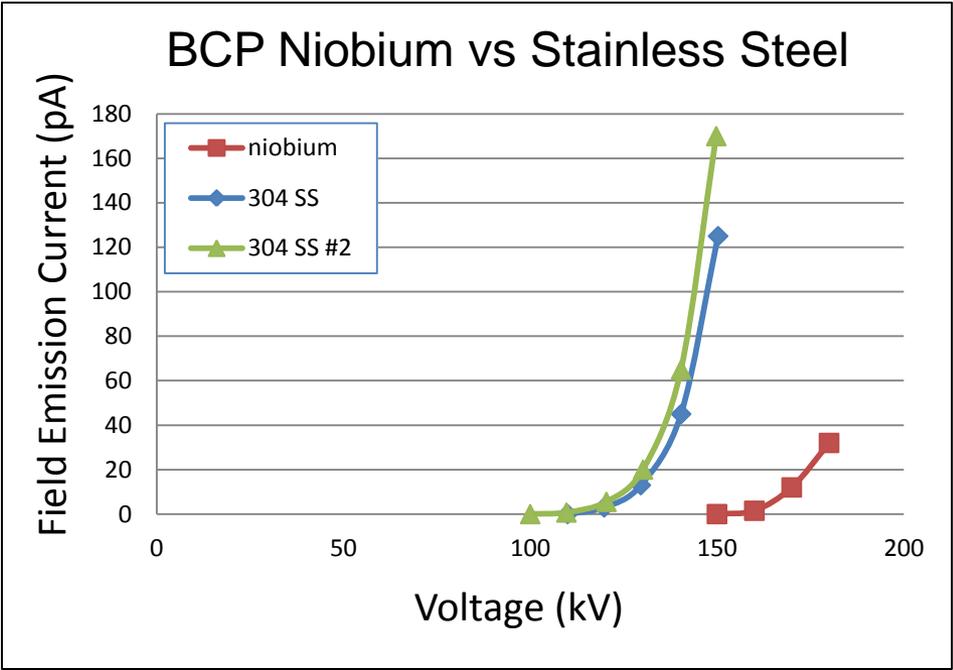
Stainless Steel and Diamond-Paste Polishing Good to  $\sim 5\text{MV/m}$  and 100kV.

- Previous measurements with flat electrodes, small gaps and low voltage - not very useful
- Want to keep gun dimensions about the same – suggests our 200kV gun needs “quiet” electrodes to 10MV/m



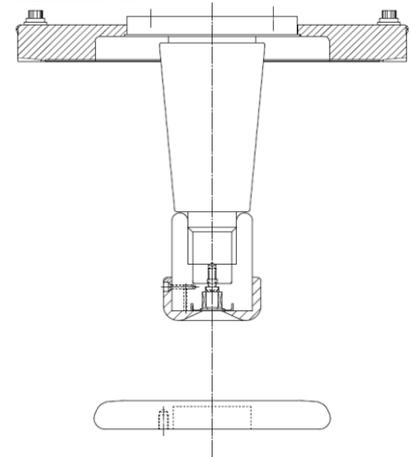
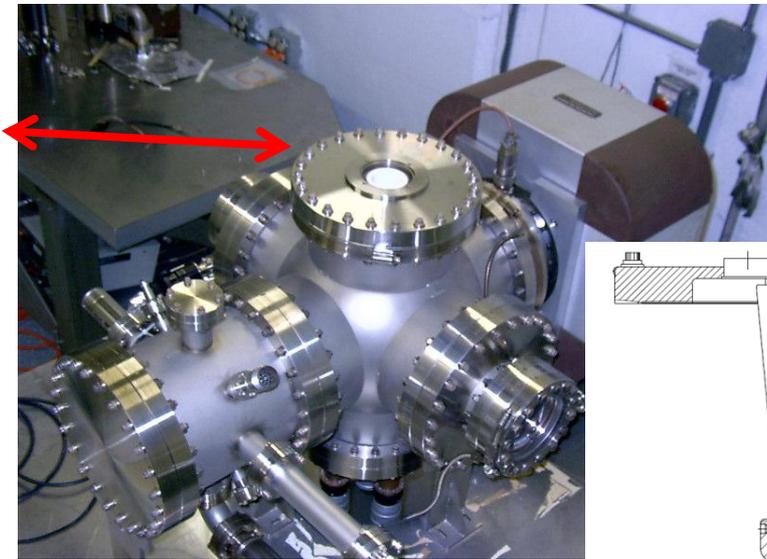
**Single Crystal Niobium:**

- Capable of operation at higher voltage and gradient?
- Buffer chemical polish (BCP) much easier than diamond-paste-polish



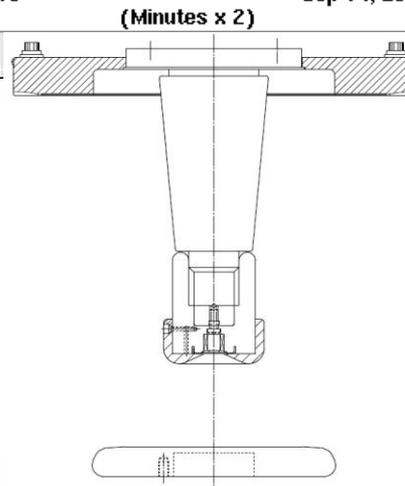
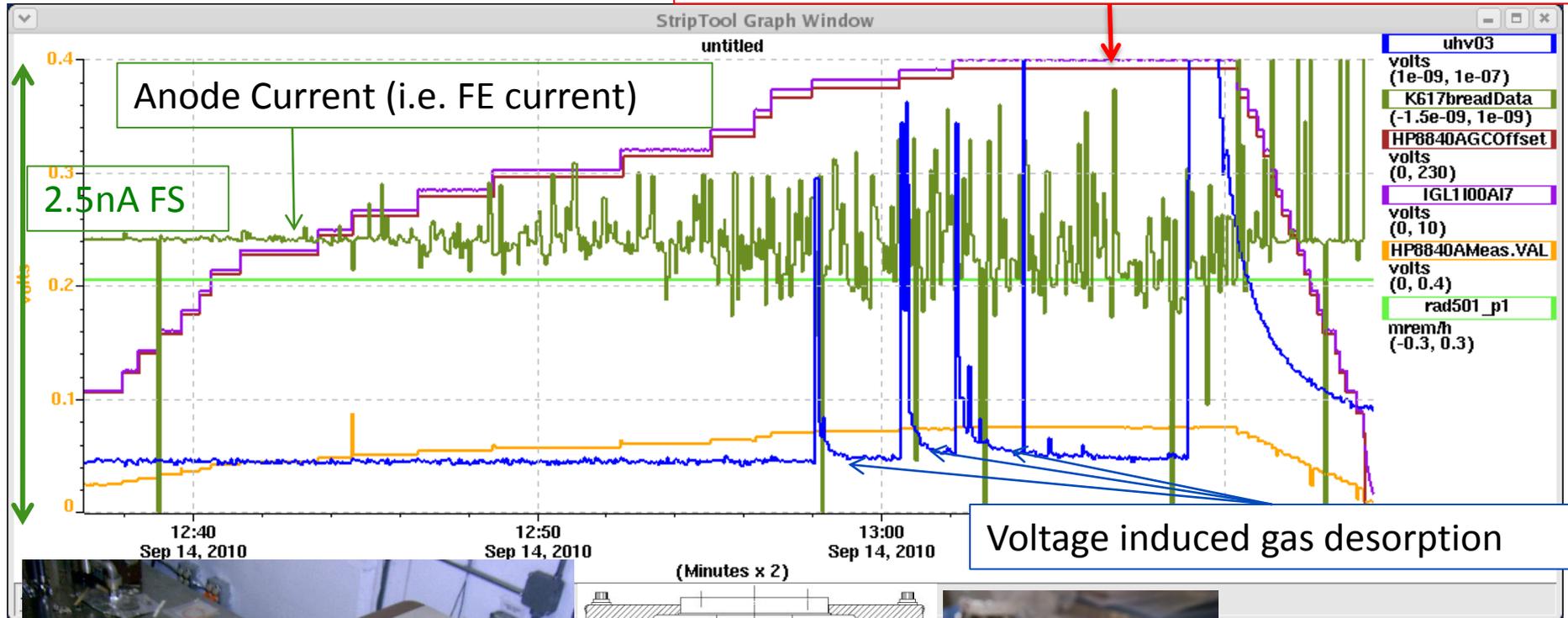
Conventional geometry: cathode electrode mounted on metal support structure

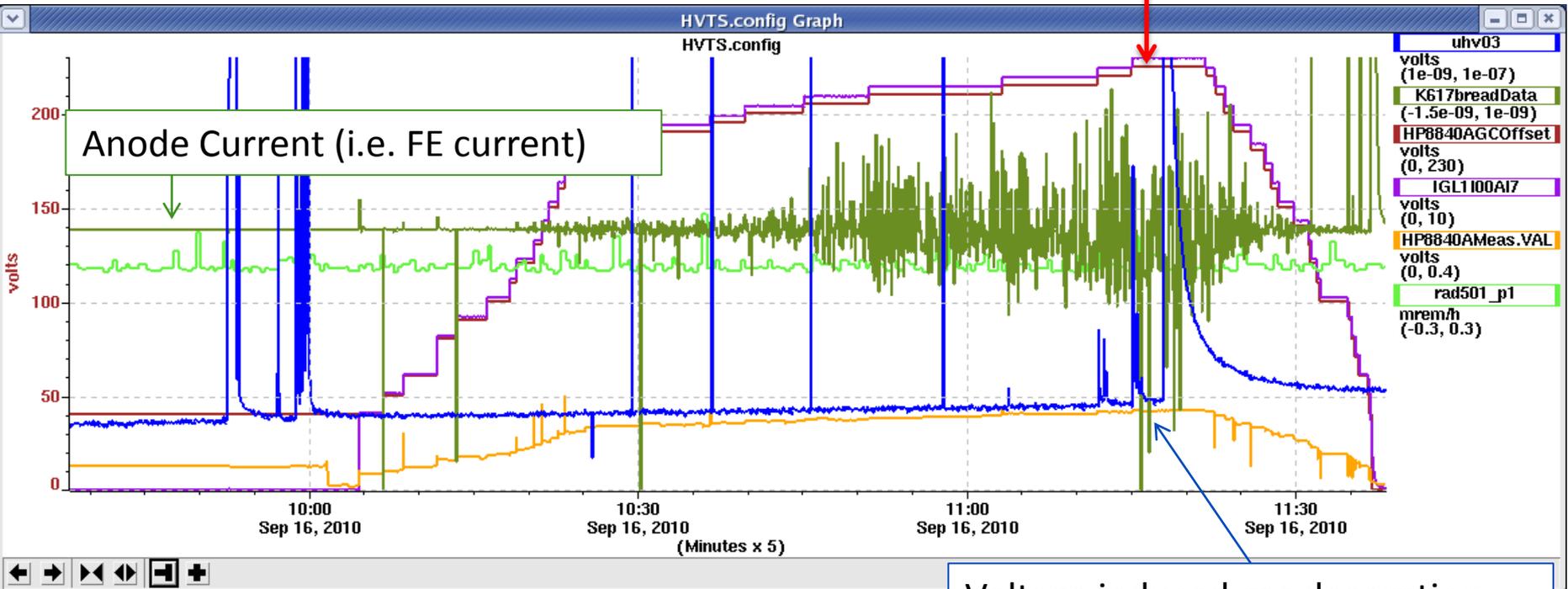
Replace conventional ceramic insulator with "Inverted" insulator: no SF6 and no HV breakdown outside chamber



# Single Crystal Nb: Good Cathode Electrode Material

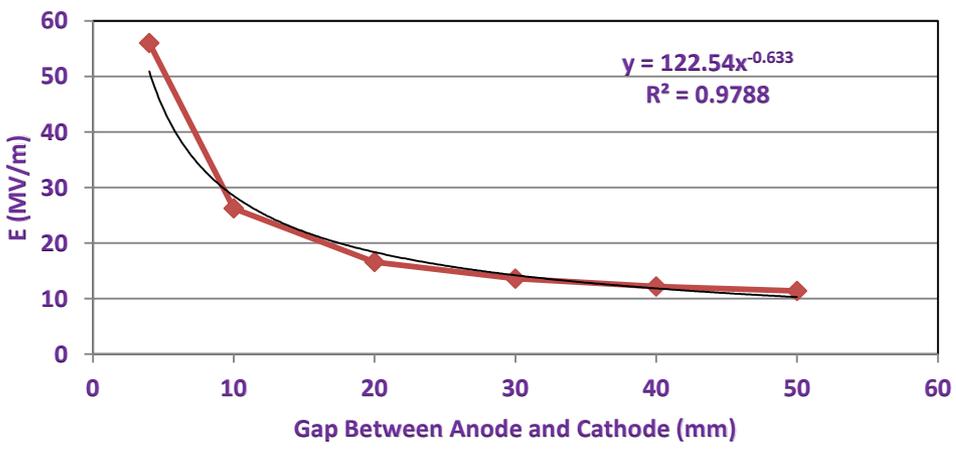
~ No field emission at 225kV bias and 50mm gap





Voltage induced gas desorption

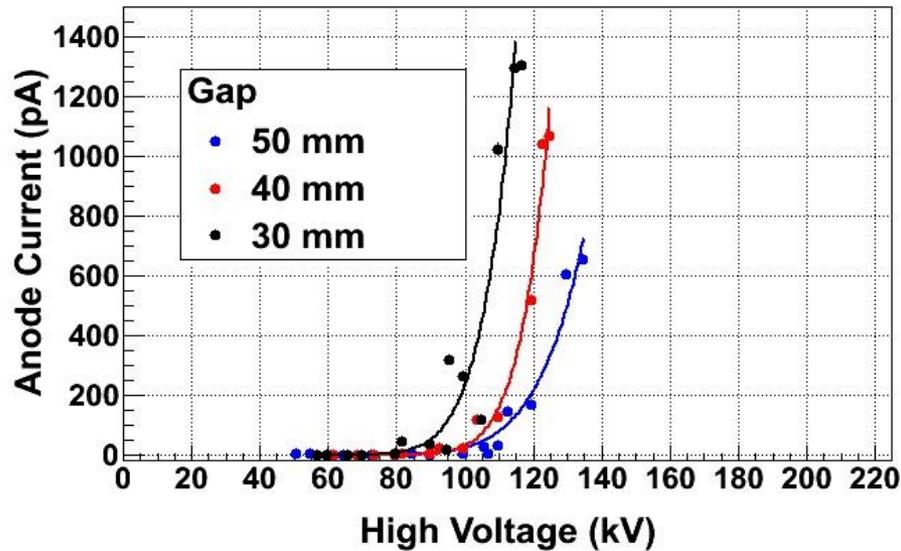
Maximum Gradient at 200 kV in HVTS



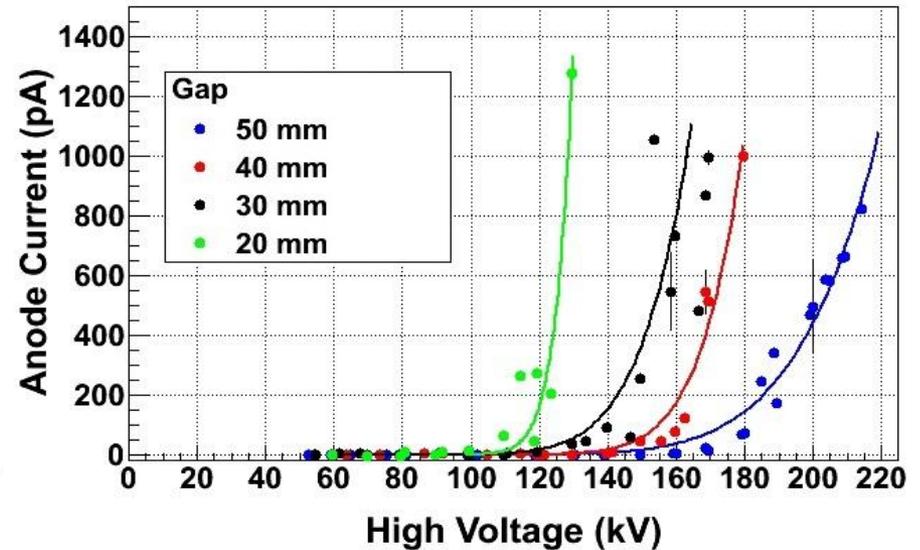
- But Niobium can be pushed too far, producing (many?) field emission sites. Avoid small gaps.
- These field emission sites can be difficult to process out
- Krypton processing works
- Sometimes, electrode needs to be re-BCP-ed.

# Why a Niobium Cathode Electrode?

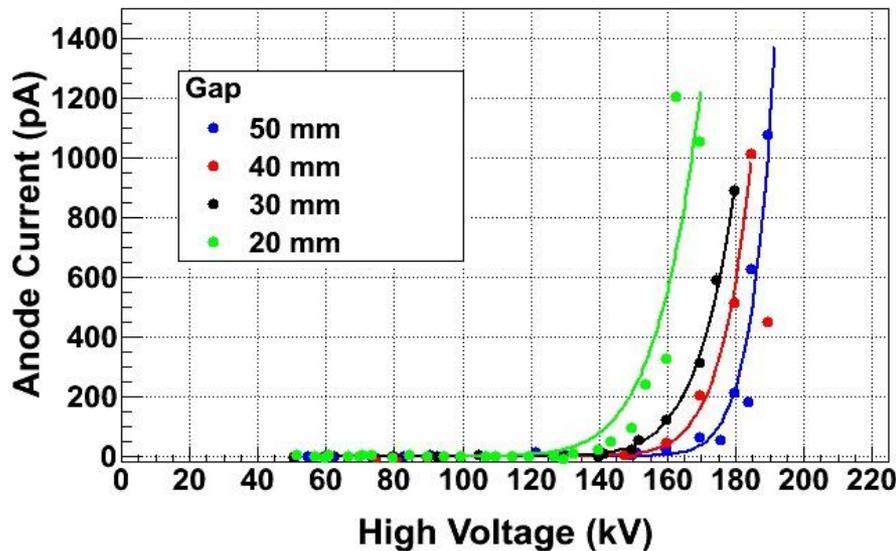
## DPP 304 SS



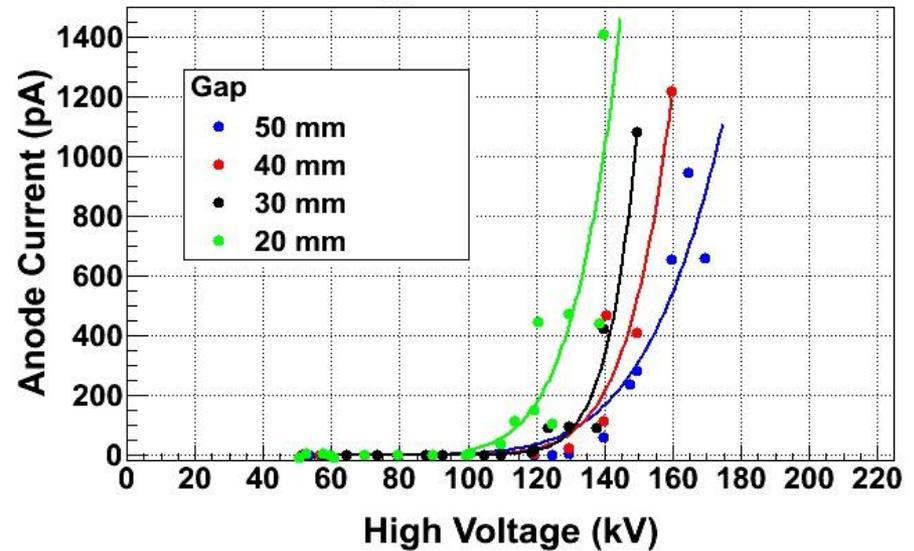
## Single Crystal Nb



## Fine Grain Nb

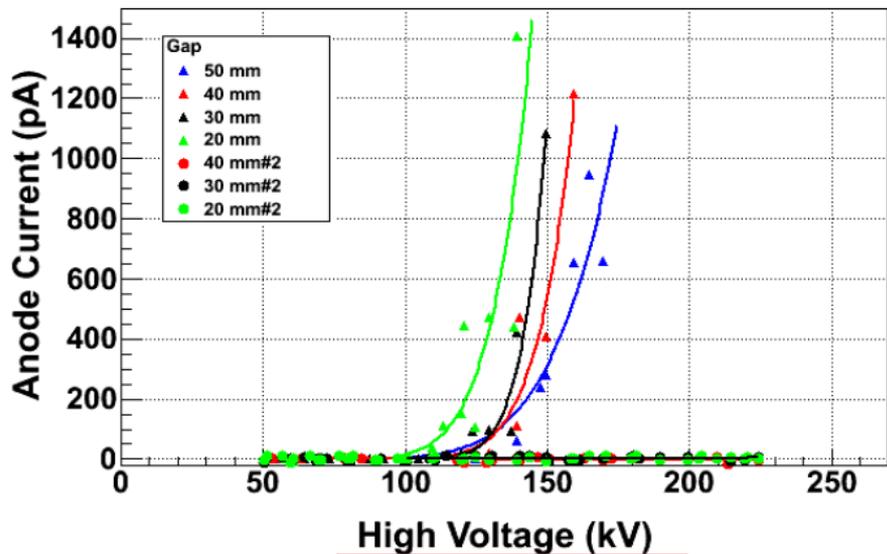


## Large Grain Nb

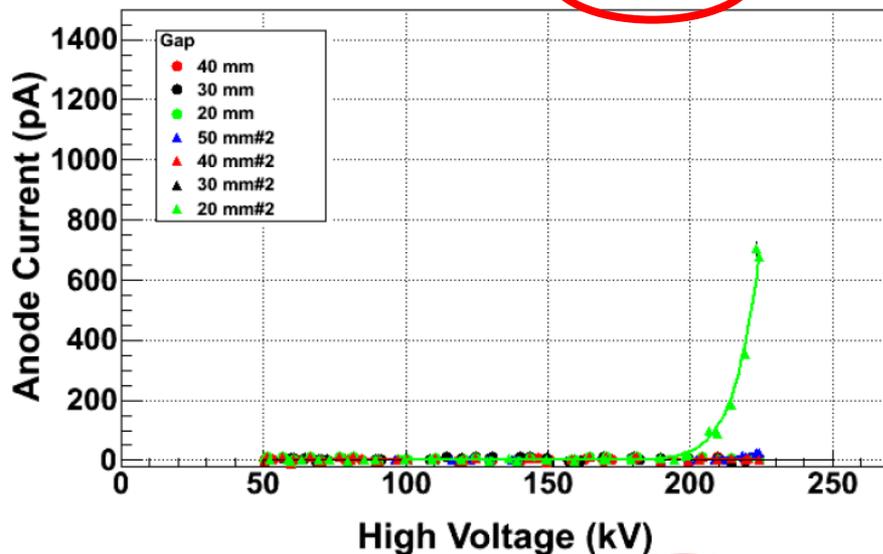


# Krypton Processing to Eliminate FE

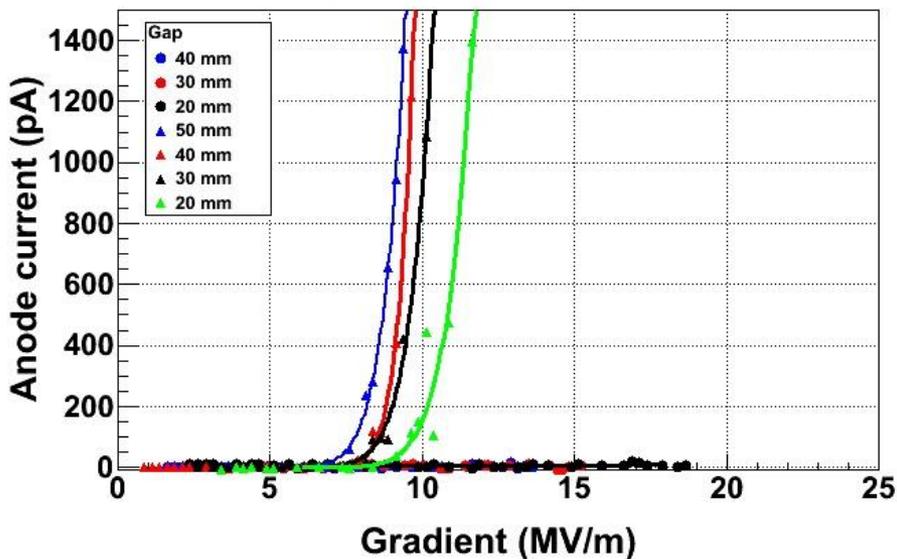
Large Grain Nb1 & 2 before Kr



Large Grain Nb after Kr



Large Grain Nb1&2 Before Kr



Large Grain Nb1&2 after Kr

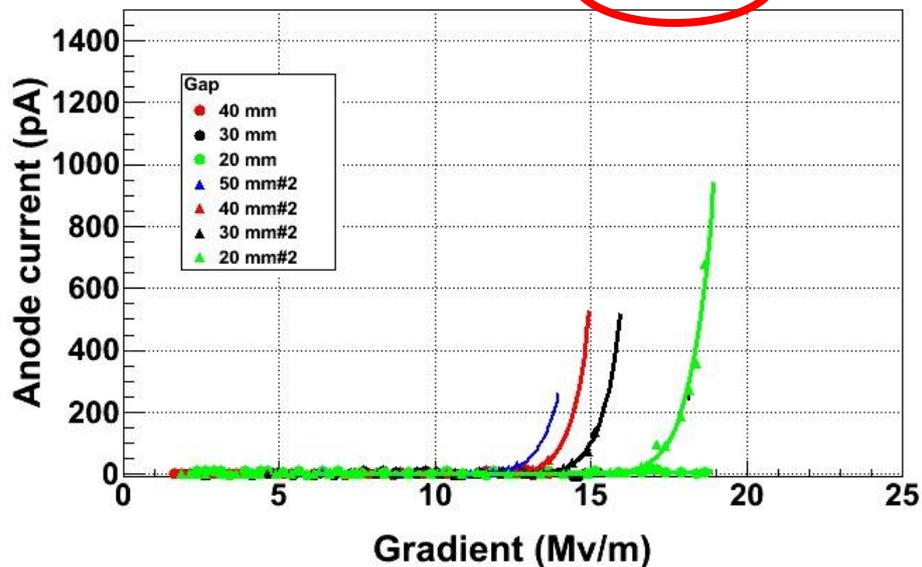
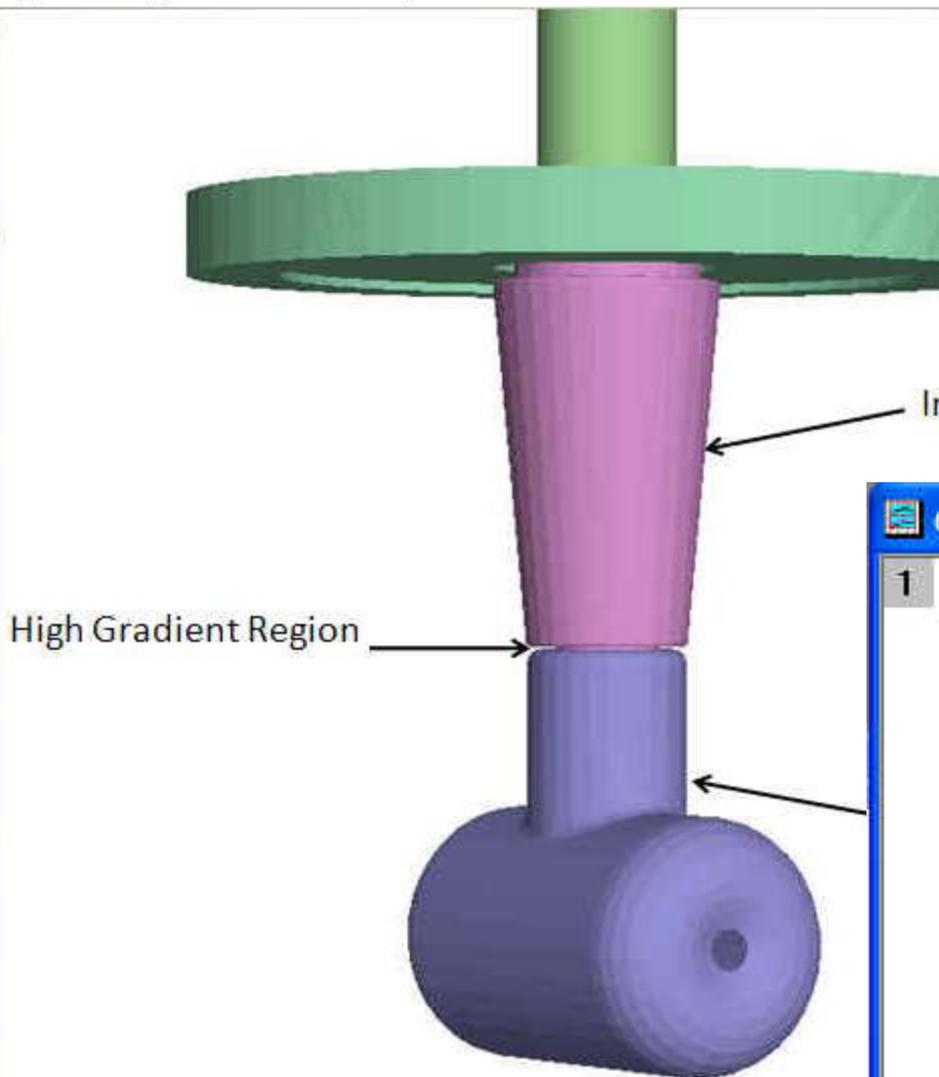
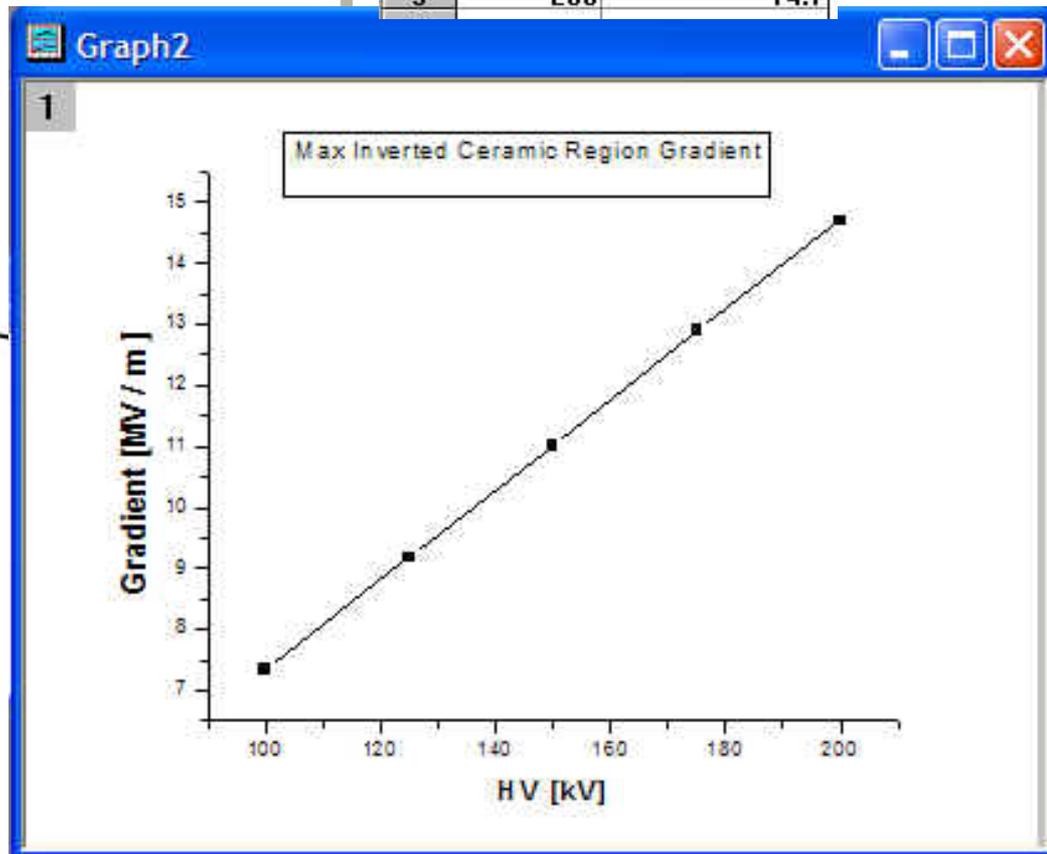


Figure 1: Highest Gradient Region

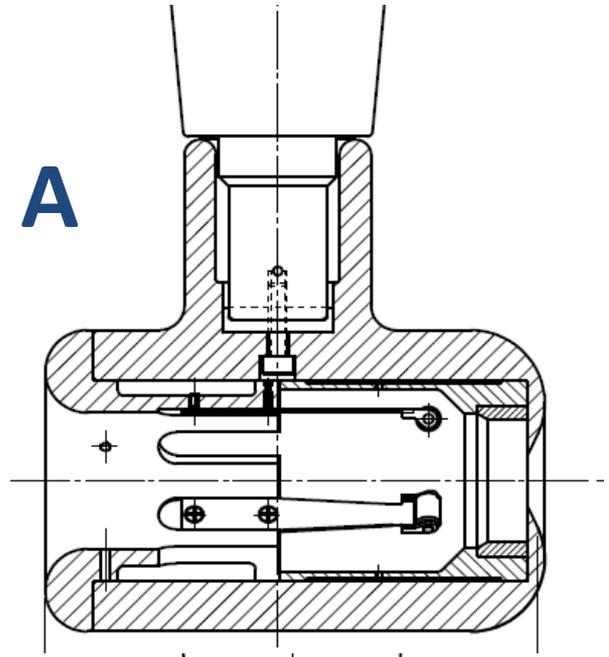


Our design has one region of “unintended” high gradient – could be problematic.....exploring new designs via electrostatic modeling

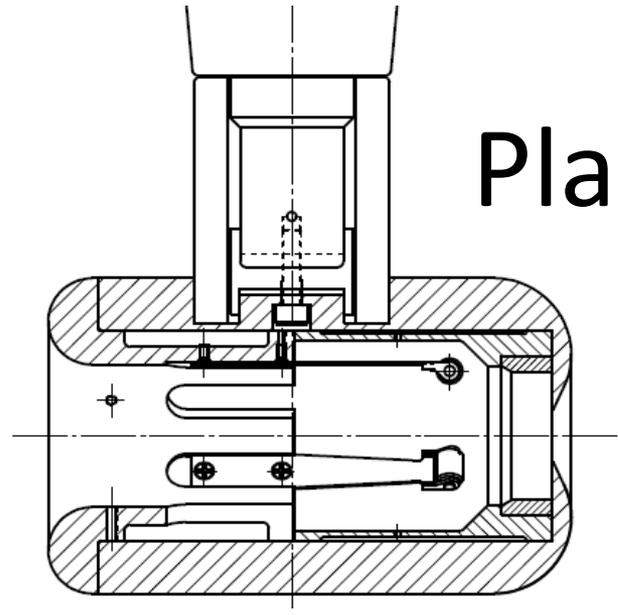
	A1[X]	A2[Y]
	HV [kV]	Gradient [MV/m]
1	100	7.35
2	125	9.18
3	150	11
4	175	12.9
5	200	14.7



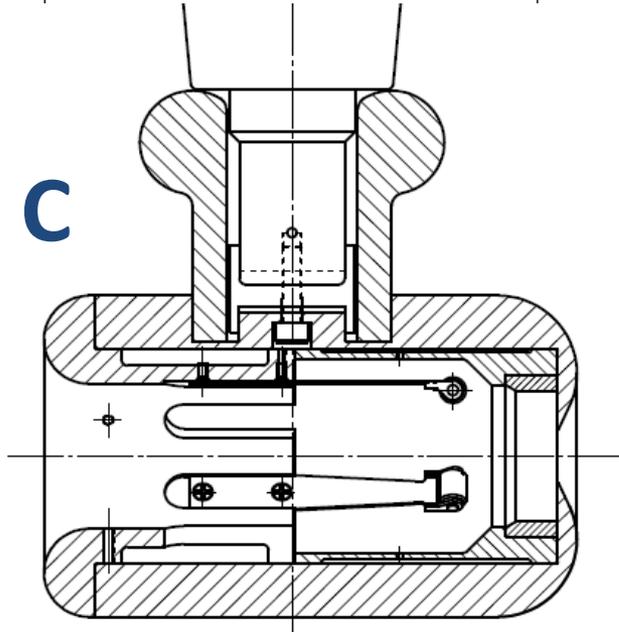
**Plan A**



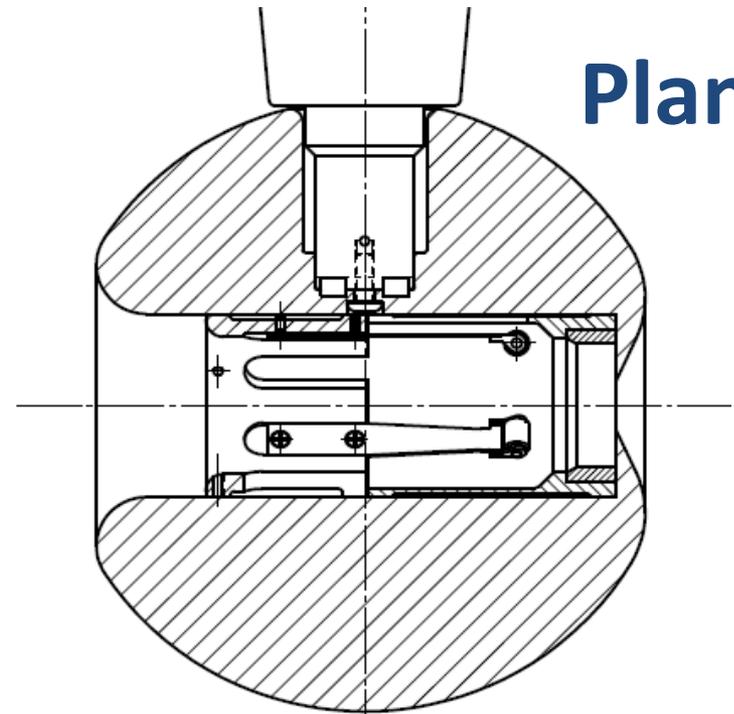
**Plan B**



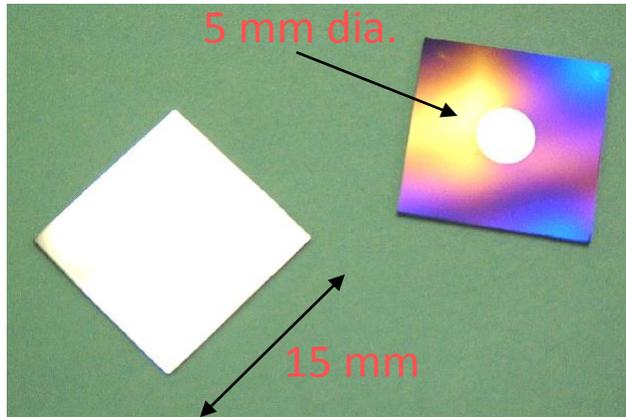
**Plan C**



**Plan D**



# Limiting the Active Area via Anodization



Normal photocathode;  
“out of box”

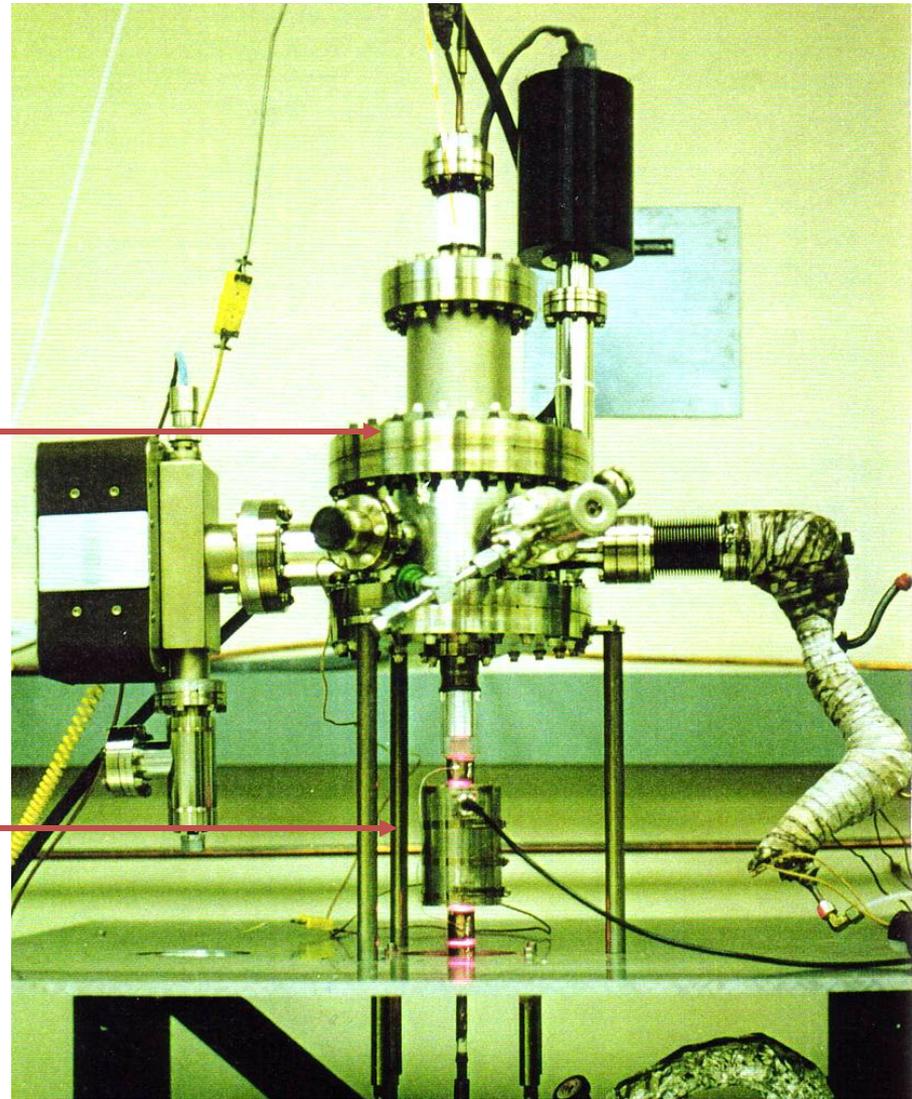
## Anodized photocathode

- Electrons emitted from edge of wafer hit vacuum chamber walls. This is bad for vacuum.
- Anodization eliminates inadvertent photoemission from locations not intentionally illuminated with laser light
- Anodizing process dirties the photocathode surface, bad for QE

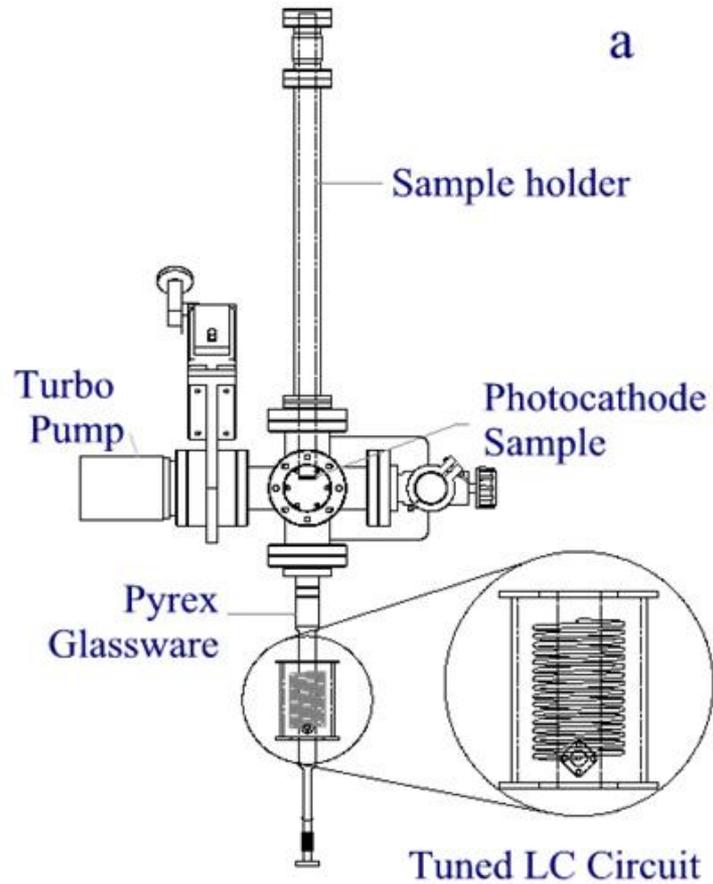
# Atomic Hydrogen Cleaning

Photocathode sits here,  
inside vacuum chamber

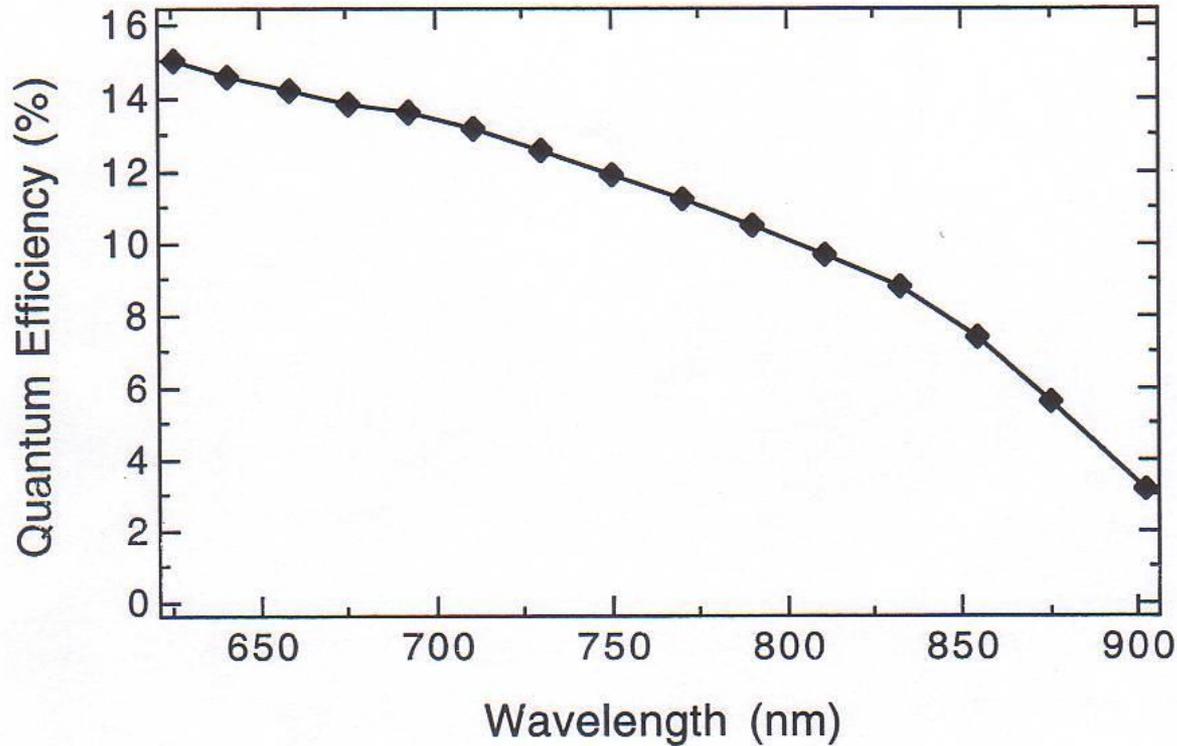
Molecular hydrogen  
dissociated with  
RF inductive discharge



# “Portable-H”

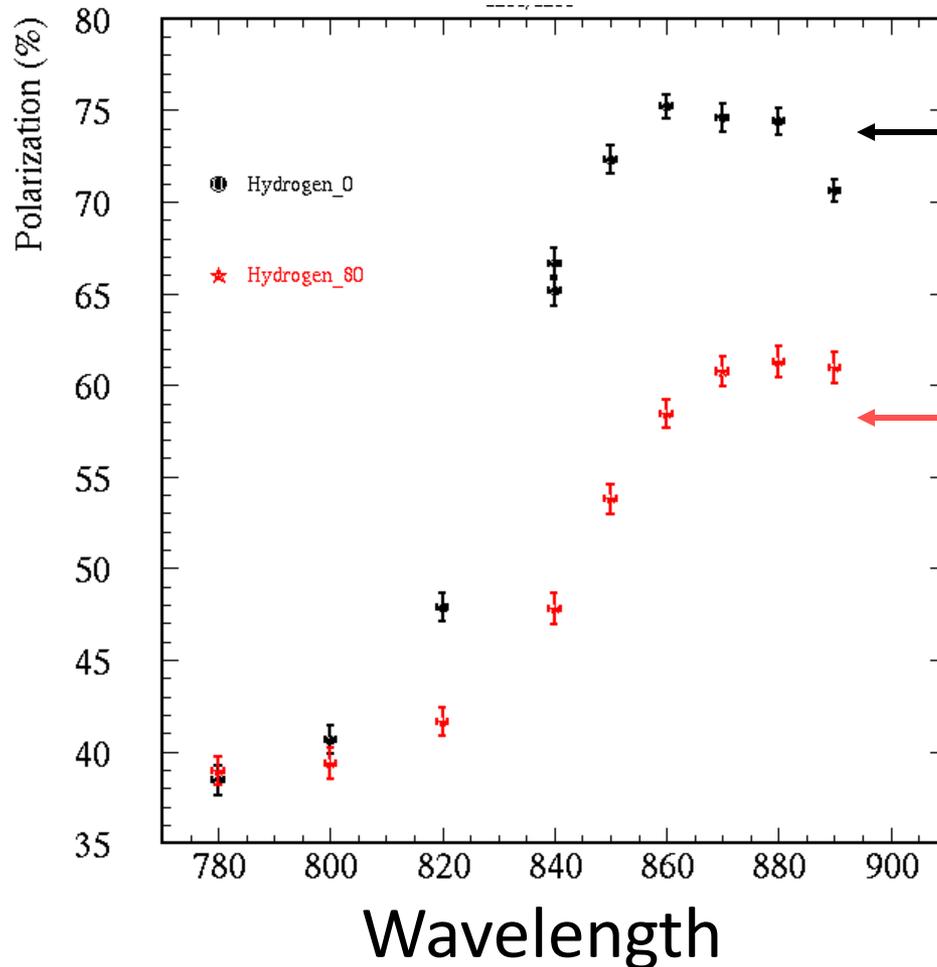


# Atomic Hydrogen Cleaning



- Extremely high QE from bulk GaAs
- Reliable cleaning method
- No wet chemicals
- *In situ* cleaning an option (i.e., put it on the gun or in prep chamber)

# But not for High Polarization Photocathodes



Polarization w/o  
Hydrogen cleaning

Polarization w/  
Hydrogen cleaning

Solution: Arsenic  
Capping and Masking

# Deep UHV gauges Theory and Practice

Marcy Stutzman  **Jefferson Lab**

Bruce Kendall Elvac Laboratories

# Pressure ranges

- ▶ Deep ultra high vacuum: below  $1 \times 10^{-10}$  Torr
  - ▶ Commercially available gauges exist
  - ▶ Care must be taken in using gauges properly
- ▶ Extreme high vacuum: below  $1 \times 10^{-12}$  Torr
  - ▶ Few room temperature systems obtain XHV
    - ▶ [Electron sources for accelerators](#) would benefit
    - ▶ Particle collider interaction regions
    - ▶ Reactive surface science applications
    - ▶ Nano-electronics
- ▶ Ionization gauges required to measure deep UHV
  - ▶ Hot filament gauges
  - ▶ Cold cathode gauges

# HOT FILAMENT GAUGES

Bayard-Alpert

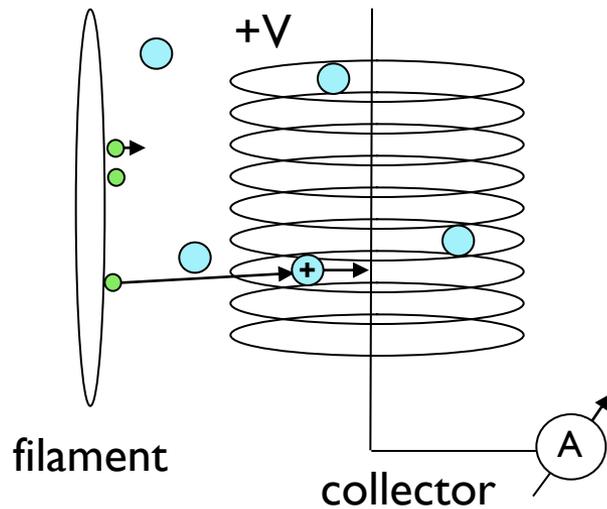
Modulated Bayard-Alpert

Extractor

Bessel Box

Bent Beam

# Hot filament gauges



- Electrons produced by hot filament
- Electrons accelerated toward biased grid
- Gas molecules ionized by electron impact
- Ionized molecules collected on wire
- Collector current proportional to gas density

$$P = nkT$$

# HOT FILAMENT GAUGE ERRORS

X-ray limit

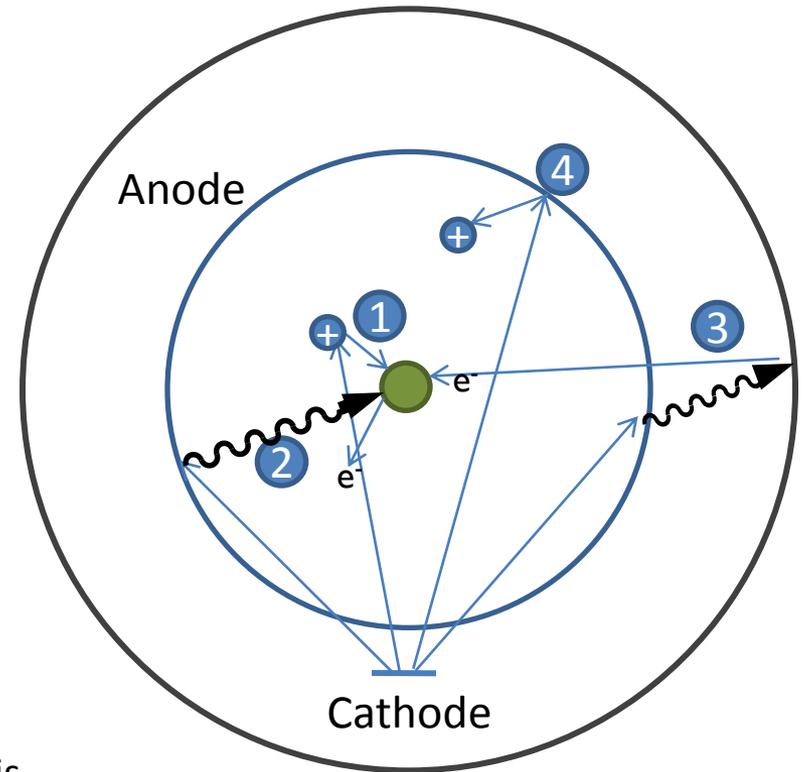
Inverse X-ray effect

Electron Stimulated Desorption

Outgassing from heated surfaces

# Hot cathode gauge operation and errors

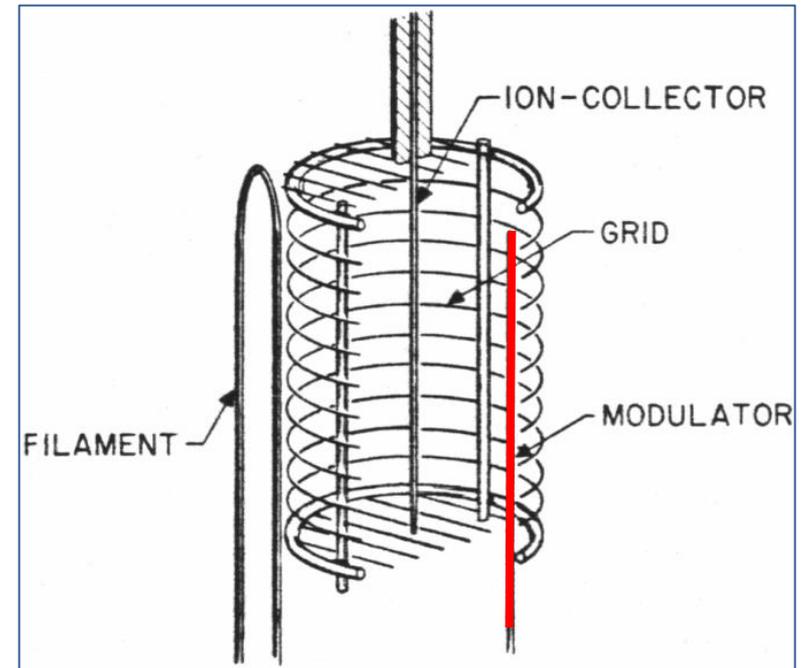
1. True gas ionization
  - Positive current
2. X-ray effect
  - e- on anode -> photons emitted
  - Photons on collector -> electrons emitted
  - Extra positive current
3. Inverse X-ray effect
  - e- on anode -> photons
  - Photons on walls -> electrons
  - Electrons to collector
  - Extra negative current
4. Electron stimulated desorption
  - e- strike gas molecules on anode
  - Gas ionized and reaches collector
    - can be distinguished with energy analysis
  - Neutral atom desorbed
    - Ionized within grid
    - Indistinguishable from real gas
    - Must eliminate source



$$I^+ = I_{real} + I_{x-ray}^- - I_{inv.x-ray}^- + I_{ESD}$$

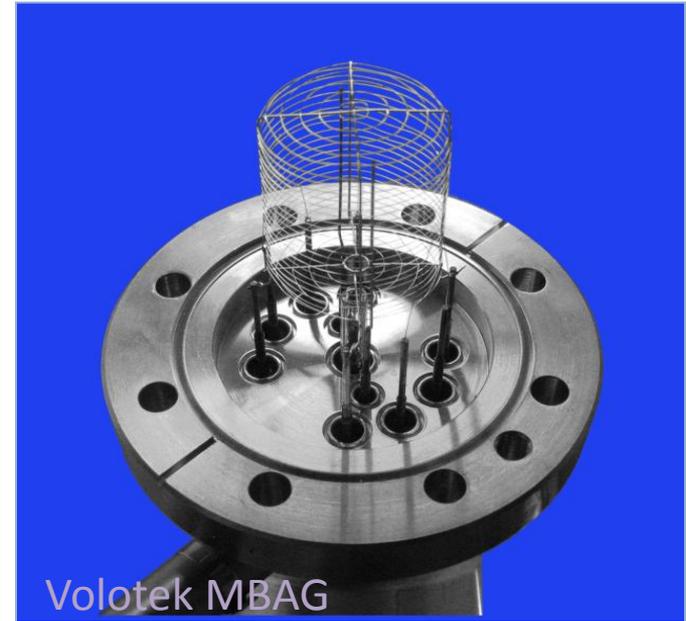
# Reduction of x-ray and ESD errors

- ▶ Modulation
- ▶ Geometry
- ▶ Extends BA gauge below  $10^{-9}$  Torr
- ▶ Redhead modulated gauges 1960s
  - ▶ ETI / Teledyne sold commercial version
- ▶ Modulator varied between potentials near grid and collector voltages
  - ▶ Careful selection of potentials required to avoid changing ESD and x-ray currents
  - ▶ Real signal modulates, background constant
  - ▶ High pressure ( $10^{-8}$  Torr) determination of modulation constant
- ▶ MBAG benefits
  - ▶ Retrofit existing BAG with external modulation unit
  - ▶ Unaffected by electrometer drift
  - ▶ Read pressure near/better? extractor gauge



# Reduction of x-ray and ESD errors

- ▶ CERN style commercial MBAG coming from Volotek
  - ▶ CERN vendor for MBAG controllers
  - ▶ Finishing prototyping
  - ▶ Commercial manufacturing run soon
  - ▶ Hope to exceed extractor capabilities
  - ▶ XHV vacuum work
    - ▶ heat treat flanges
    - ▶ ceramic feedthroughs (previously glass)
    - ▶ 4.5" flange – less wall interference
    - ▶ CERN working on qualification
- ▶ Televac/ETI have produced metal MBAG as special order – Kendall, custom electronics



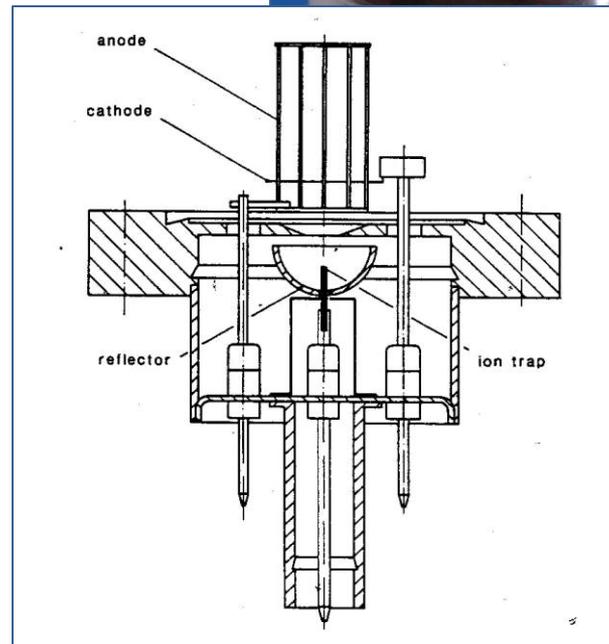
# Reduction of x-ray and ESD errors

## ▶ Geometry

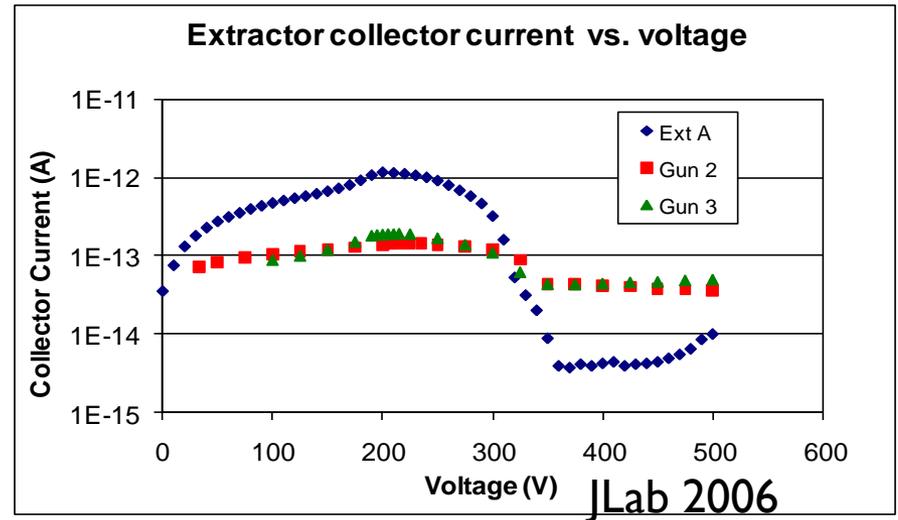
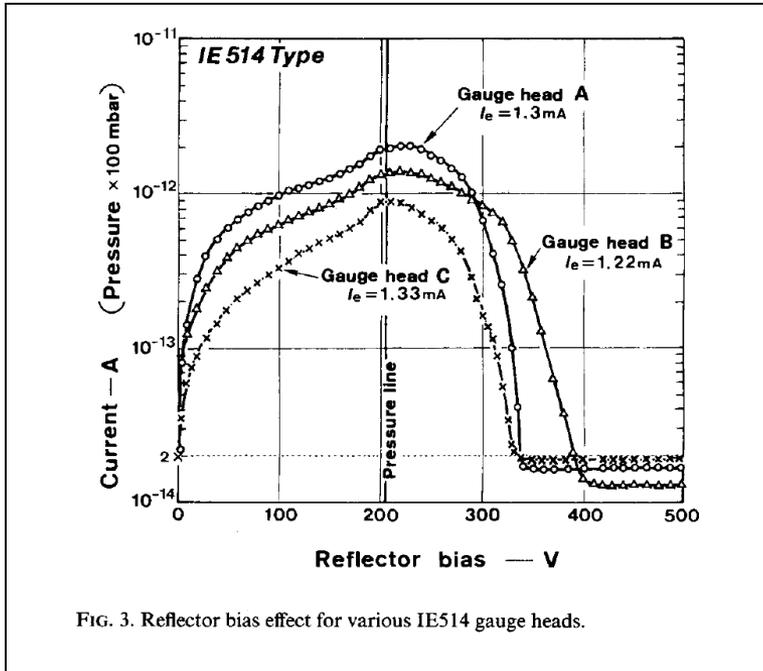
- ▶ Reduce collector solid angle (thin wire BA)
- ▶ Shield the collector from line of sight to the grid
  - ▶ Extractor
  - ▶ Bent Beam
    - Helmer
    - Ion Spectroscopy
  - ▶ Bessel Box
    - AxTran
- ▶ Energy discrimination
  - ▶ Repeller in extractor
  - ▶ Bent beam gauges



Oerlikon Leybold  
Extractor gauge



# X-ray limit measurements



Fumio Watanabe JVSTA 9 (1991).

Determines x-ray limit for certain setup

Current at reflector > grid

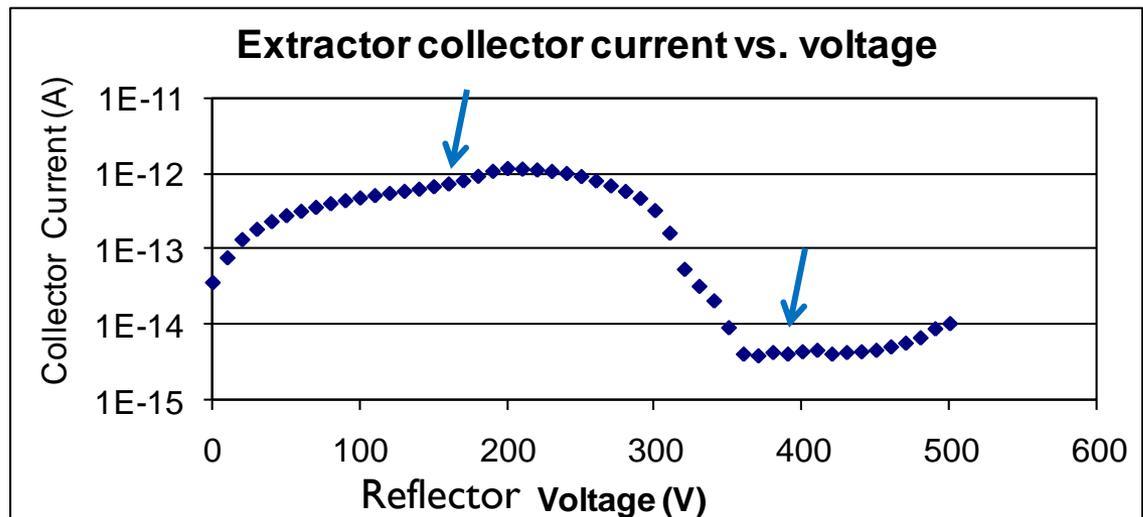
Current with voltages off

Gauge	X-ray Limit (Torr)
Watanabe A	$2.1 \times 10^{-12}$
Watanabe B	$1.6 \times 10^{-12}$
Watanabe C	$1.9 \times 10^{-12}$
JLab A	$0.63 \times 10^{-12}$
JLab Gun 2	$>2 \times 10^{-12}$
JLab Gun 3	$>2 \times 10^{-12}$

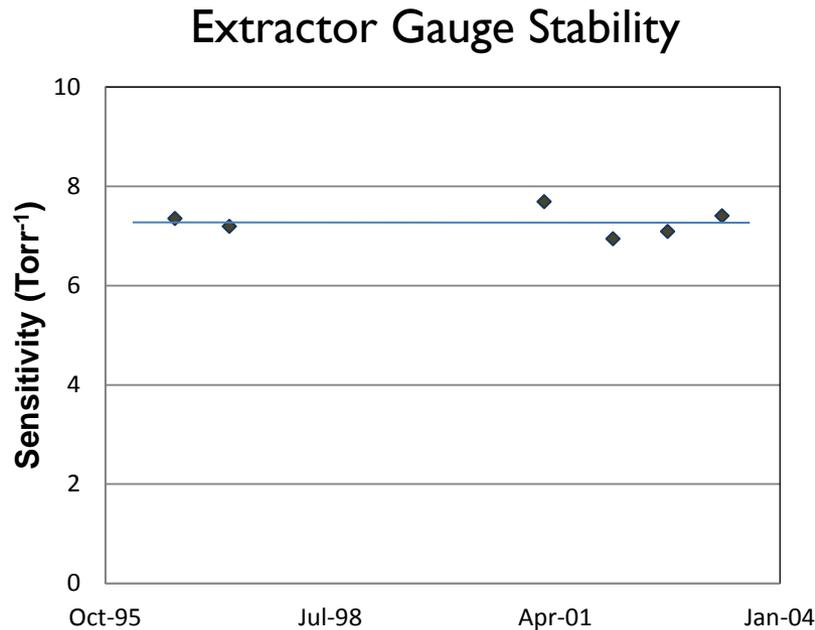
# Modulated extractor gauge

- Cornell vacuum group with Charlie Sinclair (retired)
  - Modulate reflector potential with AC voltage
  - Read signal using Lock-in amplifier system
  - Measure field-off current (often negative) and account for this
  - Real time measurement with compensation for x-ray limit

- ▶ Student project that requires follow-up
- ▶ Redhead 1966 modulated extractor with filament in grid – revisit?



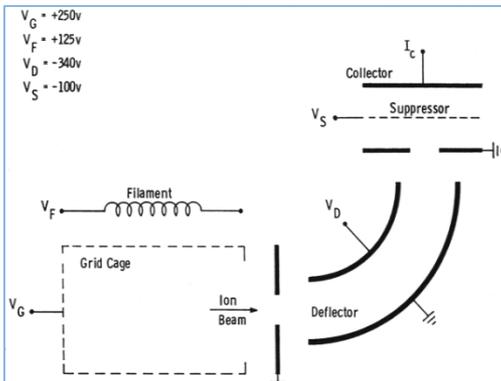
# Extractor gauge long-term stability data



- ▶ Excellent stability with near continuous operation for more than a decade
- ▶ Venting 3-4 times per year
- ▶ Largest sensitivity changes follow system bakeouts
- ▶ Factors affecting stability
  - ▶ Excessive heating - deformation
  - ▶ Contamination
  - ▶ Mechanical damage
  - ▶ Nude gauge mounting geometry
  - ▶ Degas protocol

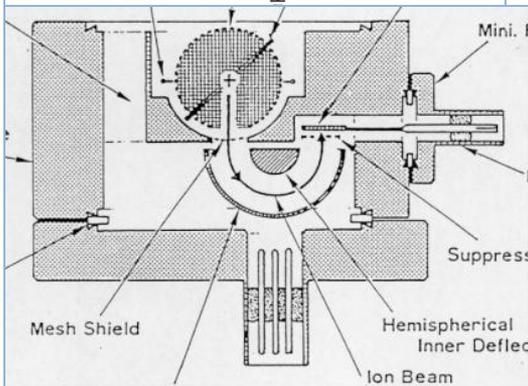
# Energy analysis for ESD ions

## Bent Beam Gauges



### Helmer/Improved Helmer

- 90° bend
- Distinguish against ions at grid potential
- <math>10^{-13}</math> Torr measured CERN ISR interaction region
- Volotek: available next year?

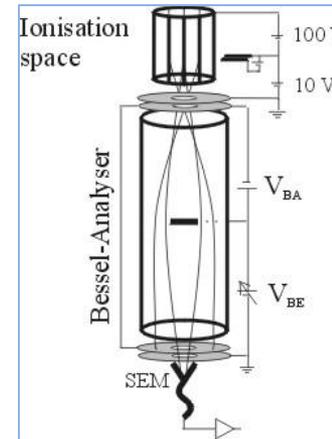


*Redhead:*  
For scientists energy analyzer gauges ideally have tunable energy for analysis

### Watanabe Ion Spectroscopy Gauge

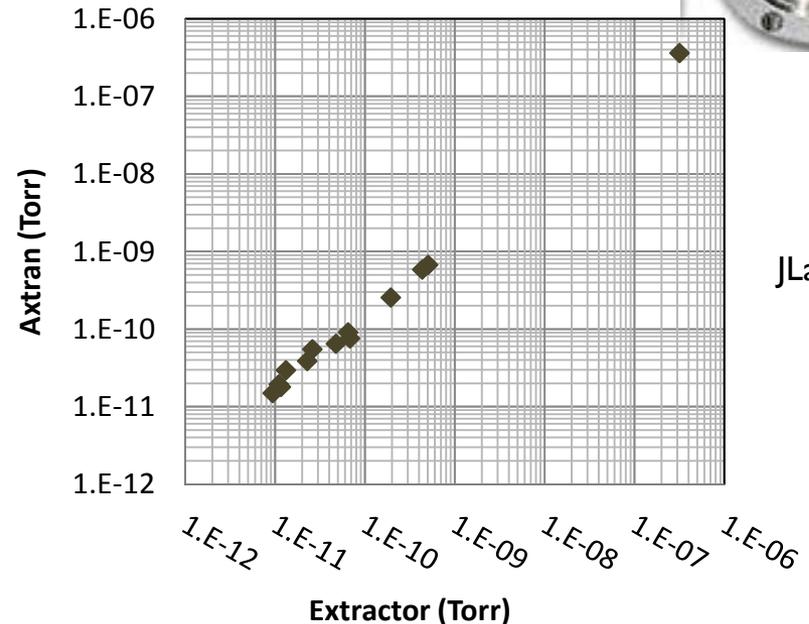
- 180° bend – hemispherical energy analyzer
- Spherical Grid - more uniform ion energy
- Not commercially available

## Bessel Box



### Bend ions

- High energy ESD ions blocked
- Sold as AxTran by ULVAC
- Good agreement with extractor
- Electron multiplier



JLab 2004

# Application notes

- ▶ Hot filament gauges will heat walls
  - ▶ Reduce heat of gauge (1 mA instead of 10 mA)
    - ▶ Outgassing from walls reduced
    - ▶ More gas adsorbed on grid, walls -> ESD increased
  - ▶ Use better wall materials
    - ▶ BeCu – Watanabe
    - ▶ Silco-steel™ – Kendall
  - ▶ Heat walls until molecules don't stick
    - ▶ Kendall: operation 700-800K eliminates adsorbed molecules on walls and grid
      - Eliminates ESD neutrals
    - ▶ Watanabe: heated grid / cold cathode gauge
- ▶ Electronics issues
  - ▶ Cable leakage
    - ▶ Replace coax cables with twin-ax or tri-ax
  - ▶ Electrometer stability
    - ▶ Always use same head/control unit combination
- ▶ Calibrate each gauge (vs. spinning rotor gauge) regularly for optimal performance

# COLD CATHODE GAUGES

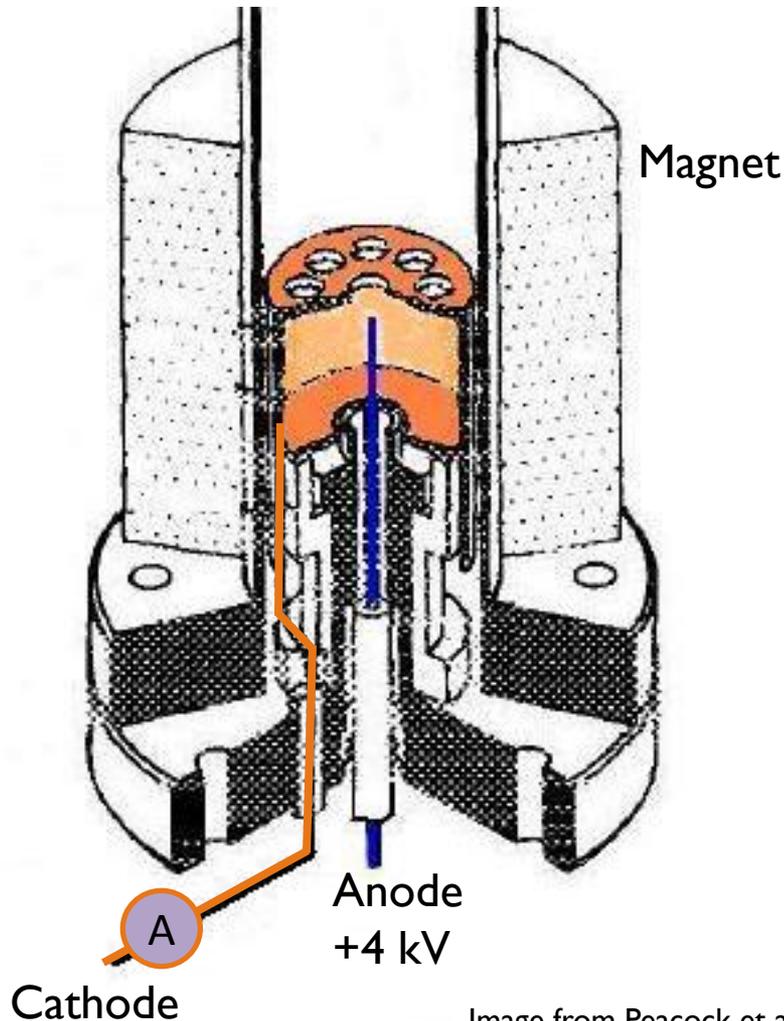
Magnetron

Inverted Magnetron

Double Inverted Magnetron

Ion pump?

# Cold Cathode Gauge Operation

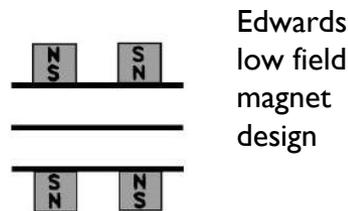
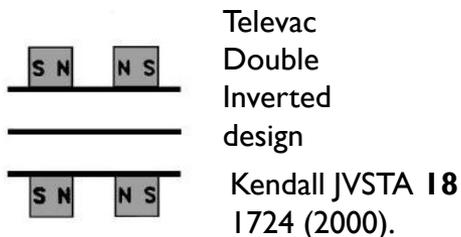


- ▶ Electron cloud trapped in crossed electric and magnetic fields
- ▶ Spontaneously starts in presence of electric field at HV pressures
- ▶ Electron cloud density limited by space charge effects
- ▶ Ionized gas collected at cathode
  - ▶ UHV starting element
    - ▶ Radioactive
    - ▶ Thermal
    - ▶ UV

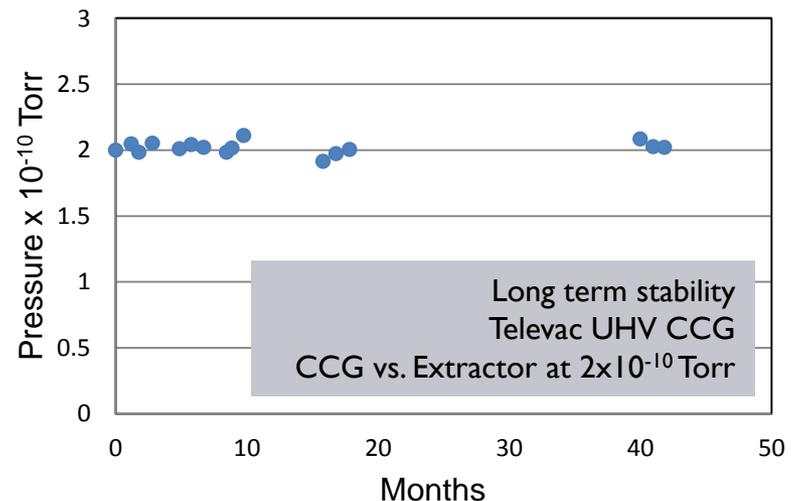
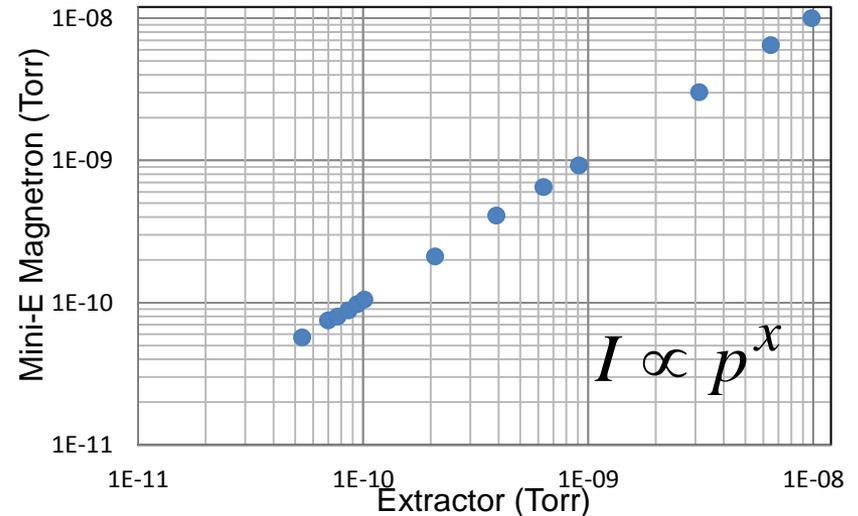
Image from Peacock et al.  
JVSTA 9 1977 (1991)

# Modern Cold Cathode Gauge

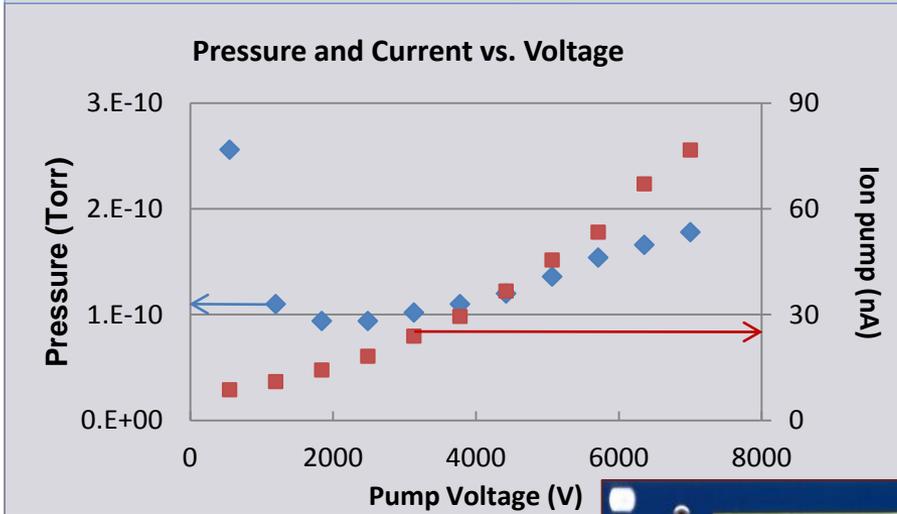
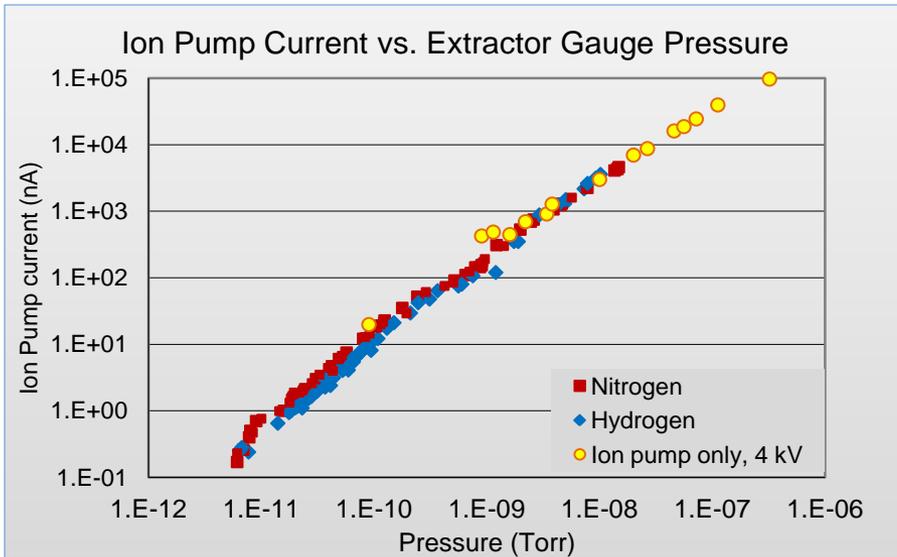
- ▶ No gauge heating
- ▶ Very rugged, low power consumption
  - ▶ Lunar missions, space applications
- ▶ Change in power law behavior at “magnetron knee”  $\sim 10^{-9}$  Torr
- ▶ Stray magnetic fields minimized in modern designs
- ▶ Accuracy for ELVAC modification of Televac CCG
  - ▶ Stronger magnets
  - ▶ Smaller volume
  - ▶ Precision alignment mounting jig
  - ▶ Controller improvements



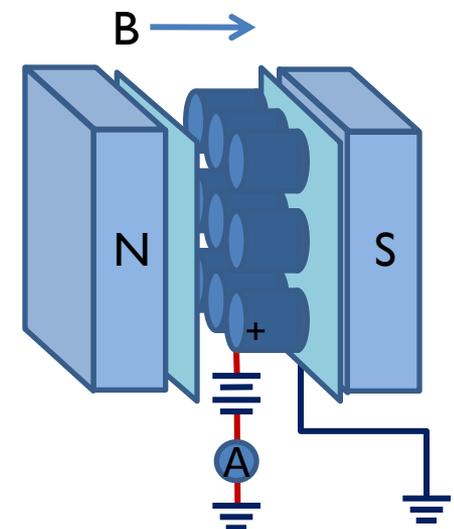
## CCG Accuracy



# Ion pump as a pressure gauge



- ▶ PE sputter DI pumps
- ▶ Penning cell
- ▶ Power supply with Electrometer



- Current linear vs. extractor gauge
- Minimum voltage to sustain discharge
- Does not work with all ion pump designs (Noble ion configuration)



# Conclusions

## Hot filament gauges

- X-ray limit, ESD ions
  - Geometry
  - Modulation
- ESD neutrals
  - Heated grid gauges
  - Novel materials
- Sensitive to abuse, contamination
- Lowest pressure measured with Helmer gauge

## Cold cathode gauges

- ▶ Rugged, low energy consumption
  - ▶ Lunar, space applications
- ▶ Compensation for “knee” in electronics
- ▶ Ion pumps with sensitive current monitor shown to work as a relative pressure gauge
- ▶ Extension of conventional gauges toward XHV requires more work

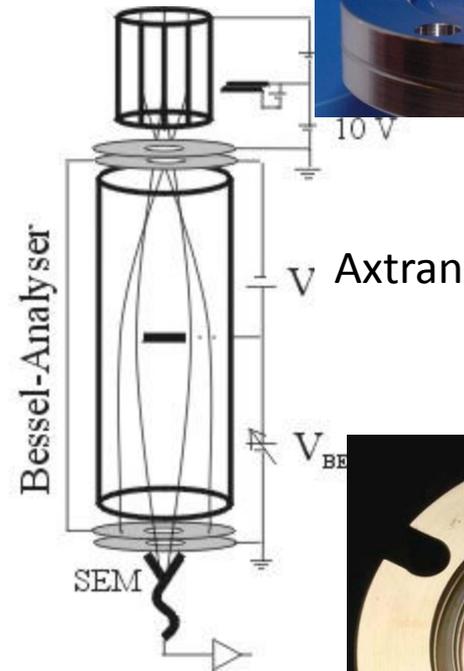
Small market – few commercially available gauges

Careful selection, utilization essential for accurate readings

Deep UHV gauges essential for improvements toward XHV

# Deep UHV/XHV gauges

- Extractor gauge
  - available for decades
  - x-ray limit reduced through geometry
  - x-ray limit quote:  $7.5 \times 10^{-13}$  Torr
- Axtran gauge
  - Bessel box energy discrimination
  - electron multiplier to assist in low current measurements
  - Purchased, not yet installed
  - Measurement limit quote:  $< 7.5 \times 10^{-15}$  Torr
- Watanabe BBB (Bent Belt Beam) gauge
  - Newly designed (JVSTA **28** (2010) p. 486)
  - Operates with Leybold IE540 controller
  - 230° degree deflector (similar to Helmer)
  - BeCu housing to reduce  $I_{\text{heating}}$
  - Manufacturer's lower limit:  $4 \times 10^{-14}$  Torr



# Pressure Measurement = Current Measurement

## *Ionization gauge current contributions*

$$I_{measured} = I_{real} + I_{x-ray} + I_{heating} + I_{ESD} + (I_{inv.x-ray} + I_{ESDneut.})$$

$I_{real}$ : pressure dependent gas phase ions – species sensitive

$I_{x-ray}$ : x-ray induced electron desorption from collector  
– reduce by geometry

$I_{ESD}$ : ions arriving at collector from electron stimulated desorption (ESD) of molecules on the grid  
– reduce by degassing grid

$I_{heating}$ : pressure rise due to filament heating – species sensitive  
– reduce by material selection, geometry, long duration

# Gauge characterization chamber

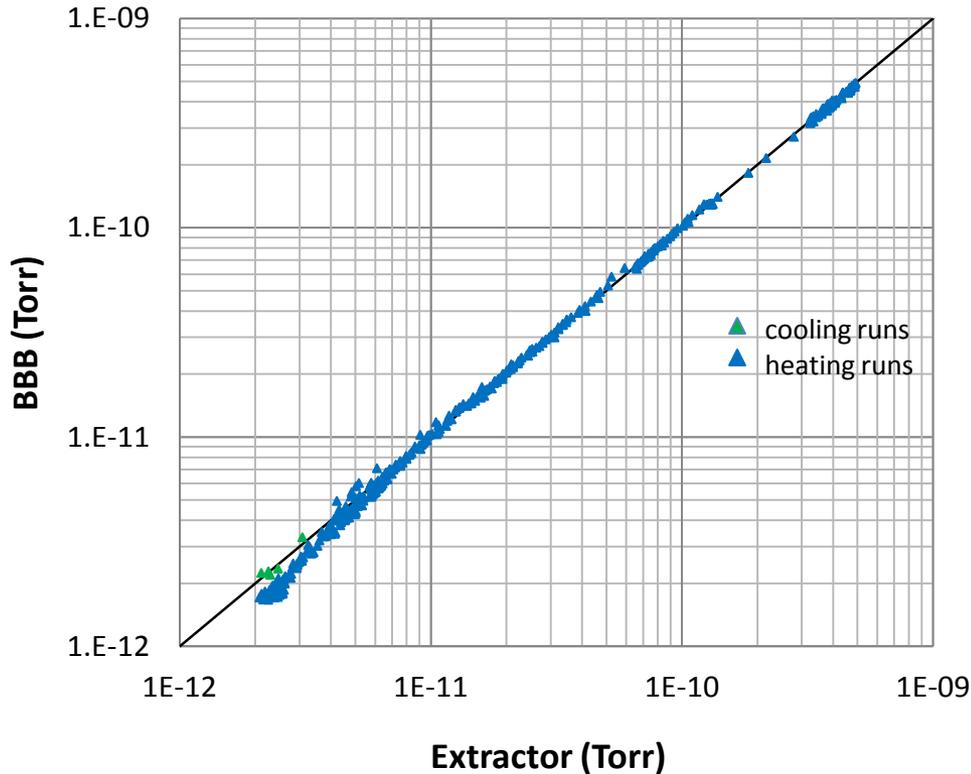
- Heat treated twice
  - 400°C 10 days
- Outgassing (Q)
  - $3 \times 10^{-14}$  Torr·L/s·cm<sup>2</sup>
- Q following 250°C bake
  - $6.3 \times 10^{-14}$  Torr·L/s·cm<sup>2</sup>
- 3800 cm<sup>2</sup>, 12L
- Pumping
  - 4 WP1250 NEG<sub>s</sub>, 60% 1300 L/s
  - 40 L/s ion pump (behind right angle valve)



**Predicted pressure**  
 **$2 \times 10^{-13}$  Torr**

- Extractor Gauge
- BBB Gauge
- 2 Leybold IE540 controllers
- 2 Keithley electrometers
- UHV ion pump power supply
- Diagnostic cross with RGA and ion pump
- NEG activation flange

# Linearity between gauges



BBB and Extractor compared vs. pressure

- Leybold IE 540 source
- Keithley Electrometer

Pressure varied in chamber by heating NEG's or chilling

Conversion to Torr using manufacturer calibration factor / sensitivity

- Depends on species
- Ionization energy
- Ionization current
- Geometry

Gauge responses linear response over decades, possible deviation at lowest pressures

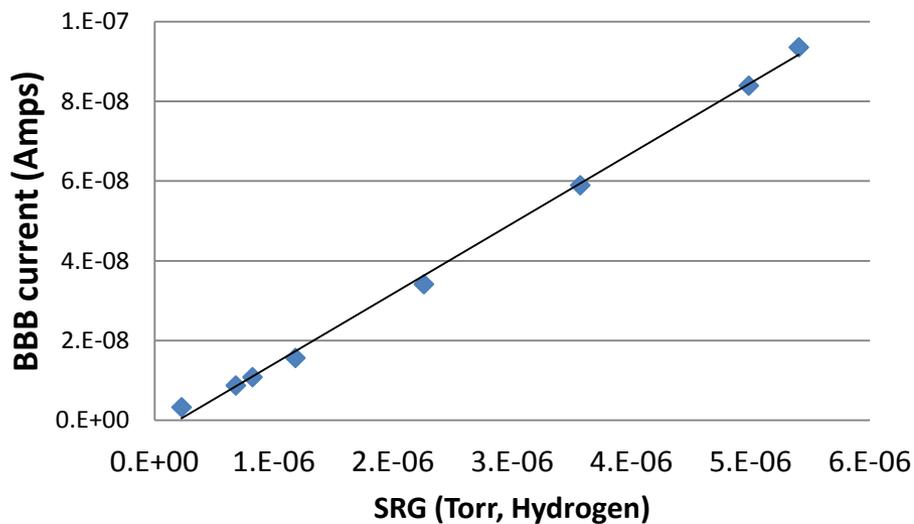
# Sensitivity

$$S = \frac{I_i \leftarrow \text{Ion current}}{P \times I_e \leftarrow \text{Emission current}}$$

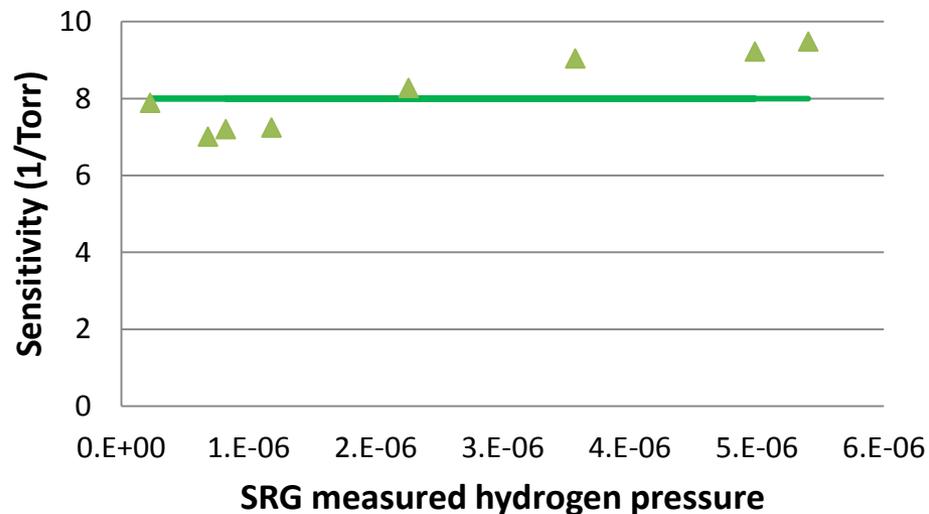
## BBB and Extractor

- 120V electron energy
- 1.6 mA emission current
- geometry, collection efficiency vary

### hydrogen pressure rise



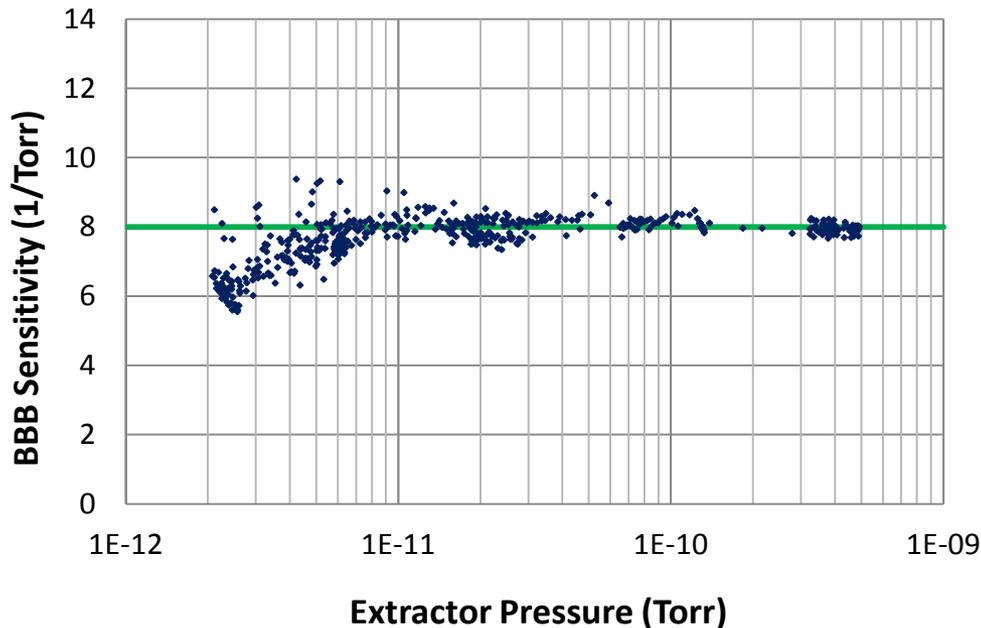
### BBB sensitivity vs. SRG



*BBB vs. SRG data from previous setup*

# BBB sensitivity calculated using extractor

SRG Data: pressure  $10^5$  higher than our area of concern  
Calculate BBB sensitivity from Extractor gauge pressure?



Calculated Extractor pressure relies on sensitivity of extractor gauge.

$$P = \frac{I_i}{S \times I_e}$$

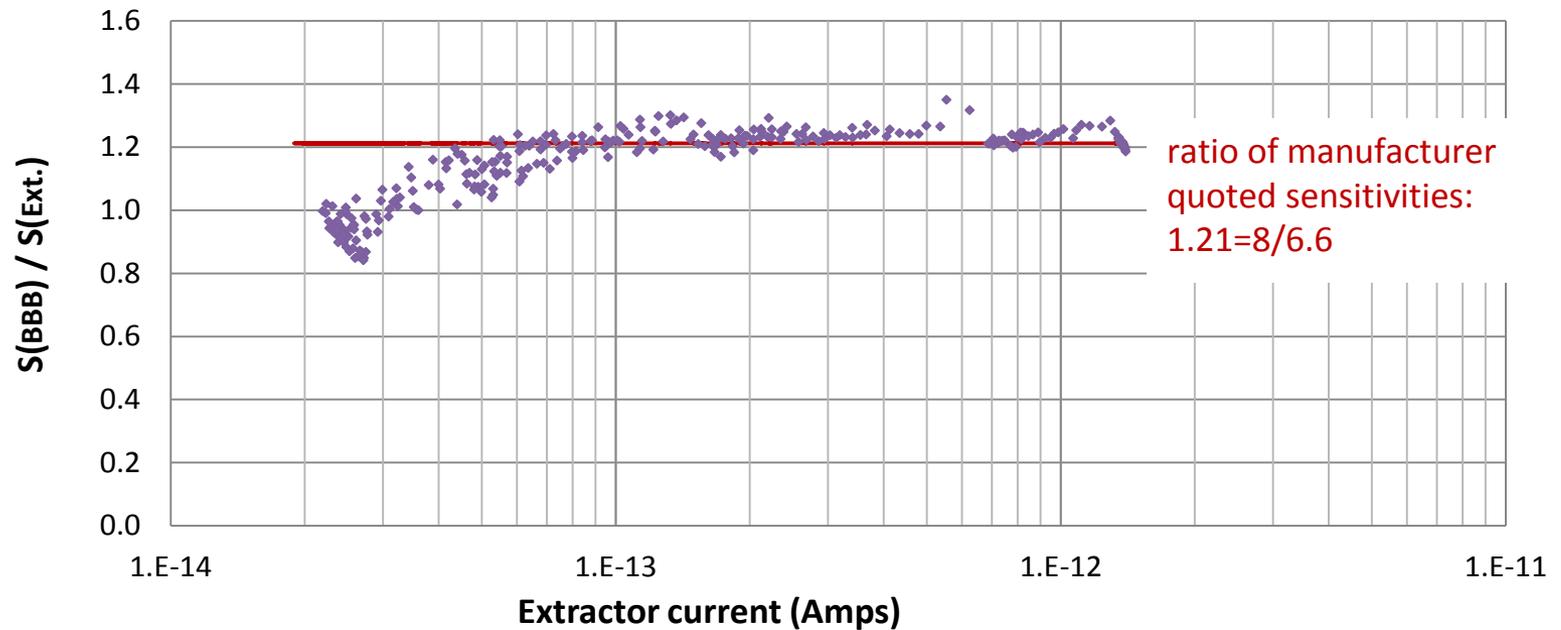
Gauge sensitivity depends on

- Ionization energy
  - Gas species
  - Geometry
  - Collection efficiency
- } *same*
- } *constant*

# relative sensitivity

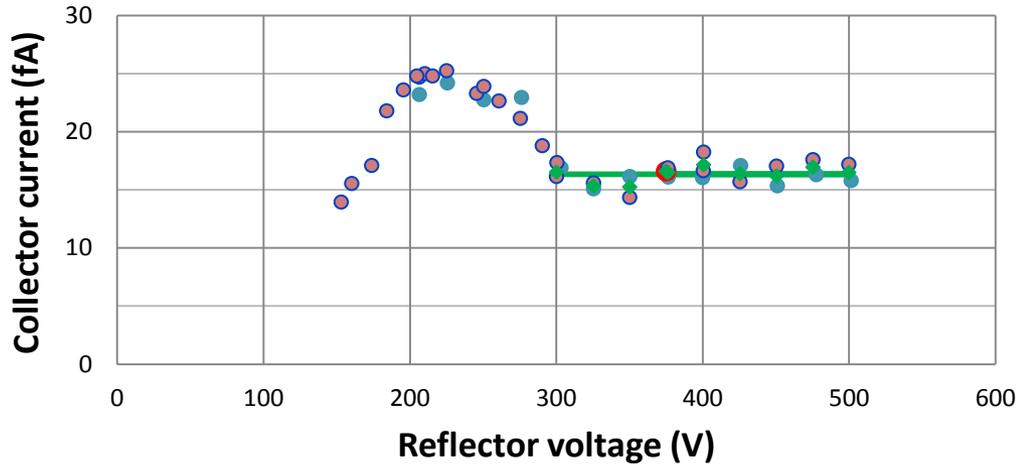
Define sensitivity ratio  
- should be constant

$$\frac{S_{BBB}}{S_{EXT}} = \frac{I_{BBB}}{I_{EXT}}$$

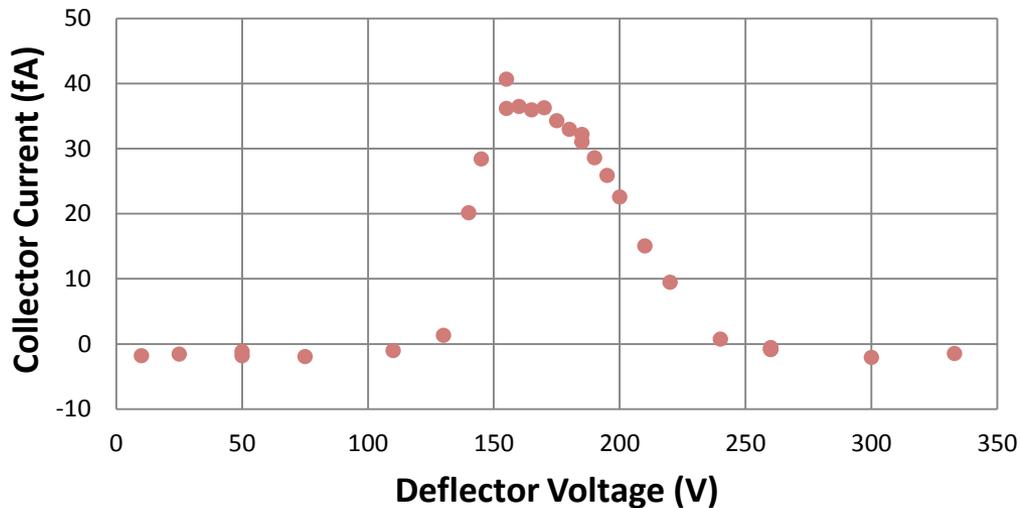


*Can the deviation from constant behavior be explained by gauge backgrounds?*

# Background current measurements



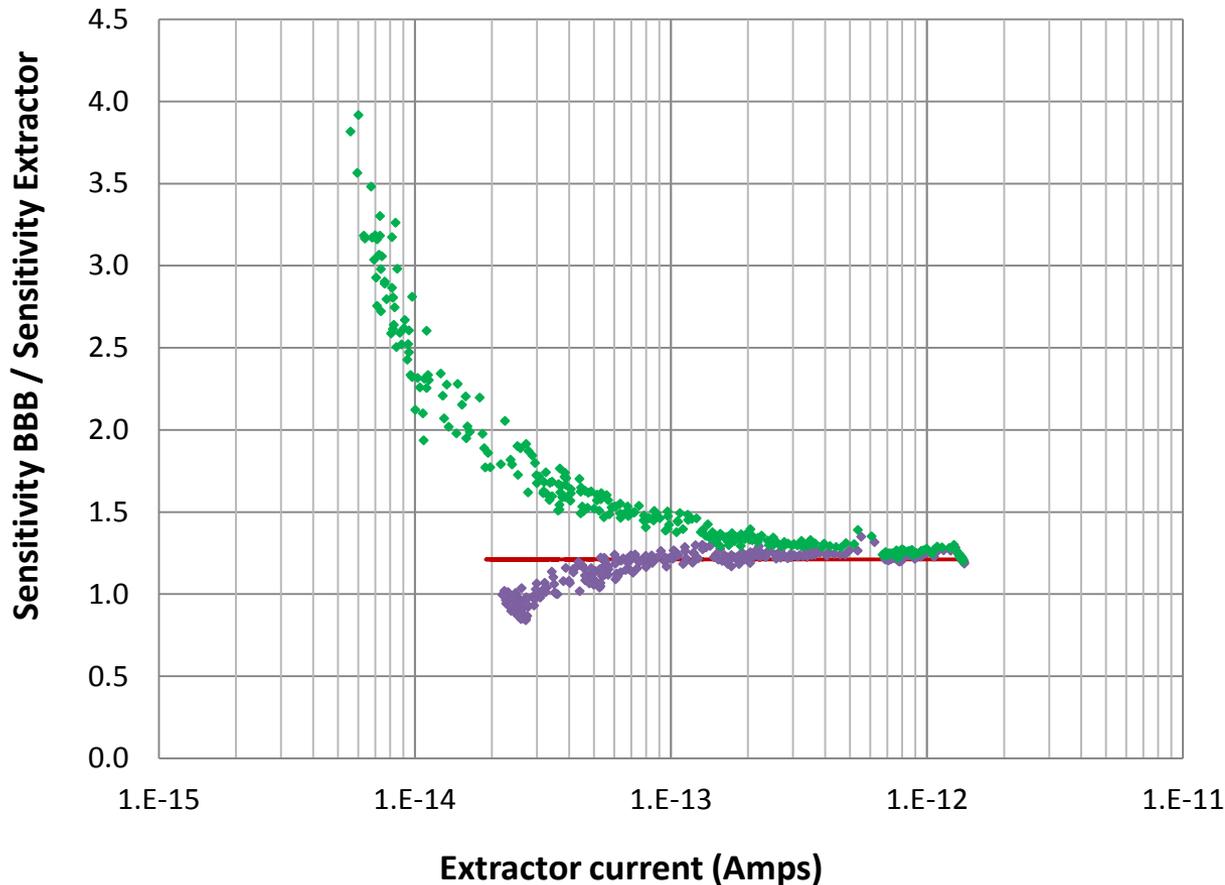
Extractor x-ray current  
accounts for  
3/5 of total measured signal



BBB signal of 35 fA with  
background of -1 fA

*Gauge backgrounds  
measured at different  
times, different pressures*

# Sensitivity ratio: x-ray limit correction

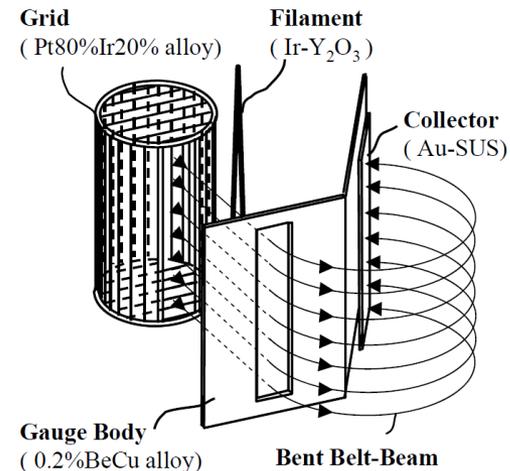
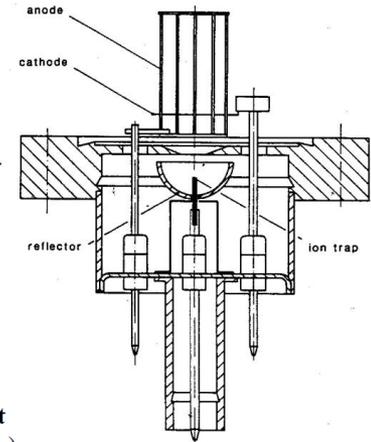


- Subtraction of x-ray background for extractor gauge overcorrects
- **What else?**
  - ESD limits
  - Load due to gauges
  - Small current measurement errors
  - nonlinearity in gauge response?

# Electron stimulated desorption

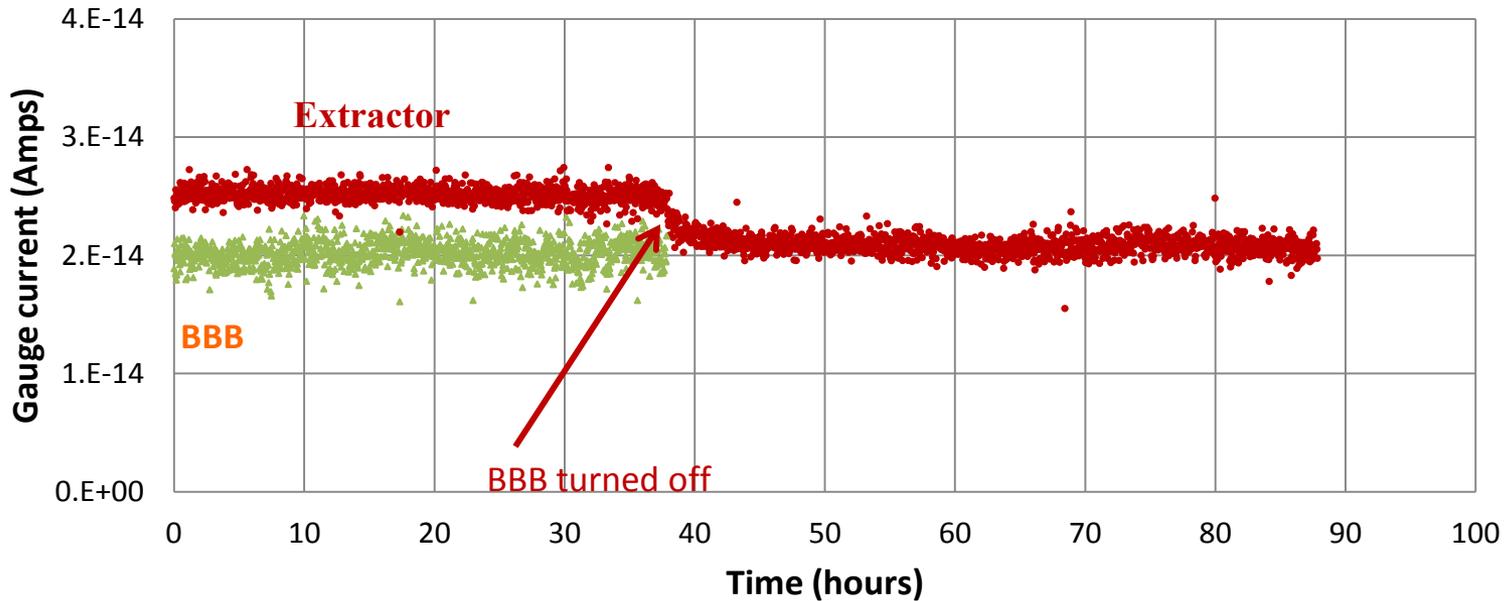
$$I_{measured} = I_{real} + I_{x-ray} + I_{heating} + I_{ESD} + \dots$$

- Electrons can liberate elements adsorbed on the grid
- If grid - filament potential equal to electron energy, ESD difficult to separate
- Methods to reduce ESD
  - high energy electron bombardment (degas mode)
  - operate grid at elevated temperature
  - grid material optimization (BBB)
  - stabilize for months
  - Axtran: energy analysis since electron energy  $\neq$  grid-filament potential



# Current due to heating by filaments

$$I_{measured} = I_{real} + I_{x-ray} + I_{heating} + I_{ESD} + \dots$$



Use one gauge to measure the additional current generated by other hot filament

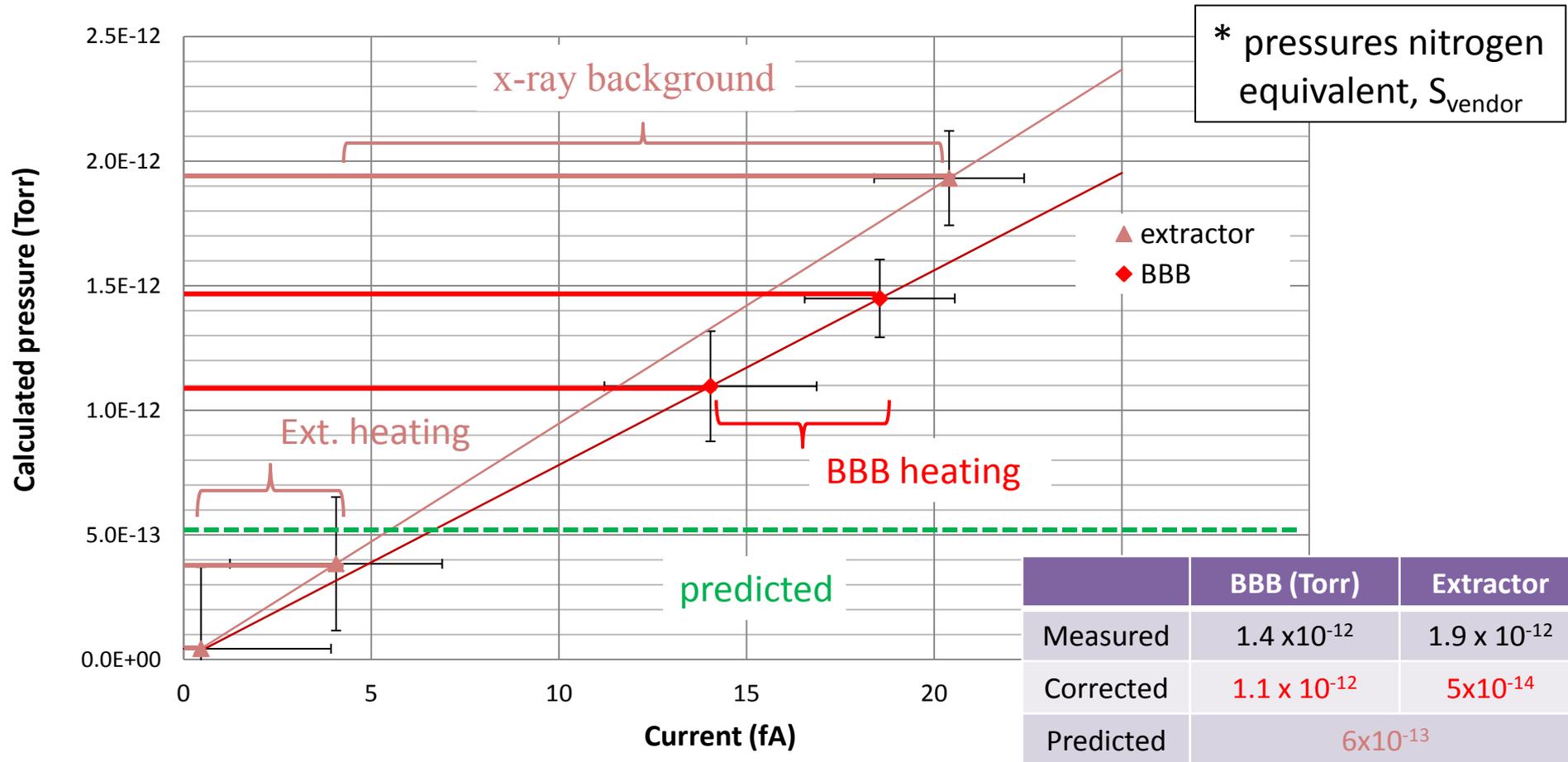
$$\Delta I (\text{BBB}) = 4.8 \text{ fA}$$

$$\Delta I (\text{Extractor}) = 5.6 \text{ fA}$$

*BeCu BBB housing should reduce effect  
Difference minimized after 6 months?*

# So what is our pressure?

$$I_{measured} = I_{real} + I_{x-ray} + I_{heating} + I_{ESD} + \dots$$



# Conclusions

- Pressure in our systems (nitrogen equivalent) corrected for gauge effects is near  $1 \times 10^{-12}$  Torr
- BBB signal to noise good: Noise < 10% signal
- Extractor gauge: measurements at lowest pressures dominated by background
- BBB and extractor agree very well above  $1 \times 10^{-11}$  Torr, diverge at lowest pressures
- The BBB gauge should be able to quantify pressure improvements in the bakable cryopump system.

Back up slides

# Emittance and Brightness

- Normalized Emittance from GaAs:

$$\varepsilon_{n,x,y} = \sqrt{\frac{q}{4\pi\varepsilon_0 E_s} \frac{k_B T_{eff}}{m_e c^2}}$$

$q$  Bunch Charge (= 0.4 pC, 200  $\mu$ A and 499 MHz)

$E_s$  Electric Field at GaAs surface

$T_{eff}$  Effective Temperature of GaAs (= 300 – 400 K, 780 nm)

$k_B T_{eff}$  Thermal Energy (= 34 meV)

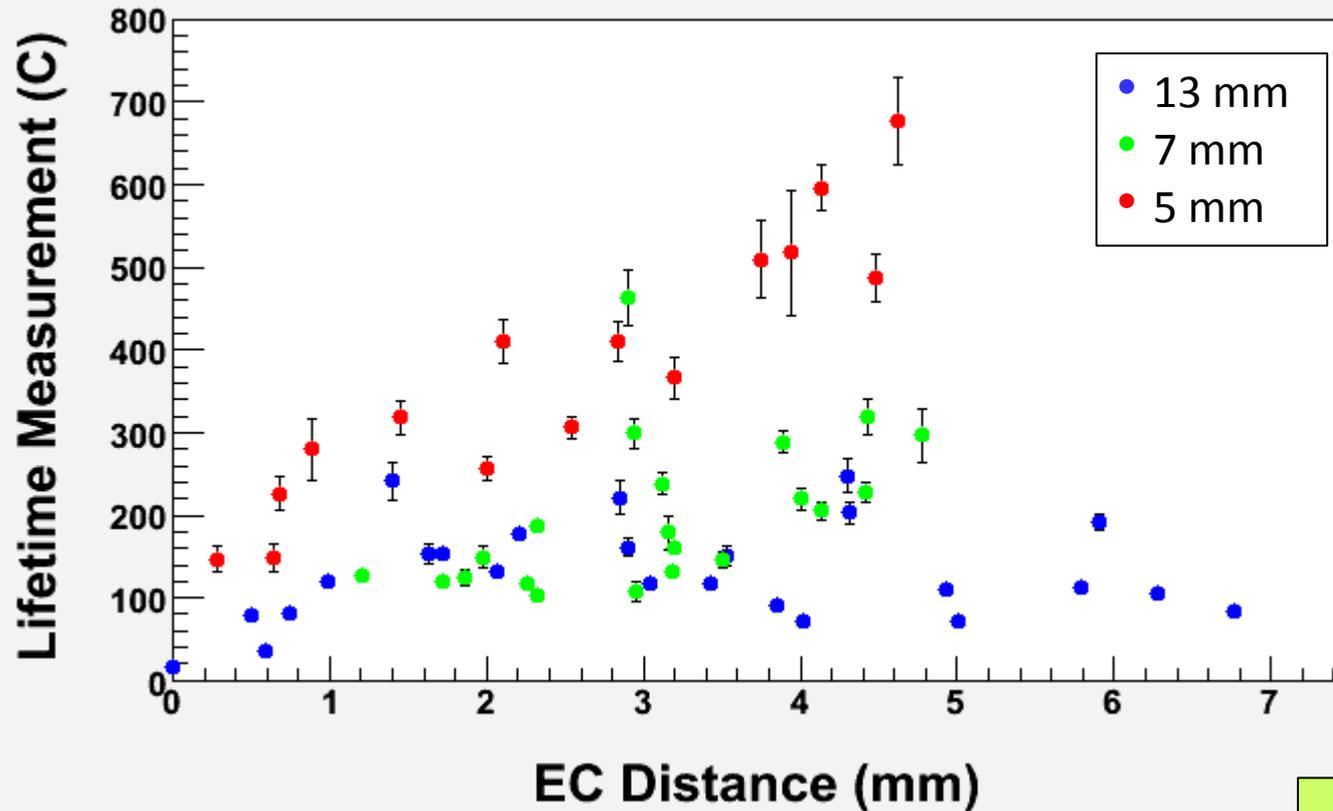
Gun HV (kV)	$E_s$ (MV/m)	$\varepsilon_n$ ( $\mu$ m)
100	2.0	0.011
140	2.8	0.009
200	4.0	0.008

- Normalized Brightness:

$$B_n \propto \frac{1}{\varepsilon^2} \propto E_s$$

Brightness is proportional to Gun HV

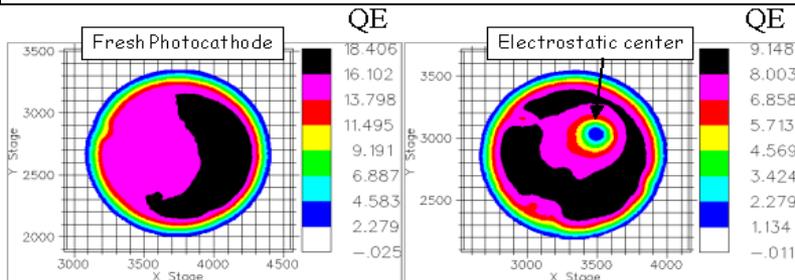
# InvGun2 : Lifetime at 2mA and 100kV bias: Versus Laser Position and Active Area



DC beam from bulk GaAs, green light and 350um spot.

Similar (good) results as with older guns, at 100kV

Finite lifetime due to ion back-bombardment



Work of Riad Suleiman

